

# Electrical Existing Conditions and Building Load Summary Report 

## Executive Summary:

This Electrical Existing Conditions and Building Load Summary Report will describe the general and specific characteristics of the existing electrical systems, summarize the total building electrical loads, and check of the size of the existing main distribution equipment of the Greater Hartford Academies for the Math and Sciences Building. This report also contains a single line diagram of the electrical distribution system, as well as narratives describing the system type, building utilization voltage, transformer configuration, emergency power systems, over-current protective devices used in the building, general location of electrical components, typical lighting systems used, and power factor correction. Important design requirements that pertain specifically to the building are also addressed within the report. A calculation of the NEC design loads were also performed using the available data and then compared to the actual electrical systems equipment used within the building. Also as an analysis of the energy requirements of the building, a summary of the utility rate structure is also included.

After analysis of the building using the NEC electrical design demand factors, there are several performance conclusions regarding the existing electrical system. First, the total KVA load calculated for each sub panel was well under the KVA rating of the panels, and the total current delivered to the panels was well under the rating of feeder over-current protective devices. But, when the total electrical load of the building was calculated, it was significantly more than the rating of the main distribution panel (about 150 KVA). There may be several reasons for this inconsistency. First, the recorded 1200 A main circuit breaker seems small for a building of this size and type, so further investigation (through verification by the electrical designer) is required to make sure that the correct switchboard size is on the drawings. Also, the building loads as defined by the panel boards on the drawings might be larger than the actual loads used within the building and these will be verified as soon as the utility information is received from the power company.

# Electrical Existing Conditions and Building Load Summary Report 

The Learning Corridor's Greater Hartford Academies for the Math and Sciences building is a unique public teaching facility that has both traditional classroom areas and many special purpose spaces such as interdisciplinary science 'suites,' as well as studios for dance, recording, and creative writing. The lighting design challenges of the space will be to enhance the performance of the current lighting systems to support the function, architecture, and efficiency of the spaces. This report will describe different aspects of the existing electrical system, as well as document other aspects related to building power, distribution, and regulation of the electrical demand within the building.

## System Type

The system type is a radial power distribution system because all power is supplied by the main distribution panel which has one primary feeder and transformer.

## Building Utilization Voltage

Electrical power is supplied to the building by a 208/120V, $3 \phi$, 4W system.

## Transformer Configuration

The transformer is rated to convert utility supply voltage to $208 / 120 \mathrm{~V}$ and is provided by the utility company. The utility transformer is located in Transformer Room 175.

## Emergency Power Systems

The building does not an emergency generator. Emergency lighting is provided using battery ballasts. Exit signs are LED type with battery back up.

## Over-current Protective Devices

The over-current protective devices used within the building are located in several locations. The main location is on the main distribution panel located in the first floor switchgear room. The main distribution panel has a 1200A, 3 pole circuit breaker. This main panel feeds almost all of the other panels located throughout the building and contains 3 pole circuit breakers of type 60A, 100A, 125A, 175A, 225A, and 400A. All panels are main lug only panelboards.

There is also a protective device on a panel located in a first floor electrical room that feeds a panel located within the same electrical room and is protected by a 3 pole, 60A circuit breaker.

The circuit which feeds the elevator 25 hp motor from the main panel is protected by a 175A, 3 pole circuit breaker on the main panel, and also a fused disconnect switch rated 125A.

## Locations of Electrical Control Gear

The location of the main distribution panel is in the first floor switchgear room. Lighting panels are located in storage rooms and closets on the first and second floor. Power panels and control panels are located in the main electrical room on the first floor, closets, storage rooms and hallways on the first and second floors. Mechanical panels are located in the switchgear room, the mezzanine and a second floor closet.

## Typical Lighting Systems

The lighting for the building (outdoor and indoor) is of 4 main types: fluorescent, high intensity discharge, incandescent, and halogen.

- All fixtures operate at 120 V .
- Most high intensity discharge lamps are metal halides.
- Exit signs have LED lamps


## Power Factor Correction

According to the specifications, the power factor used for compact fluorescent lamps shall be 0.90 at minimum. The other fixture types did not have a specified constraint for power factor, therefore we will assume that the minimum power factor for all sources was 0.90 for this study.

There was no power factor correction applied within the building.

## Important Design Requirements

The specialty high school has many power-sensitive loads such as certain electronic equipment (computers), communication equipment, and controls that need to be isolated from other equipment and special consideration must be given to reducing transients on their circuits. As a part of this protection, all control panels have a double neutral isolated ground. Transient voltage surge suppressors are also used to reduce transients produced by motors, fluorescent lighting and other types of sources in order to protect the powersensitive loads.

## Primary Lamps and Ballast

| General Ballast Properties |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Type | Ballast Factor | Maximum Current Crest Factor | THD | Minimum <br> Power <br> Factor | Frequency | Starting Temperature | Sound Rating | Other |
| Electronic Ballast for Linear Fluorescent T8 Lamps | Between 0.90 and 1.00 | 1.7 | < 20\% | 0.90 | 20 kHz or higher | $0^{\circ} \mathrm{F}$ | A | -- |
| Electronic <br> Ballast for <br> Compact <br> Fluorescent Lamps | Between 0.90 and 1.00 | 1.7 | < 20\% | 0.90 | 20 kHz or higher | $0^{\circ} \mathrm{F}$ | A | -- |
| Pulse Start Metal Halide Lamp Ballast | Between 0.90 and 1.00 | -- | -- | 0.90 | 60 Hz | $-22^{\circ} \mathrm{F}$ min (Normal Ambient Operating Temp of $104^{\circ} \mathrm{F}$ ) | -- | Auxillary, instant-on, quartz system |
| High <br> Pressure <br> Sodium <br> Ballast | Between 0.90 and 1.00 | -- | -- | 0.90 | 60 Hz | $22^{\circ} \mathrm{F}$ min (Normal Ambient Operating Temp of $104^{\circ} \mathrm{F}$ ) | -- | Solid-state Instant restrike device |

All electronic ballasts are on the CL\&P (Power Company, Connecticut Light and Power) list of approved ballasts.

Cherise Rollins
Lighting/Electrical Option
The Learning Corridor, Hartford, CT
Faculty Consultant: Dr.Mistrick
Submission Date: October 29, 2003

| General Lamp Properties |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Type | CCT | CRI <br> minimum | Average Life | Wattage |
| Linear Fluorescent Lamps | 3500 K | 85 | 20,000 hrs | 32W |
| Compact Fluorescent Lamps | 3500 K | 85 | 10,000 hrs | Varies depending on fixture |
| Metal Halide Lamps -Above 150W -150W and below | $\begin{aligned} & 3600 \mathrm{~K} \\ & 3200 \mathrm{~K} \end{aligned}$ | $\begin{aligned} & 70 \\ & 80 \end{aligned}$ | $\begin{aligned} & 10,000 \mathrm{hrs} \\ & 10,000 \mathrm{hrs} \end{aligned}$ | Varies depending on fixture |
| Halogen Lamps | -- | 100 | 2,000 hrs | Varies depending on fixture |

Halogen Lamps are to be "IR" lamps by Sylvania or G.E.

Cherise Rollins
Lighting/Electrical Option
The Learning Corridor, Hartford, CT
Faculty Consultant: Dr.Mistrick
Submission Date: October 29, 2003

## Major Mechanical Equipment

The electrical load of the major mechanical equipment is summarized in the table below:

| Mechanical Equipment Properties |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Equipment Designation | Description | Location | Voltage | Ph | Hz | HP | RPM | Load (KVA) |
| AHU-1 | Air Handling Unit 1 | Mezzanine Mechanical Room | 208 | 3 | 60 | 15.0 | 1750 | 16.5 |
| AHU-2 | Air Handling Unit 2 | Mezzanine Mechanical Room | 208 | 3 | 60 | 7.5 | 1750 | 8.7 |
| AHU-3 | Air Handling Unit 3 | Mezzanine Mechanical Room | 208 | 3 | 60 | 30.0 | 1750 | 33.0 |
| RTAH-4 | Roof Top Air Handling Unit 4 | Roof East | 208 | 3 | 60 | 25.0 | 1750 | 50.4 |
| RTAH-5 | Roof Top Air Handling Unit 5 | Roof East | 208 | 3 | 60 | 20.0 | 1750 | 31.5 |
| RTAH-6 | Roof Top Air Handling Unit 6 | Roof East | 208 | 3 | 60 | 7.5 | 1750 | 15.4 |
| EF-18 | Exhaust Fan 18 | Mezzanine Mechanical Room | 208 | 3 | 60 | 0.25 | 1750 | 0.7 |
| EF-19 | Exhaust Fan 19 | Mezzanine Mechanical Room | 208 | 3 | 60 | 0.25 | 1750 | 0.7 |
| RF-1 | Return Fan 1 | Mezzanine Mechanical Room | 208 | 3 | 60 | 6.3 | 1750 | 5 |
| RF-2 | Return Fan 2 | Mezzanine Mechanical Room | 208 | 3 | 60 | 3.9 | 1750 | 3 |
| RF-3 | Return Fan 3 | Mezzanine Mechanical Room | 208 | 3 | 60 | 8.7 | 1750 | 7.5 |
| REF-10 | Roof Top Exhaust Fan 10 | Roof West | 208 | 3 | 60 | 7.5 | 1750 | 6.3 |
| REF-11 | Roof Top Exhaust Fan 11 | Roof West | 208 | 3 | 60 | 10 | 1750 | 11.6 |
| REF-12 | Roof Top Exhaust Fan 12 | Roof West | 208 | 3 | 60 | 7.5 | 1750 | 9.1 |
| HWP-3 | Hot Water Pump 3 | Mechanical Room | 208 | 3 | 60 | 7.5 | 1750 | 9.1 |
| HWP-4 | Hot Water Pump 4 | Mechanical Room | 208 | 3 | 60 | 7.5 | 1750 | 9.1 |
| CHWP-3 | Chilled Water Pump 3 | Mechanical Room | 208 | 3 | 60 | 10 | 1750 | 11.6 |
| CHWP-4 | Chilled Water Pump 4 | Mechanical Room | 208 | 3 | 60 | 10 | 1750 | 11.6 |
| FFP-1 | Freeze Protection Pump 1 | Mezzanine Mechanical Room | 208 | 3 | 60 | 0.25 | 1750 | 0.7 |
| FFP-2 | Freeze Protection Pump 2 | Mezzanine Mechanical Room | 208 | 3 | 60 | 0.25 | 1750 | 0.7 |
| FFP-3 | Freeze Protection Pump 3 | Mezzanine Mechanical Room | 208 | 3 | 60 | 0.75 | 1750 | 1.2 |
| FFP-4 | Freeze Protection Pump 4 | $2{ }^{\text {nd }}$ Floor East | 208 | 3 | 60 | 0.25 | 1750 | 1.4 |
| FFP-5 | Freeze Protection Pump 5 | $2{ }^{\text {nd }}$ Floor East | 208 | 3 | 60 | 0.25 | 1750 | 1.4 |
| FFP-6 | Freeze Protection Pump 6 | $2^{\text {nd }}$ Floor East | 208 | 3 | 60 | 0.25 | 1750 | 1.4 |

The mechanical load table does not include the following smaller mechanical loads since their contribution to the overall electrical loads are minimal: rooftop exhaust fans $=1 / 3 \mathrm{hp}$, $1 / 4 \mathrm{hp}$, wall exhaust fans $=1 / 10 \mathrm{hp}$, ceiling fans $=75 \mathrm{~W}$, exhaust fans $=1 / 6 \mathrm{hp}, 1 / 2 \mathrm{hp}$, cabinet unit heaters $=1 / 10 \mathrm{hp}$, unit heaters $=1 / 20 \mathrm{hp}, 1 / 30 \mathrm{hp}$.

## Analysis of the Building Load

The following is an analysis of NEC building design loads (according to NEC 2002). The calculations are then compared against the actual sizes for the main building transformer, the main distribution panel, sub panels, and all feeders that leave the main distribution panel. The analysis is first calculated according to the loads on each individual panel, and then for the main distribution panel.

The following demand factors were applied:

| Connected Load |  |
| :--- | :--- |
|  |  |
|  | Demand Factor |
| Receptacles | 1.25 (continuous) |
| Resistance Heat | 1 (for 1st 10 KVA); 0.5 (for $>10$ KVA) |
| Air Conditioning | 0 since a/c load is greater than the heat load |
| Motors | 1 |
| Largest Motor | 1 |
| Other Loads | 0.5 |
| Water Heating | 1 |
| Spare Capacity | 1 |

## Panel LP1E: Lighting Panel 1 East

Lighting Load $=8.4 \mathrm{KVA}$
Lighting Demand Factor $=1.25$ (continuous loading)
Total Lighting Load $=1.25$ * $8.4=10.5 \mathrm{KVA}$
Total Current $(\mathrm{I})=10.5 \mathrm{KVA} /\left(3^{\wedge} .5^{*} .208 \mathrm{KV}\right)=29.15 \mathrm{~A}$
I $=29.15$ A < 100 A circuit breaker from MDP and 100 A rated panel, OK
Panel LP2E: Lighting Panel 2 East
Lighting Load $=17.67$ KVALighting Demand Factor = 1.25 (continuous loading)

$$
\text { Total Lighting Load }=1.25 * 17.67=22.09 \mathrm{KVA}
$$

$$
\text { Total Current }(I)=22.09 \mathrm{KVA} /\left(3^{\wedge} .5^{*} .208 \mathrm{KV}\right)=61.32 \mathrm{~A}
$$

$$
\text { I = 61.32 A < } 100 \text { A circuit breaker from MDP and } 100 \text { A rated panel, OK }
$$

Panel LP3E: Lighting Panel 3 East
Lighting Load $=12.27$ KVALighting Demand Factor $=1.25$ (continuous loading)
Total Lighting Load $=1.25$ * $12.27=15.34 \mathrm{KVA}$
Total Current $(\mathrm{I})=15.34 \mathrm{KVA} /\left(3^{\wedge} .5^{*} .208 \mathrm{KV}\right)=42.58 \mathrm{~A}$
$\mathrm{I}=42.58 \mathrm{~A}<100 \mathrm{~A}$ circuit breaker from MDP and 100 A rated panel, OK
Panel LP4E: Lighting Panel 4 East
Lighting Load $=27.85 \mathrm{KVA}$
Lighting Demand Factor = 1.25 (continuous loading)
Total Lighting Load $=1.25 * 27.85=34.81 \mathrm{KVA}$Total Current $(\mathrm{I})=34.81 \mathrm{KVA} /\left(3^{\wedge} .5^{*} .208 \mathrm{KV}\right)=96.62 \mathrm{~A}$
I = 96.62 A < 100 A circuit breaker from MDP and 100 A rated panel, OK
Panel LP1W: Lighting Panel 1 West
Lighting Load $=12.7 \mathrm{KVA}$Lighting Demand Factor $=1.25$ (continuous loading)
Total Lighting Load $=1.25$ * $12.7=15.88$ KVA
Total Current $(\mathrm{I})=15.88 \mathrm{KVA} /\left(3^{\wedge} .5^{*} .208 \mathrm{KV}\right)=44.08 \mathrm{~A}$
$I=44.08 \mathrm{~A}<100 \mathrm{~A}$ circuit breaker from MDP and 100 A rated panel, OK

## Panel LP2W: Lighting Panel 2 West

$$
\text { Lighting Load }=\quad 21.1 \text { KVA }
$$

Lighting Demand Factor $=1.25$ (continuous loading)
Total Lighting Load $=1.25 * 21.1=26.38 \mathrm{KVA}$
Total Current $(\mathrm{I})=26.38 \mathrm{KVA} /\left(3^{\wedge} .5^{*} .208 \mathrm{KV}\right)=73.22 \mathrm{~A}$
I = 73.22 A < 100 A circuit breaker from MDP and 100 A rated panel, OK

Panel PP1E: Power Panel 1 East

Number of receptacles $=122$
Receptacle load $=180$ VA * $122=21960 \mathrm{VA}$
Receptacle Demand Factor for first 10 KVA $=1.0$
Receptacle Demand Factor for $>10 \mathrm{KVA}=0.5$
Total Receptacle Load $=(10 * 1)+(11.96 * 0.5)=15.98$ KVA
Total Other Loads $=17$ KVA Panel 'PP3E'
+14 KVA Kiln
31 KVA (Demand Factor = 1)
Total Panel Load $=15.98+31=46.98 \mathrm{KVA}$
Total Current $(\mathrm{I})=46.98 \mathrm{KVA} /\left(3^{\wedge} .5\right.$ * .208 KV$)=130.4 \mathrm{~A}$
I = 130.4 A < 225 A circuit breaker from MDP and 225 A rated panel, OK

## Panel PP2E: Power Panel 2 East

Number of receptacles $=51$
Receptacle load $=180 \mathrm{VA} * 51=9180 \mathrm{VA}$
Receptacle Demand Factor for first 10 KVA $=1.0$
Receptacle Demand Factor for $>10 \mathrm{KVA}=0.5$
Total Receptacle Load $=9.18$ * $1=9.18$ KVA
Total Motors and Other Loads $=9.5 \mathrm{KVA}$
Demand Factor = 1
Largest Motor $=2.5 \mathrm{KVA}$
Demand Factor $=0.25$

$$
\text { Total Largest Motor }=0.25 * 2.5=0.63 \mathrm{KVA}
$$

$$
\text { Total Panel Load }=9.18+9.5+0.63=19.31 \mathrm{KVA}
$$

$$
\text { Total Current }(I)=19.31 \mathrm{KVA} /\left(3^{\wedge} .5^{*} .208 \mathrm{KV}\right)=53.60 \mathrm{~A}
$$

$$
\text { I = 53.60 A < } 100 \text { A circuit breaker from MDP and } 100 \text { A rated panel, OK }
$$

```
Panel PP3E: Power Panel 3 East
Total Motors and Other Loads = 16.0 KVA
    Demand Factor = 1
Largest Motor = 2.5 KVA
    Demand Factor = 0.25
Total Largest Motor =0.25*2.5 = 0.63 KVA
Total Panel Load = 16.0 + 0.63=16.63 KVA
Total Current (I) = 16.63 KVA/(3^.5 *.208 KV) = 46.16 A
I = 46.16 A < 60 A circuit breaker from Panel 'PP1E' and 60 A rated panel, OK
```


## Panel PP1W: Power Panel 1 West

Number of receptacles $=47$
Receptacle load $=180 \mathrm{VA} * 47=8460 \mathrm{VA}$
Receptacle Demand Factor for first 10 KVA $=1.0$
Receptacle Demand Factor for $>10 \mathrm{KVA}=0.5$
Total Receptacle Load $=8.46$ * $1=8.46$ KVA
Total Motors and Other Loads $=20.0 \mathrm{KVA}$
Demand Factor = 1
Largest Motor $=2.5 \mathrm{KVA}$
Demand Factor $=0.25$
Total Largest Motor $=0.25 * 2.5=0.63 \mathrm{KVA}$
Total Panel Load $=8.46+20.0+0.63=29.09$ KVA
Total Current $(\mathrm{I})=29.09 \mathrm{KVA} /\left(3^{\wedge} .5^{*} .208 \mathrm{KV}\right)=80.7 \mathrm{~A}$
I = 80.7 A < 100 A circuit breaker from MDP and 100 A rated panel, OK

```
Panel PP2W: Power Panel 2 West
Number of receptacles = 96
Receptacle load = 180 VA * 96 = 17280 VA
    Receptacle Demand Factor for first 10 KVA = 1.0
    Receptacle Demand Factor for > 10KVA = 0.5
Total Receptacle Load = (10 * 1) + (7.28 * 0.5) = 13.64 KVA
Total Other Loads = 1.0 KVA
    Demand Factor = 1
Total Panel Load = 13.64 + 1.0 = 14.64 KVA
Total Current (I) = 14.64 KVA/(3^.5 *.208 KV ) = 40.64 A
I = 40.64 A < 100 A circuit breaker from MDP and 100 A rated panel, OK
```

Panel PP3W: Power Panel 3 West
Number of receptacles $=100$
Receptacle load $=180$ VA * $100=18000$ VA
Receptacle Demand Factor for first 10 KVA $=1.0$
Receptacle Demand Factor for $>10 \mathrm{KVA}=0.5$
Total Receptacle Load $=(10 * 1)+(8 * 0.5)=14.0$ KVA
Total Motors and Other Loads $=7.9 \mathrm{KVA}$
Demand Factor = 1
Largest Motor $=2.0 \mathrm{KVA}$
Demand Factor $=0.25$
Total Largest Motor $=0.25 * 2.0=0.5 \mathrm{KVA}$
Total Panel Load $=14.0+7.9+0.5=22.4$ KVA
Total Current $(\mathrm{I})=22.4 \mathrm{KVA} /\left(3^{\wedge} .5^{*} .208 \mathrm{KV}\right)=62.18 \mathrm{~A}$
I = 62.18 A < 100 A circuit breaker from MDP and 100 A rated panel, OK

Cherise Rollins
Lighting/Electrical Option
The Learning Corridor, Hartford, CT
Faculty Consultant: Dr.Mistrick
Submission Date: October 29, 2003

## Panel PP4W: Power Panel 4 West

Number of receptacles $=168$
Receptacle load $=180$ VA * $168=30240$ VA
Receptacle Demand Factor for first 10 KVA $=1.0$
Receptacle Demand Factor for $>10 \mathrm{KVA}=0.5$
Total Receptacle Load $=(10$ * 1$)+(20.24$ * 0.5$)=20.12$ KVA
Total Other Loads $=21.5 \mathrm{KVA}$
Demand Factor = 1

Total Panel Load $=20.12+21.5=41.62$ KVA
Total Current $(\mathrm{I})=41.62 \mathrm{KVA} /\left(3^{\wedge} .5^{*} .208 \mathrm{KV}\right)=115.53 \mathrm{~A}$
I = 115.53 A < 225 A circuit breaker from MDP and 225 A rated panel, OK

## Panel PP5W: Power Panel 5 West

Number of receptacles $=19$
Receptacle load $=180$ VA * $19=3420 \mathrm{VA}$
Receptacle Demand Factor for first 10 KVA $=1.0$
Receptacle Demand Factor for $>10 \mathrm{KVA}=0.5$
Total Receptacle Load $=3.42$ * $1=3.42 \mathrm{KVA}$
Total Other Loads $=13.8 \mathrm{KVA}$
Demand Factor = 1
Total Panel Load $=3.42+13.8=17.22 \mathrm{KVA}$
Total Current $(I)=17.22 \mathrm{KVA} /\left(3^{\wedge} .5\right.$ * .208 KV$)=35.51 \mathrm{~A}$
I = 35.51 A < 100 A circuit breaker from MDP and 100 A rated panel, OK

```
Panel PP6W: Power Panel 6 West
    Total Motors and Other Loads = 28.4 KVA
    Demand Factor = 1
    Largest Motor = 11.6 KVA
    Demand Factor = 0.25
    Total Largest Motor =0.25 * 11.6 = 2.9 KVA
    Total Panel Load = 11.6 + 2.9 = 14.5 KVA
    Total Current (I) = 14.5 KVA/(3^.5 * . 208 KV) = 40.25 A
    I=40.25 A < 100 A circuit breaker from MDP and 100 A rated panel, OK
```


## Panel CP1E: Control Panel 1 East

Number of receptacles $=142$
Receptacle load $=180$ VA * $142=25560$ VA
Receptacle Demand Factor for first 10 KVA $=1.0$
Receptacle Demand Factor for $>10 \mathrm{KVA}=0.5$
Total Receptacle Load $=(10$ * 1$)+(15.56 * 0.5)=17.78$ KVA
Total Current $(\mathrm{I})=17.78 \mathrm{KVA} /\left(3^{\wedge} .5^{*} .208 \mathrm{KV}\right)=49.35 \mathrm{~A}$
I $=49.35 \mathrm{~A}<100 \mathrm{~A}$ circuit breaker from MDP and 100 A rated panel, OK

## Panel CP2E: Control Panel 2 East

Number of receptacles = 95
Receptacle load $=180$ VA * $95=17100$ VA
Receptacle Demand Factor for first 10 KVA $=1.0$
Receptacle Demand Factor for $>10 \mathrm{KVA}=0.5$
Total Receptacle Load $=(10 * 1)+(7.1 * 0.5)=13.55 \mathrm{KVA}$
Total Current $(\mathrm{I})=13.55 \mathrm{KVA} /\left(3^{\wedge} .5{ }^{*} .208 \mathrm{KV}\right)=37.61 \mathrm{~A}$
I = 37.61 A < 100 A circuit breaker from MDP and 100 A rated panel, OK

> Panel CP1W: Control Panel 1 West
> Number of receptacles $=83$
> Receptacle load $=180$ VA * $83=14940 \mathrm{VA}$
> Receptacle Demand Factor for first $10 \mathrm{KVA}=1.0$
> Receptacle Demand Factor for $>10 \mathrm{KVA}=0.5$
> Total Receptacle Load $=(10 * 1)+(4.94 * 0.5)=12.47 \mathrm{KVA}$
> Total Current $(\mathrm{I})=12.47 \mathrm{KVA} /\left(3^{\wedge} .5 * .208 \mathrm{KV}\right)=34.61 \mathrm{~A}$
> I $=34.61 \mathrm{~A}<100 \mathrm{~A}$ circuit breaker from MDP and 100 A rated panel, OK

## Panel CP2W: Control Panel 2 West

Number of receptacles $=59$
Receptacle load $=180$ VA * $59=10620$ VA
Receptacle Demand Factor for first $10 \mathrm{KVA}=1.0$
Receptacle Demand Factor for $>10 \mathrm{KVA}=0.5$
Total Receptacle Load $=(10 * 1)+(0.62 * 0.5)=10.31 \mathrm{KVA}$
Total Current $(\mathrm{I})=10.31 \mathrm{KVA} /\left(3^{\wedge} .5^{*} .208 \mathrm{KV}\right)=28.62 \mathrm{~A}$
I = 28.62 A < 100 A circuit breaker from MDP and 100 A rated panel, OK

Panel CP3W: Control Panel 3 West
Number of receptacles $=124$
Receptacle load = 180 VA * $124=22320$ VA
Receptacle Demand Factor for first 10 KVA $=1.0$
Receptacle Demand Factor for $>10 \mathrm{KVA}=0.5$
Total Receptacle Load $=(10$ * 1$)+(12.32$ * 0.5$)=16.16$ KVA
Total Current $(I)=16.16 \mathrm{KVA} /\left(3^{\wedge} .5^{*} .208 \mathrm{KV}\right)=44.86 \mathrm{~A}$
$\mathrm{I}=44.86 \mathrm{~A}<100 \mathrm{~A}$ circuit breaker from MDP and 100 A rated panel, OK

## Panel CP4W: Control Panel 4 West

Number of receptacles $=155$
Receptacle load $=180$ VA * $155=27900$ VA
Receptacle Demand Factor for first 10 KVA $=1.0$
Receptacle Demand Factor for $>10 \mathrm{KVA}=0.5$
Total Receptacle Load $=(10$ * 1$)+(17.9 * 0.5)=18.95$ KVA
Total Current $(\mathrm{I})=18.95 \mathrm{KVA} /\left(3^{\wedge} .5^{*} .208 \mathrm{KV}\right)=52.6 \mathrm{~A}$
I = 52.6 A < 100 A circuit breaker from MDP and 100 A rated panel, OK

## Panel CP5W: Control Panel 5 West

Number of receptacles $=129$
Receptacle load $=180$ VA * $129=23220$ VA
Receptacle Demand Factor for first $10 \mathrm{KVA}=1.0$
Receptacle Demand Factor for $>10 \mathrm{KVA}=0.5$
Total Receptacle Load $=(10 * 1)+(13.22 * 0.5)=16.61$ KVA
Total Current $(I)=16.61 \mathrm{KVA} /\left(3^{\wedge} .5\right.$ *. 208 KV$)=46.1 \mathrm{~A}$
I = 46.1 A < 100 A circuit breaker from MDP and 100 A rated panel, OK

```
Panel MP: Mechanical Panel 1
Lighting Load = 0.75 KVA
    Lighting Demand Factor = 1.25 (continuous loading)
Total Lighting Load = 1.25* 0.75 = 0.9375 KVA
Number of receptacles = 20
Receptacle load = 180 VA * 20 = 3600 VA
    Receptacle Demand Factor for first 10 KVA = 1.0
    Receptacle Demand Factor for > 10KVA = 0.5
Total Receptacle Load = 3.6 * 1 = 3.6 KVA
Total Motors and Other Loads = 23.2 KVA
    Resistance Heat Load = 26.5 KVA (Demand Factor = 0)
    Air Conditioning Load = 23.2 KVA (Demand Factor = 1)
```

$$
\begin{aligned}
& \text { Largest Motor }=11.6 \mathrm{KVA} \\
& \text { Demand Factor }=0.25 \\
& \text { Total Largest Motor }=0.25 * 11.6=2.9 \mathrm{KVA} \\
& \text { Total Panel Load }=0.9375+3.6+23.2+2.9=30.64 \mathrm{KVA} \\
& \text { Total Current }(\mathrm{I})=30.64 \mathrm{KVA} /\left(3^{\wedge} .5 * .208 \mathrm{KV}\right)=85.04 \mathrm{~A} \\
& \mathrm{I}=85.04 \mathrm{~A}<225 \mathrm{~A} \text { circuit breaker from MDP and } 225 \mathrm{~A} \text { rated panel, OK }
\end{aligned}
$$

## Panel MP2: Mechanical Panel 2

$$
\begin{aligned}
& \text { Total Motors and Other Loads = 49.3 KVA } \\
& \text { Resistance Heat Load }=23.17 \mathrm{KVA} \\
& \text { Air Conditioning Load }=26.13 \mathrm{KVA} \\
& \\
& \text { (Demand Factor }=0) \\
& \text { Largest Motor }=16.5 \mathrm{KVA} \\
& \text { Demand Factor }=0.25 \\
& \text { Total Largest Motor }=0.25 * 16.5=4.13 \mathrm{KVA} \\
& \text { Total Panel Load }=26.13+4.13=30.26 \mathrm{KVA} \\
& \text { Total Current }(\mathrm{I})=30.26 \mathrm{KVA}\left(3^{\wedge} .5 * .208 \mathrm{KV}\right)=84.0 \mathrm{~A} \\
& \mathrm{I}=84.0 \mathrm{~A}<225 \mathrm{~A} \text { circuit breaker from MDP and } 225 \mathrm{~A} \text { rated panel, OK }
\end{aligned}
$$

Panel MP3: Mechanical Panel 3

$$
\begin{array}{ll}
\text { Total Motors and Other Loads }=97.3 \text { KVA } \\
\text { Resistance Heat Load }=46.71 \text { KVA } & \text { (Demand Factor }=0) \\
\text { Air Conditioning Load }=50.59 \text { KVA } & \text { (Demand Factor }=1)
\end{array}
$$

Largest Motor = 22.4 KVA

$$
\text { Demand Factor }=0.25
$$

$$
\text { Total Largest Motor }=0.25 \text { * } 22.4=5.6 \text { KVA }
$$

$$
\text { Total Panel Load }=50.59+5.6=56.19 \text { KVA }
$$

$$
\text { Total Current }(\mathrm{I})=56.19 \mathrm{KVA} /\left(3^{\wedge} .5^{*} .208 \mathrm{KV}\right)=156.0 \mathrm{~A}
$$

$$
\text { I = 156.0 A < } 400 \mathrm{~A} \text { circuit breaker from MDP and } 400 \mathrm{~A} \text { rated panel, OK }
$$

| NEC Total Load Calculations |  |  |
| :---: | :---: | :---: |
| Panel | Total Load (KVA) | Total Current (A) |
| LP1E | 10.50 | 29.15 |
| LP2E | 22.09 | 61.32 |
| LP3E | 15.34 | 42.58 |
| LP4E | 34.81 | 96.62 |
| LP1W | 15.88 | 44.08 |
| LP2W | 26.38 | 73.22 |
| PP1E | 46.98 | 130.40 |
| PP2E | 19.31 | 53.60 |
| PP3E | [16.63] Fed from PP1E | [46.16] Fed from PP1E |
| PP1W | 29.09 | 80.70 |
| PP2W | 14.64 | 40.64 |
| PP3W | 22.40 | 62.18 |
| PP4W | 41.62 | 115.53 |
| PP5W | 17.22 | 35.51 |
| PP6W | 14.50 | 40.25 |
| CP1E | 17.78 | 49.35 |
| CP2E | 13.55 | 37.61 |
| CP1W | 12.47 | 34.61 |
| CP2W | 10.31 | 28.62 |
| CP3W | 16.16 | 44.86 |
| CP4W | 18.95 | 52.6 |
| CP5W | 16.61 | 46.1 |
| MP | 30.64 | 85.04 |
| MP2 | 30.26 | 84.0 |
| MP3 | 56.19 | 156.0 |
|  |  |  |
| TOTALS | 553.68 | 1524.57 |

Total Capacity $=$ 553.68 KVA calculated $=1536.86$ A distributed by MDP $\left(3^{\wedge} .5\right)$ * $(0.208)$

The Main Switchboard (MDP) is rated for 1200A < 1536 calculated.
Therefore the MDP is insufficient for the given system. A 1200A MDP for a building of this size and with these types of loads seems to be too small. There might be an error on the drawings in terms of the size of the MDP. The electrical designer will be contacted to verify sizes of the major loads and the MDP and the
updated information will be available in resubmission. A panel of 2000 A seems more appropriate for a school building of this size. If a 2000A main switchboard is used, the available KVA on the $208 \mathrm{~V} / 120$ system is:

2000 A * $\left(3^{\wedge} 0.5\right)$ * $0.208 \mathrm{KV} * 0.80(80 \%$ maximum capacity design factor) $=$ 576.43 KVA which is greater than the 553.68 KV needed for the building loads.

Also, another issue might be that the actual loads for the building are well under those initially established by the panel boards on the drawings. If this is the case, the 1200A main circuit breaker may be sufficient for the building. These loads will be verified by the data received by the utility power company (please see below).

## Utility Rate Structure

The electrical designer was contacted and all utility information from the MEP company is not available, but it was noted that the building is on a grid system and that the proper electrical power at the building is supplied by CL\&P (Connecticut Light and Power). The power company was contacted and permission is needed from the owner to release any utility rate structure data for the building. The owner is currently working with the power company to obtain a summary of the electric utility load data for the previous 12 months and resubmission of this report will include this data when it becomes available. All necessary updates to load sizes will be made and incorporated into the report as soon as possible.


