

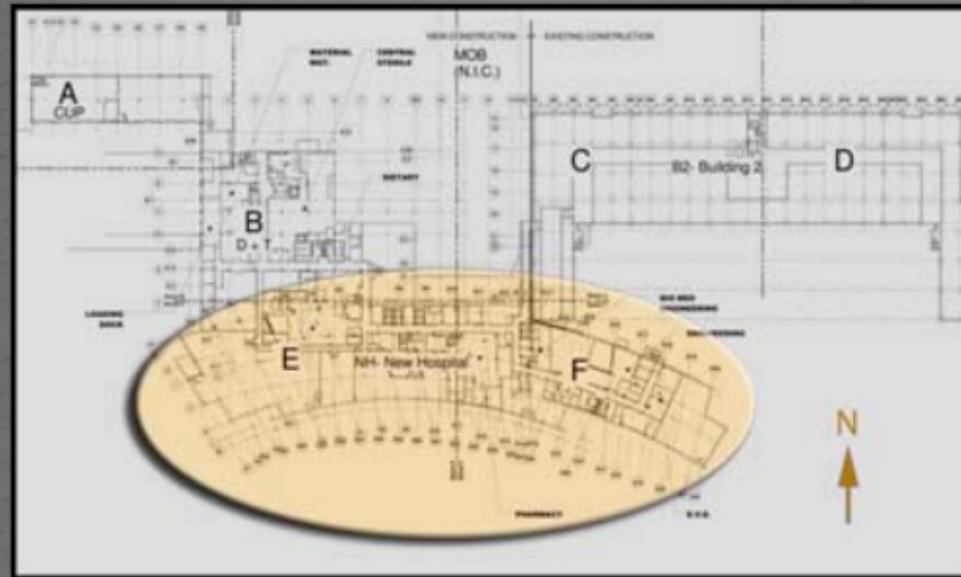
2010 AE Senior Thesis

University Medical Center at Princeton

Presented by: Stephen Perkins
5th year Structural Option
BAE/MAE

Advised by: Dr. Linda Hanagan





- UMCP consists of three separate facilities
 - Central Utility plant
 - D&T Building
 - New Hospital
- Focus of this thesis is limited to New Hospital
- Building Statistics

Size: 400,000 sq.ft.
Height: 91'-0" above grade
Design height = 147'-0"
(Future 4 story addition)
Stories: 6 stories + 1 level below grade
Typical story height = 14'-0"
Construction start: May 2009
Construction end: January 2012
Overall cost (NH): ~\$115 million
Delivery method: Design-Bid-Build

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Structural

- Gravity system
 - Composite beam floor system
 - 3-1/4" LWC over 3", 20 Ga. composite metal deck
 - 3/4" shear studs, ASTM 108
 - Typical bay size: 30'-0" x 30'-0"; 30'-0" x 18'-0"
 - Typical sizes: W14 columns
W12-W27 beams/girders
- Lateral system
 - 18 braced frames (9 in each wing)
 - HSS shapes for diagonals
 - Each frame has unique brace configuration
 - 4 moment frames
 - Along north and south facades
 - PR moment connections
- Foundation
 - Primarily spread footings w/ mat foundations in certain areas
 - Tension-only mini piles attached to braced frame footings
 - Extend into bedrock found 8'-30' below ground level



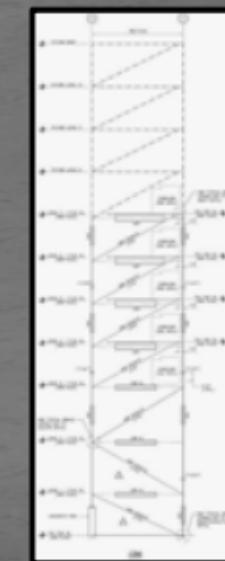
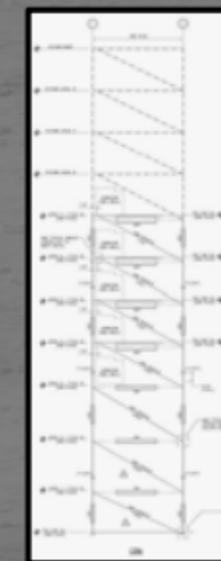
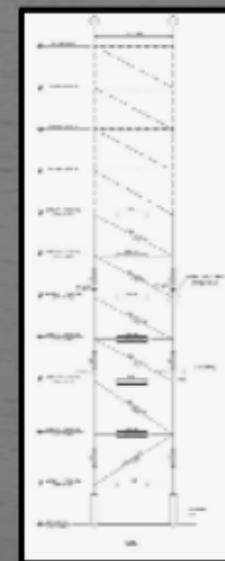
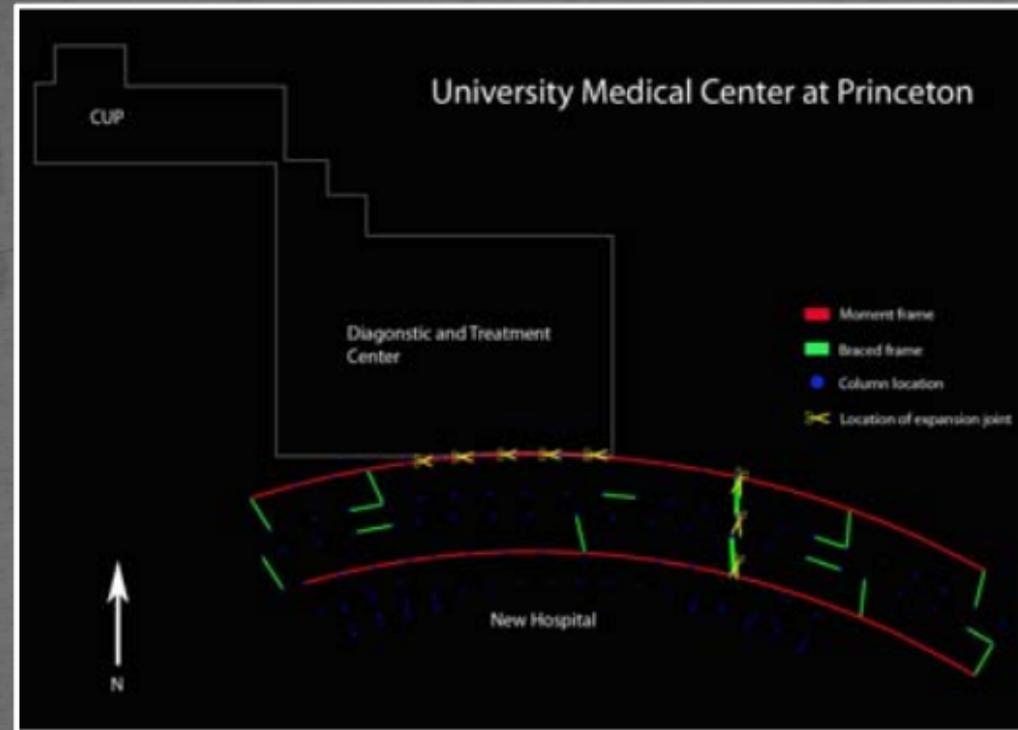
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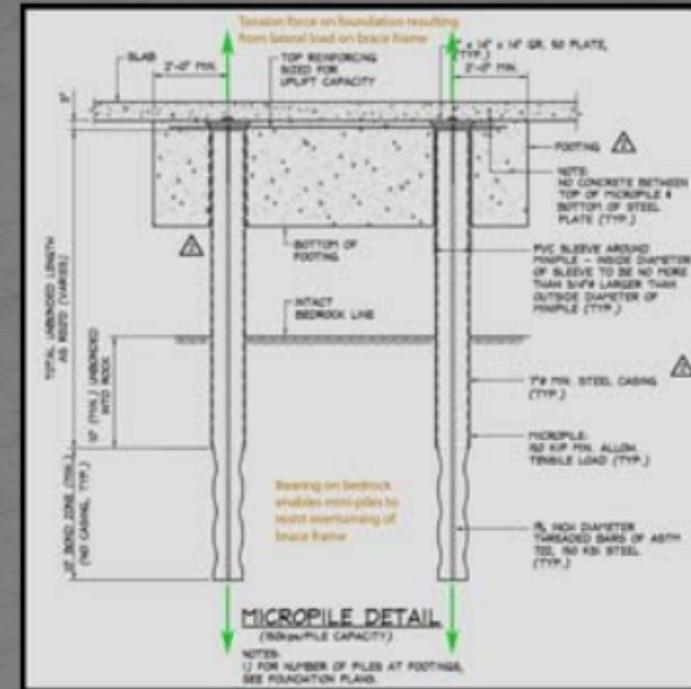
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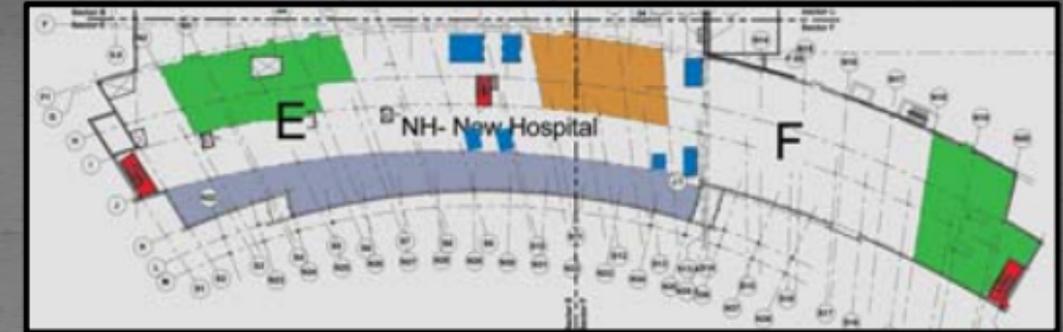
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Architectural

- Curtain wall on south façade is prominent architectural feature
 - 92'-0" tall
 - Insulated glass with low-e coating
 - Glass is tinted at floor levels to hide structure
 - Provides great deal of daylight in patient rooms
- 1st floor is mainly public space
 - Café
 - Lobbies
 - Sensitive equipment areas
- Floors above 2nd floor are private patient areas
 - Rooms located along north and south facades
 - Nurse stations, offices, corridors in middle



1st Floor Plan



Typical Floor Plan

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Goal #1

Eliminate net tension at the foundation level

- No longer would need tension only mini-piles underneath spread footings

Goal #2

Improve vibration performance of floor system

- Meet standards established for sensitive equipment

Design Solution

Redesign the structural system in concrete!

- Would increase compressive force enough to overcome tension from lateral loads
- Concrete floor systems tend to perform better under vibration than steel floor systems

Presentation Outline

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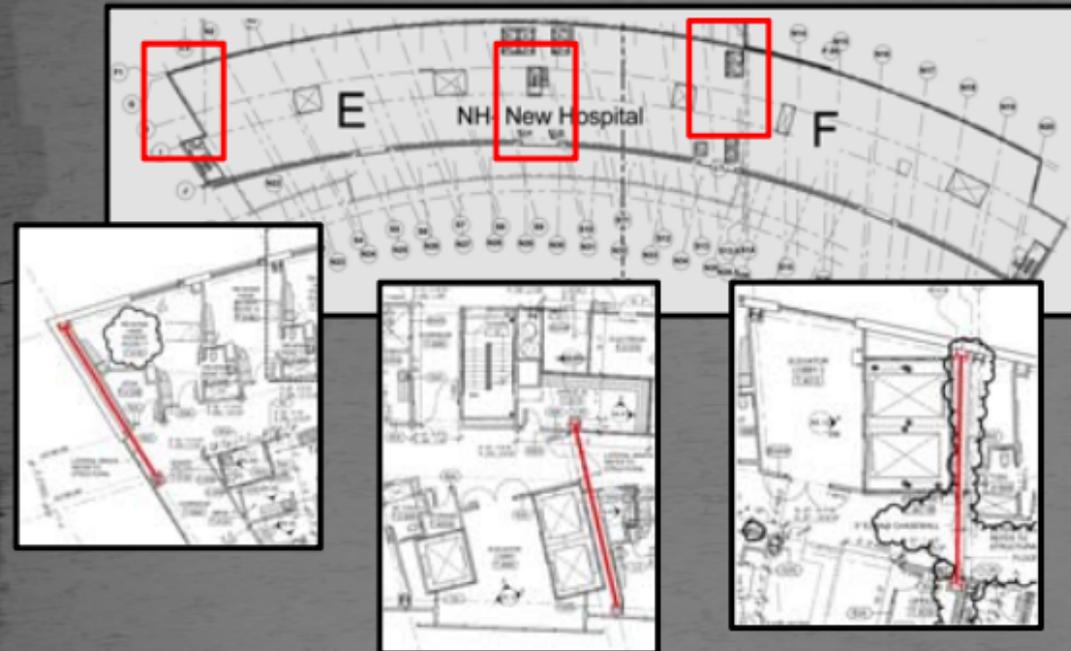
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Structural considerations...

- Redesign of lateral system → Shear walls, moment frames
- Redesign slab → Two-way flat slab
- Redesign columns → Use same column grid (no floor plan disruption)
- Redesign beams → Only on exterior to support curtain wall; included in moment frames
- Redesign foundation → Spread and continuous footings; mat foundation assumed where necessary

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Architectural considerations....

- Floor plan adjustments → Careful shear wall placement
- Curtain wall interaction with structure → Breadth topic



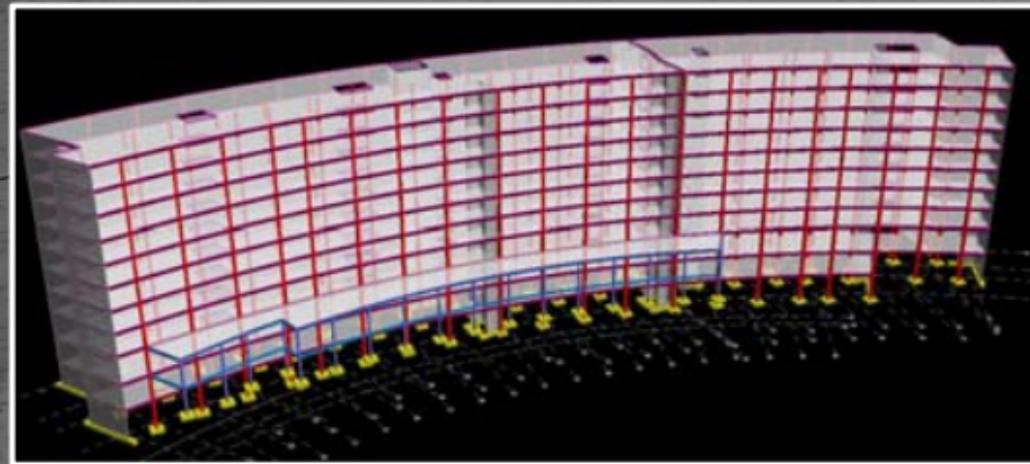
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Construction Management considerations...

- Changes to project cost → Breadth topic
- Changes to project schedule → Breadth topic

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Initial Assumptions

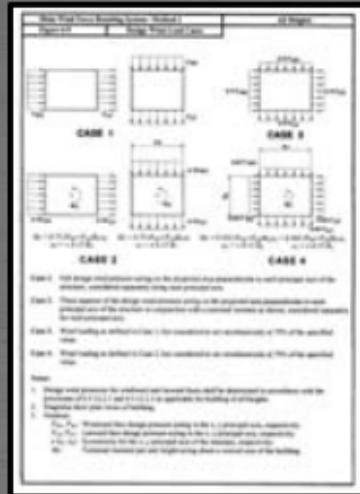
- Expansion joint modeled
- Hospital designed as 10-story building

Modeling Assumptions

- Slab acts as rigid diaphragm
 - Columns braced against side sway by shear walls and slab
 - Moment frame beams modeled as fixed in order to transfer moment across the frame
 - Rigid end zones applied with 50% reduction
 - P- Δ effects considered within model
 - Shear walls have no stiffness out-of-plane
 - Modified moment of inertia...
 - Columns: $0.70I_g$
 - Beams: $0.35I_g$
 - Walls: $0.35I_g$
 - Slab: $0.25I_g$
- (Per ACI 10.10.4.1)

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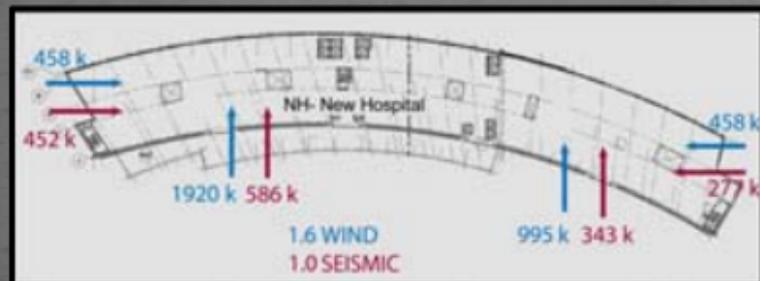
Applied loads

Wind

- Four different load cases to account for variability in wind direction
- These wind cases (8 in total) were calculated by hand and entered manually into RAM model

Seismic

- Fundamental period of both wings exceeded $C_u T_a$. Therefore, $C_u T_a$ was used to determine seismic forces.
- Lateral system defined as special reinforced concrete shear walls
 - $R = 6.0$
 - $C_d = 5.0$
- Building weight and seismic loads were calculated by hand to confirm RAM calculation
 - Base shears within 1.0%



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Natural Frequency

$$f_n = (c * \phi) / a^2$$

where $c = [Eh^3/12(1-\nu^2)] * g/q$

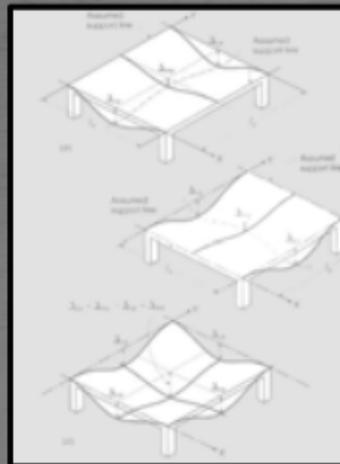
Peak Acceleration

$$a_p/g \leq P_o e^{-0.35f_n} / \beta W$$

Vibration Velocity

$$V = U_v \Delta_p / f_n$$

where $U_v = \pi F_m f_o^2$



$$\Delta_{total} = \Delta_{midA} + \Delta_{colB}$$

Floor Vibration

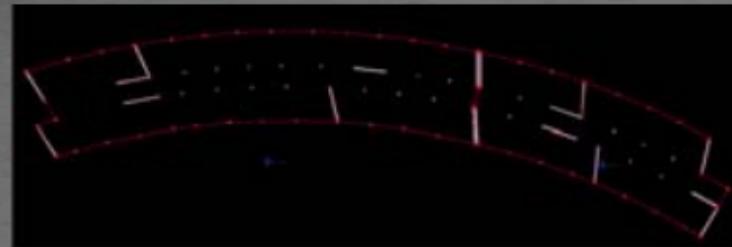
- Initially assumed that slab thickness would be governed by vibration
- Considerations for vibration design:
 1. Source
 2. Transmission path
 3. Floor characteristics
 4. Human sensitivity
 5. Acceptable standards

Vibration Considerations	Description	Value	Units
Source	Walking	2-3	Hz
Transmission path	Mass	W/g	kg·s ² /m
	E	1.25Ec	ksi
Floor Characteristics	Damping	5%	n/a
	Nat. Frequency	f _n	Hz
	Peak Acceleration	a _p /g	n/a
Human Sensitivity	Variable range	4-8	Hz
Acceptable Standards	Humans	0.005	n/a
	Sensitive Equipment	4000	μin/s

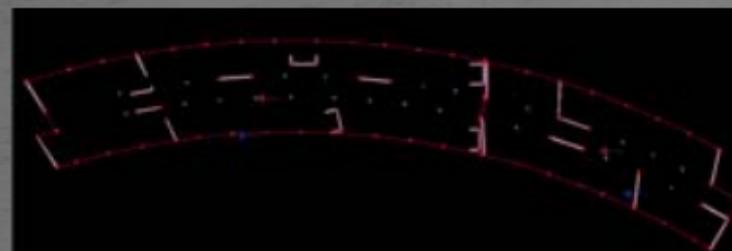
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Lateral System Layout

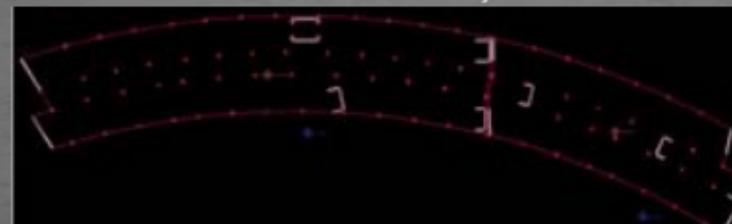
Initial iteration



34th iteration



Final Shear Wall Layout



Trial #34				
Wall f_c	10 ksi			
Wall thickness	24'			
Slab thickness	10'			
Design Periods				
Direction	West		East	
	Period	Mode	Period	Mode
X	1.682	1	1.314	2
Y	1.308	3	0.719	5
Z	0.941	4	0.585	6

Final Iteration				
Wall f_c	8 ksi			
Wall thickness	12'			
Slab thickness	8'			
Design Periods				
Direction	West		East	
	Period	Mode	Period	Mode
X	2.810	2	3.763	1
Y	2.035	3	1.865	4
Z	1.431	5	1.100	6

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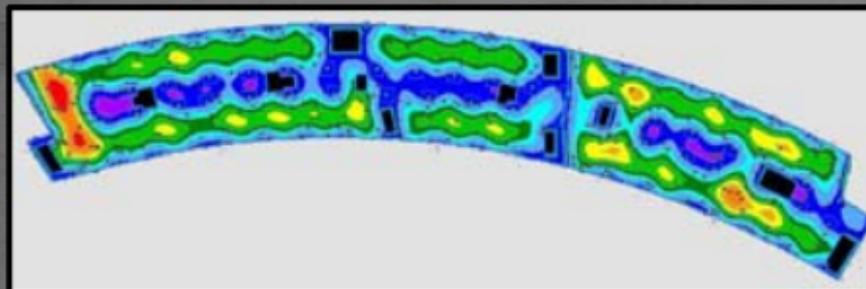
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Check assumed behavior

Slab Deflection



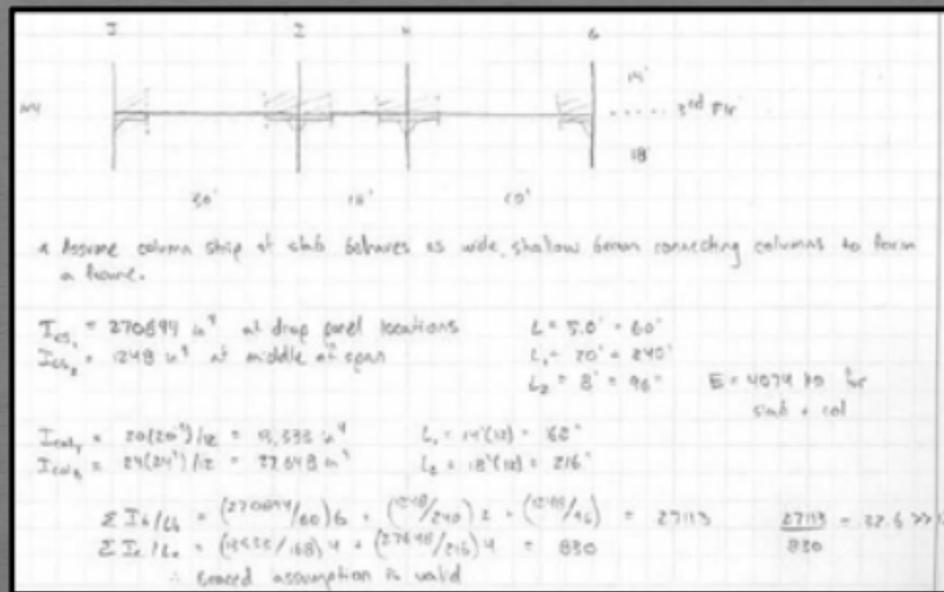
Dead Load Deflection				
Δ_{fcdD}	Δ_{fmidA}	Δ_{max}	$\Delta_{concept}$	% Diff
(in.)				
0.160	0.034	0.194	0.180	7.8

Dead + Live Load Deflection				
Δ_{fcdD}	Δ_{fmidA}	Δ_{max}	$\Delta_{concept}$	% Diff
(in.)				
0.304	0.065	0.369	0.350	5.4

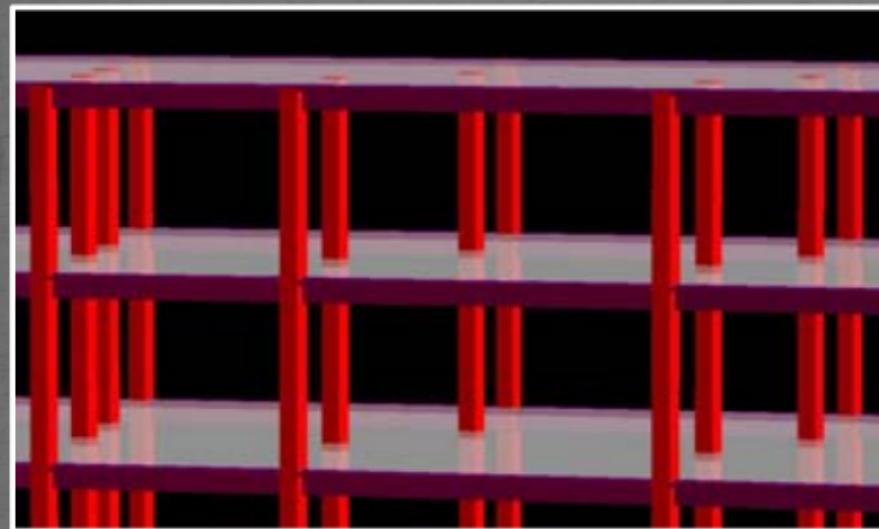
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Check assumed behavior

Non-Sway Columns



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Wall Design

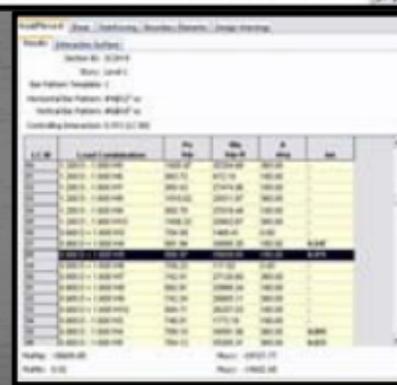
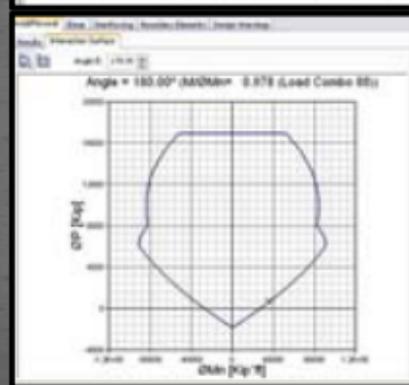
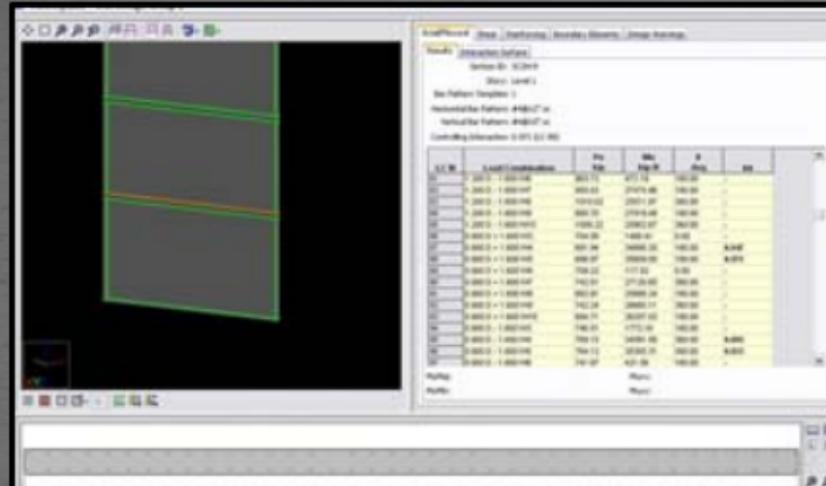
Thickness = 12"

$f'_c = 8$ ksi

Typical reinforcing:

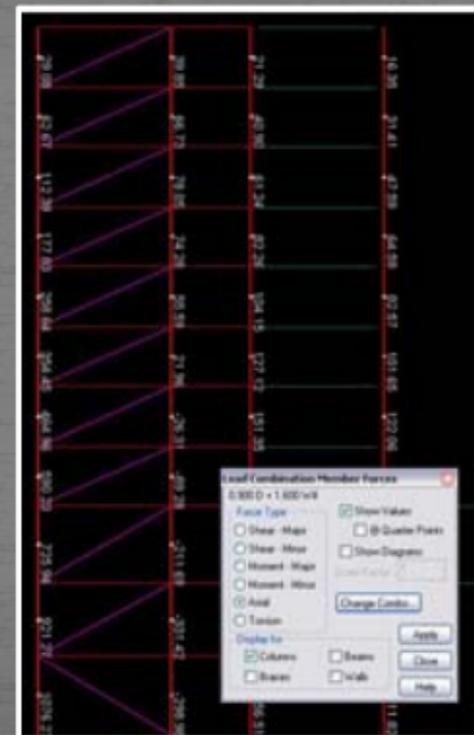
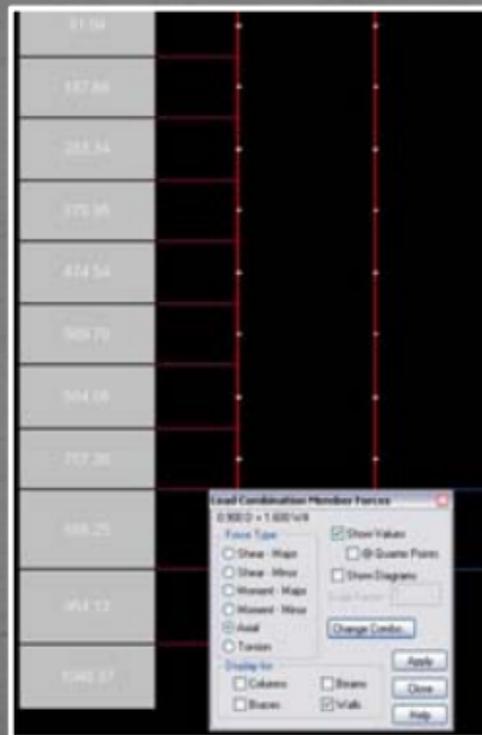
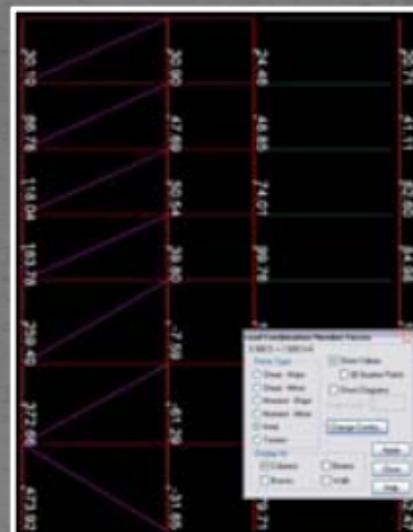
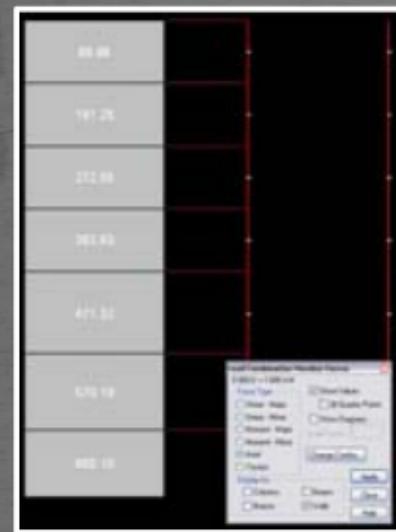
Horizontal- #4 @ 12" o.c.

Vertical- #6 @ 10" o.c.

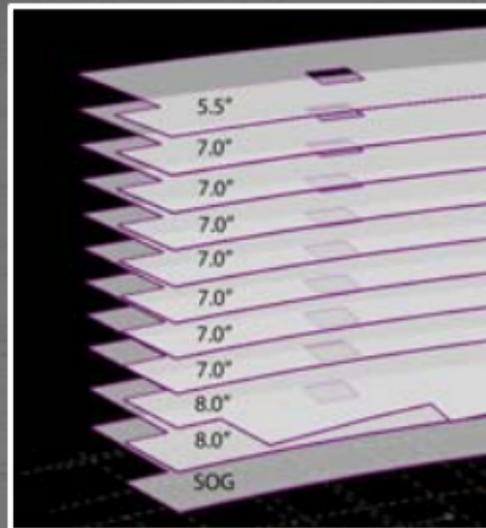


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Slab Design

8" slab

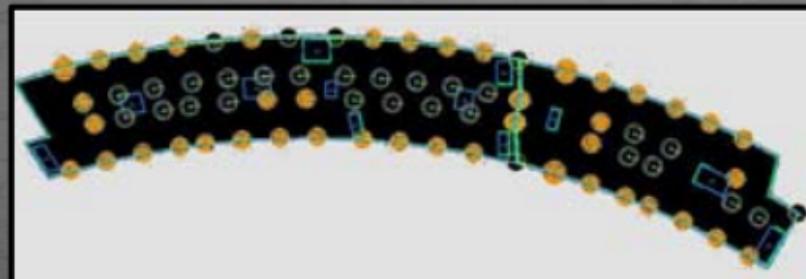
Vibration for Sensitive Equipment				Vibration for Walking	
Velocity	Walking Rate			a_p/g	0.0011
	Fast	Medium	Slow		
V	3991.89	887.09	238.45	4000 operating	0.0025 operating 0.005 offices

7" slab

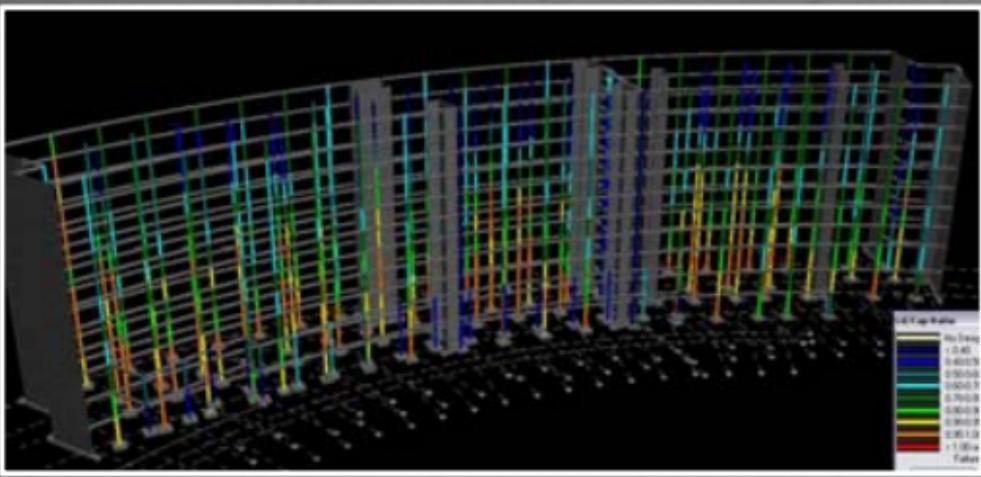
Vibration for Sensitive Equipment				Vibration for Walking	
Velocity	Walking Rate			a_p/g	0.0018
	Fast	Medium	Slow		
V	6706.69	1490.38	400.61	4000 operating	0.0025 operating 0.005 offices

Composite Beam

Vibration for Sensitive Equipment				Vibration for Walking	
Velocity	Walking Rate			a_p/g	0.0023
	Fast	Medium	Slow		
V	43000.00	9502.00	2554.00	4000 operating	0.0025 operating 0.005 offices



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Column Design

Stories 1-4: 24"x24"

Stories 5-7: 20"x20"

Addition: 18"x18"

$f'_c = 5 \text{ ksi}$

Typical reinforcing:

20 bars (6x4)

24 bars (7x5)

28 bars (8x6)

Longitudinal: #5-#8 bars

Transverse: #4 bars

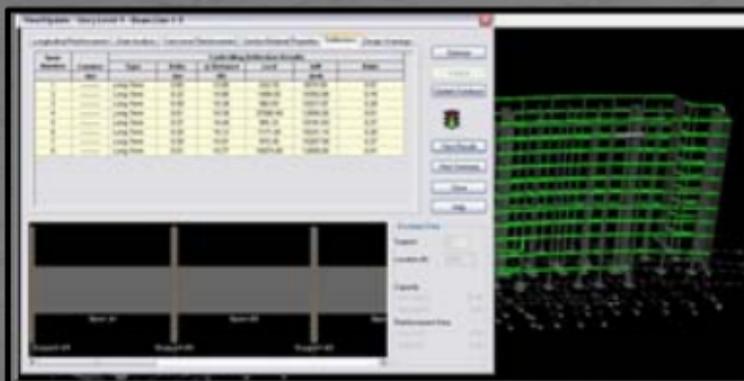
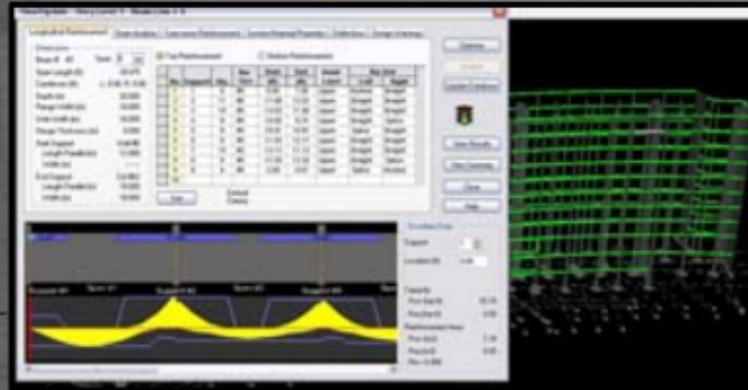
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Beam Design

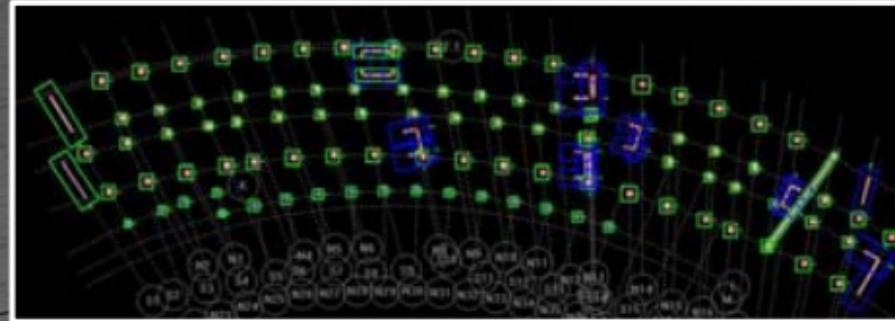
Size: 18" x 20"

$f'_c = 5$ ksi

Typical reinforcing:
#7 - #11 bars



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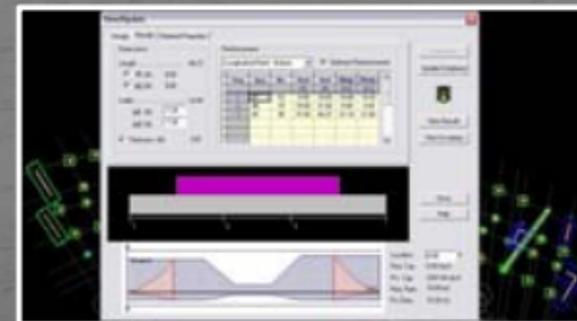
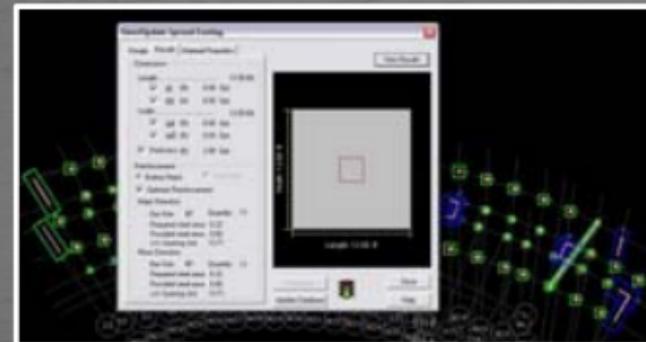


Foundation Design

- Size: 7' x 7' interior spread footings
- 10' x 10' exterior spread footings
- 15' wide continuous walls footings

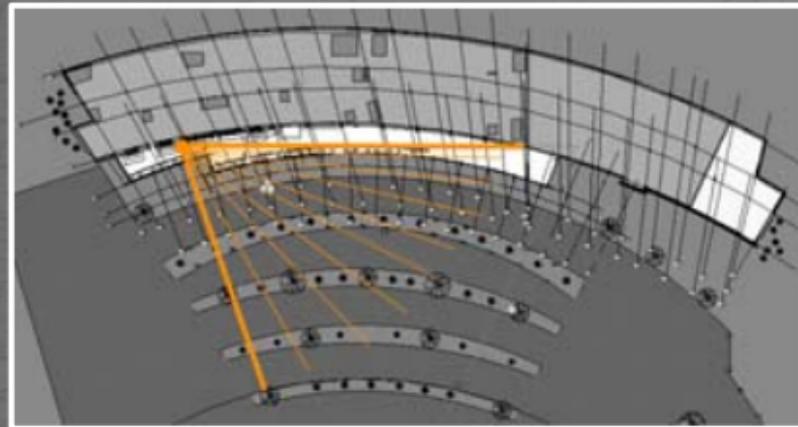
$f'_c = 3$ ksi

Typical reinforcing:
#7 - #11 bars



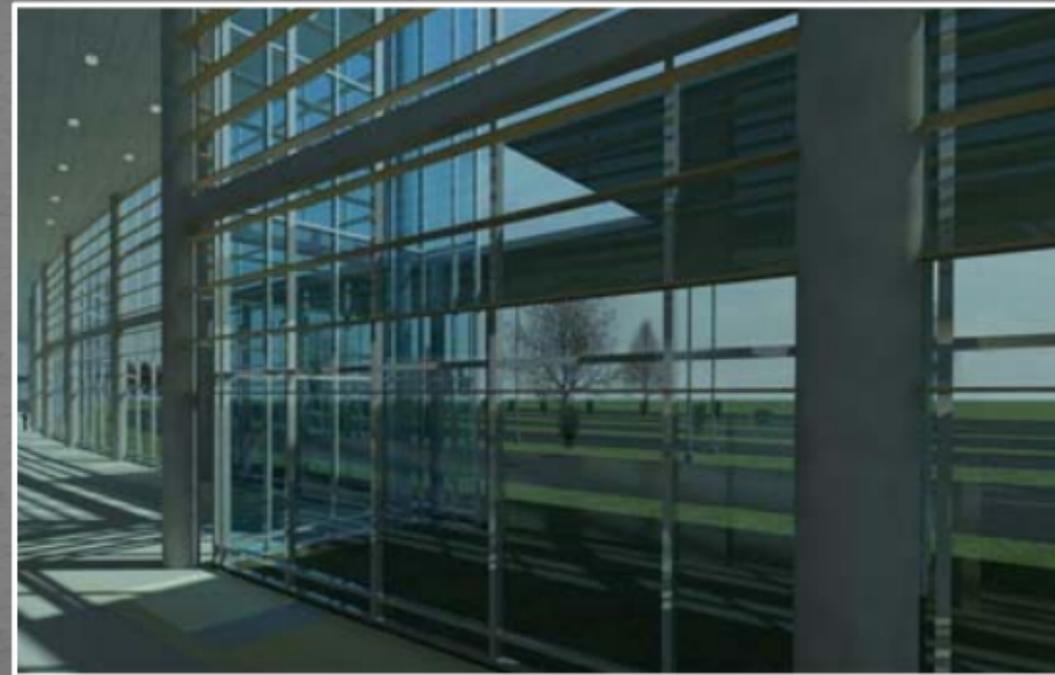
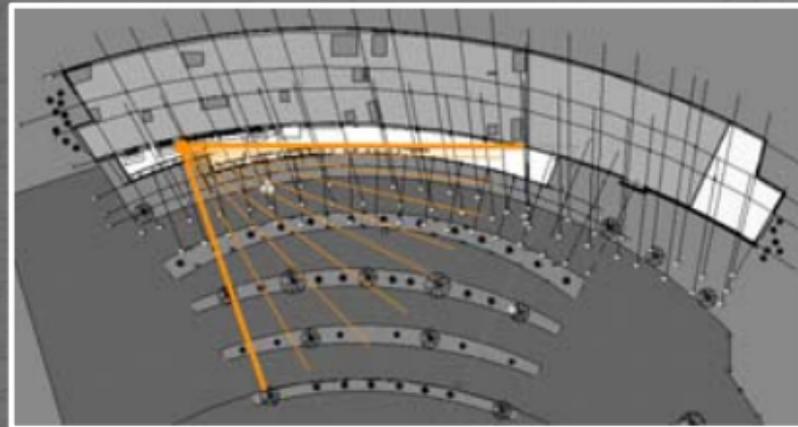
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Interior Lobby-Steel Design



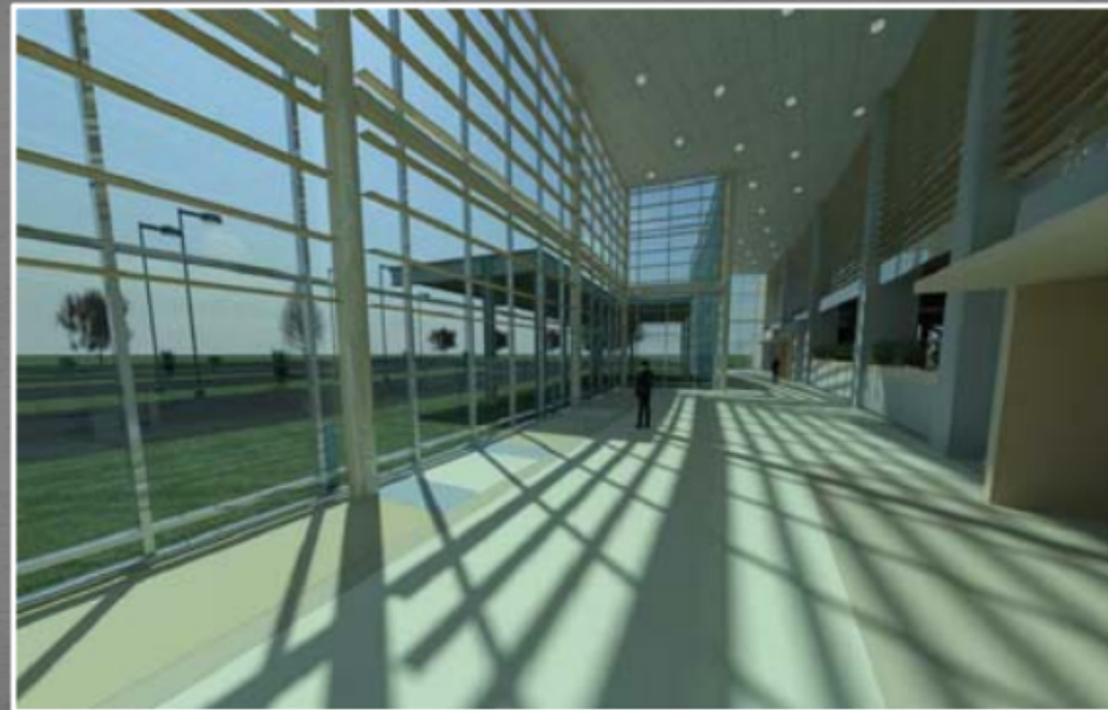
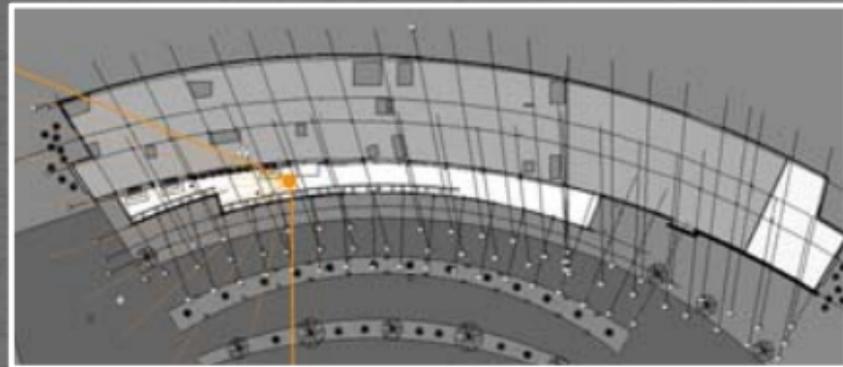
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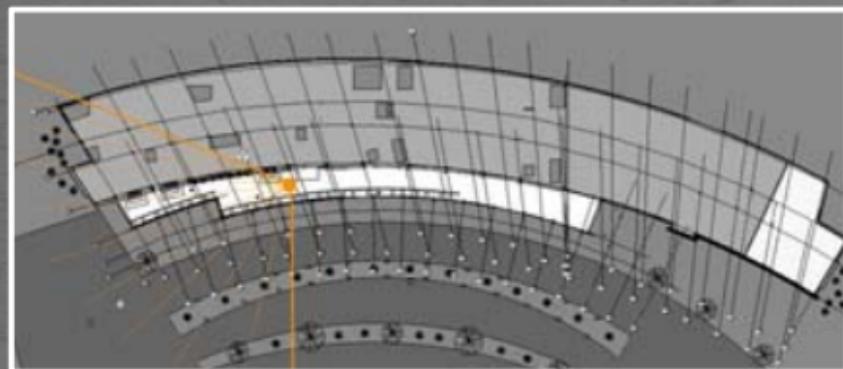
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Interior Lobby-Steel Design



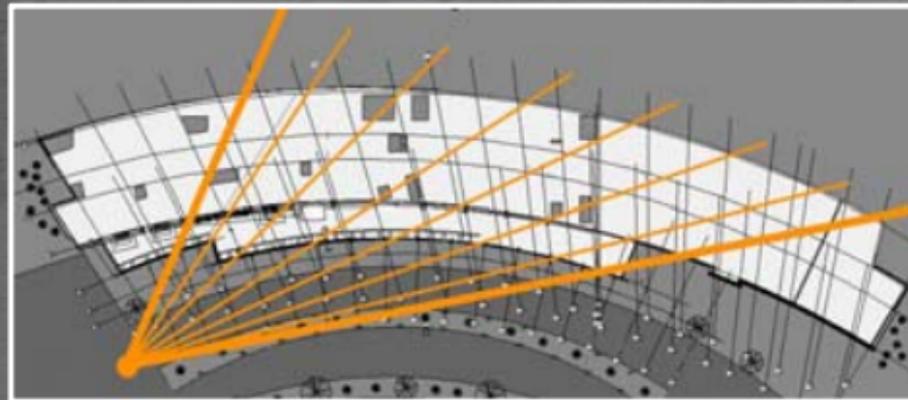
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Interior Lobby-Concrete Design



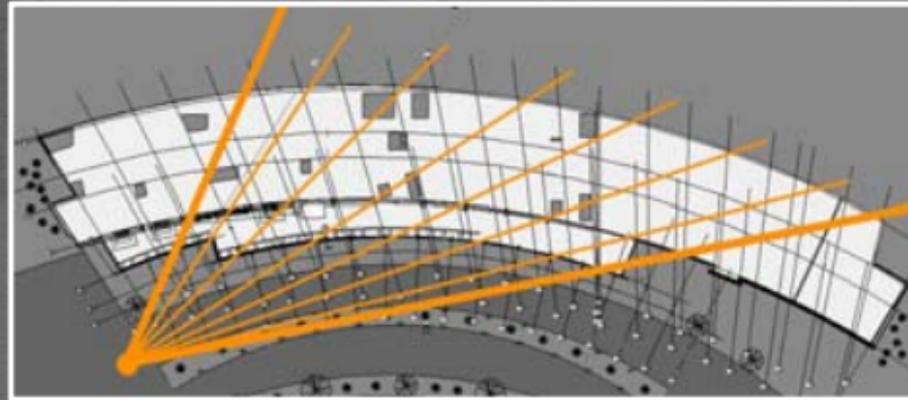
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Exterior-Steel Design



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Cost Analysis- Steel

Structural Framing Schedule		RS Means 2010					
Family and Type	Count	Length (ft.)	Units				Total Cost
			Material	Labor	Equipment		
HSB8X8X1/4	1	80	Each	645	52	12	3,194.00
HSB8X8X1/16	0	180	Each	645	52	12	6,588.00
HSB8X8X1/8	2	40	Each	645	52	12	1,456.00
HSB10X4X1/8	14	447	Each	645	52	12	24,732.00
HSB10X8X1/2	6	210	Each	645	52	12	6,732.00
HSB10X8X1/8	28	520	Each	645	52	12	14,560.00
HSB10X8X3/16	3	60	Each	645	52	12	2,184.00
HSB10X12X1/2	3	225	Each	645	52	12	5,085.00
HSB10X12X1/8	3	25	Each	645	52	12	5,024.00
HSB12X4X3/8	3	20	Each	645	52	12	726.00
HSB12X8X1/2	4	120	Each	645	52	12	2,604.00
HSB12X8X3/8	4	180	Each	645	52	12	4,164.00
HSB12X12X1/2	11	127	Each	645	52	12	7,281.00
HSB12X12X3/8	25	81	Each	645	52	12	14,580.00
HSB12X12X1/2	49	1499	Each	645	52	12	31,488.00
HSB14X4X1/8	2	30	Each	645	52	12	1,456.00
HSB14X8X3/8	1	30	Each	645	52	12	726.00
HSB16X8X3/8	11	180	Each	645	52	12	7,281.00
HSB16X8X3/16	3	60	Each	645	52	12	2,184.00
HSB20X8X1/8	3	90	Each	645	52	12	1,456.00
HSB20X12X1/2	11	201	Each	645	52	12	7,281.00
W/Wide Flange-W8X10	142	2417	LF	\$12.50	\$4.20	\$2.68	\$45,019.68
W/Wide Flange-W8X12	36	832	LF	\$16.00	\$4.64	\$2.80	\$3,860.12
W/Wide Flange-W12X14	13	21	LF	\$18.35	\$2.90	\$1.80	\$305.68
W/Wide Flange-W12X19	623	9647	LF	\$26.50	\$2.90	\$1.80	\$16,213.15
W/Wide Flange-W12X26	6	97	LF	\$31.50	\$2.90	\$1.80	\$2,085.11
W/Wide Flange-W12X35	46	539	LF	\$42.50	\$3.15	\$1.80	\$25,624.94
W/Wide Flange-W12X50	3	60	LF	\$60.50	\$3.40	\$2.16	\$8,308.70
W/Wide Flange-W14X22	125	2417	LF	\$31.50	\$2.58	\$1.62	\$6,072.70
W/Wide Flange-W14X28	669	2009	LF	\$35.00	\$2.55	\$1.41	\$25,548.22
W/Wide Flange-W16X18	64	185	LF	\$37.50	\$2.84	\$1.79	\$8,231.41
W/Wide Flange-W16X24	194	4863	LF	\$42.50	\$3.80	\$1.80	\$21,480.28
W/Wide Flange-W18X40	13	90	LF	\$48.50	\$3.80	\$1.80	\$5,864.96
W/Wide Flange-W20X44	184	1549	LF	\$53.00	\$3.47	\$1.80	\$10,865.86
W/Wide Flange-W20X50	38	1152	LF	\$60.50	\$3.47	\$1.80	\$7,594.24
W/Wide Flange-W20X55	2	81	LF	\$75.00	\$3.57	\$1.80	\$5,956.18
W/Wide Flange-W24X55	209	6104	LF	\$66.50	\$3.33	\$1.80	\$43,886.64
W/Wide Flange-W24X62	11	130	LF	\$75.00	\$3.33	\$1.80	\$8,049.26
W/Wide Flange-W24X68	36	1080	LF	\$82.50	\$3.33	\$1.80	\$47,025.84
W/Wide Flange-W24X76	22	727	LF	\$92.00	\$3.33	\$1.80	\$69,669.02
W/Wide Flange-W24X84	20	228	LF	\$126.00	\$3.52	\$1.67	\$26,811.12
W/Wide Flange-W27X34	64	208	LF	\$102.00	\$3.13	\$1.47	\$21,666.40
W/Wide Flange-W30X30	3	67	LF	\$120.00	\$3.08	\$1.46	\$12,080.18
W/Wide Flange-W30X39	6	100	LF	\$120.00	\$3.08	\$1.46	\$7,182.00
W/Wide Flange-W30X45	3	110	LF	\$131.00	\$3.08	\$1.46	\$11,960.52
W/Wide Flange-W30X54	4	130	LF	\$140.00	\$3.19	\$1.51	\$18,678.20
W/Wide Flange-W33X33	2	60	LF	\$143.00	\$3.14	\$1.49	\$9,741.58
W/Wide Flange-W33X42	2	60	LF	\$157.00	\$3.26	\$1.55	\$11,164.89
W/Wide Flange-W33X54	2	70	LF	\$174.00	\$3.26	\$1.55	\$13,008.94
W/Wide Flange-W36X30	1	67	LF	\$165.00	\$3.53	\$1.60	\$11,699.84
W/Wide Flange-W36X42	1	11	LF	\$265.00	\$3.53	\$1.60	\$11,416.00
Totals	2827	67995					\$ 1,217,303.00

Structural Column Schedule		RS Means 2010					
Family and Type	Length (ft.)	Count	Units				Total Cost
			Material	Labor	Equipment		
HSS Column-HSS14X0.300	751	20	Each	\$ 1,300.00	\$ 97.00	\$ 33.90	\$ 27,890.00
W/Wide Flange-Column-W12X72	407	22	LF	\$ 105.00	\$ 2.60	\$ 1.63	\$ 44,436.61
W/Wide Flange-Column-W14X80	1366.5	55	LF	\$ 143.00	\$ 2.66	\$ 1.67	\$ 204,050.43
W/Wide Flange-Column-W14X99	1369.5	49	LF	\$ 143.00	\$ 2.66	\$ 1.67	\$ 204,507.44
W/Wide Flange-Column-W14X109	616	22	LF	\$ 143.00	\$ 2.66	\$ 1.67	\$ 61,987.28
W/Wide Flange-Column-W14X120	900.16	18	LF	\$ 143.00	\$ 2.66	\$ 1.67	\$ 86,128.56
W/Wide Flange-Column-W14X132	1864.7	66	LF	\$ 143.00	\$ 2.66	\$ 1.67	\$ 282,933.93
W/Wide Flange-Column-W14X145	1868.36	62	LF	\$ 213.00	\$ 2.80	\$ 1.76	\$ 406,480.40
W/Wide Flange-Column-W14X150	433.40	13	LF	\$ 213.00	\$ 2.80	\$ 1.76	\$ 94,743.20
W/Wide Flange-Column-W14X176	927.66	25	LF	\$ 213.00	\$ 2.80	\$ 1.76	\$ 201,821.71
W/Wide Flange-Column-W14X191	38.67	2	LF	\$ 213.00	\$ 2.80	\$ 1.76	\$ 8,413.05
W/Wide Flange-Column-W14X211	993.67	25	LF	\$ 213.00	\$ 2.80	\$ 1.76	\$ 129,198.89
W/Wide Flange-Column-W14X242	991.34	34	LF	\$ 213.00	\$ 2.80	\$ 1.76	\$ 202,822.31
Totals	11792	460					\$1,987,166.45

Floor/Roof Schedule		RS Means 2010										
Family and Type	Level	Volume (cu. ft.)	Area (sq. ft.)	Units	Deck			Concrete			Total Cost	
					Material	Labor	Equipment	Material	Labor	Equipment		
Floor Lobby Floor	Level 1	25131.35	49329	SF	\$ 1.50	\$ 0.31	\$ 0.05	CY	\$ 108.00	\$ 11.25	\$ 35.25	\$ 232,750.59
Floor EWC concrete on Metal Deck	Level 2	24282.67	49794	SF	\$ 1.50	\$ 0.31	\$ 0.05	CY	\$ 108.00	\$ 11.25	\$ 35.25	\$ 236,147.24
Floor EWC concrete on Metal Deck	Level 3	23860.23	49034	SF	\$ 1.50	\$ 0.31	\$ 0.05	CY	\$ 108.00	\$ 11.25	\$ 35.25	\$ 231,205.02
Floor EWC concrete on Metal Deck	Level 4	24130.17	49143	SF	\$ 1.50	\$ 0.31	\$ 0.05	CY	\$ 108.00	\$ 11.25	\$ 35.25	\$ 234,493.68
Floor EWC concrete on Metal Deck	Level 5	24117.61	49144	SF	\$ 1.50	\$ 0.31	\$ 0.05	CY	\$ 108.00	\$ 11.25	\$ 35.25	\$ 234,492.36
Floor EWC concrete on Metal Deck	Level 6	24012.28	49142	SF	\$ 1.50	\$ 0.31	\$ 0.05	CY	\$ 108.00	\$ 11.25	\$ 35.25	\$ 233,605.60
Roof Roof S2	Level 8	4393.86	9038	SF	\$ 1.30	\$ 0.30	\$ 0.04	CY	\$ 108.00	\$ 11.25	\$ 35.25	\$ 44,172.84
Roof Roof S2	Level 8	40350.72	50790	SF	\$ 1.30	\$ 0.30	\$ 0.04	CY	\$ 108.00	\$ 11.25	\$ 35.25	\$ 12,960.26
Totals		890707	311141									\$ 1,771,987.82

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Cost Analysis- Concrete

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Structural Beam Schedule																		
RS Means 2010																		
Type	Length (ft.)	Area (sq. ft.)	Volume (CY)	Formwork				Concrete				Reinforcing				Total Cost		
				Units	Material	Labor	Equipment	Units	Material	Labor	Equipment	Type	Weight (tons)	Units	Material		Labor	Equipment
18"x20"	1412	6207	117.0	SF	\$3.43	\$865	\$ -	CY	\$109.00	\$30.50	\$ 10.85	#7 and below	80.00	Ton	\$ 800.00	\$ 915.00	\$ -	\$ 233,608.89
18"x20"	866	39039	774.59	SF	\$3.43	\$865	\$ -	CY	\$109.00	\$30.50	\$ 10.85							\$ 602,021.53
\$ 835,630.42																		

Structural Column Schedule																			
RS Means 2010																			
Family and Type	Length (ft.)	Area (sq. ft.)	Volume (CY)	Count	Formwork				Concrete				Reinforcing				Total Cost		
					Units	Material	Labor	Equipment	Units	Material	Labor	Equipment	Type	Weight (tons)	Units	Material		Labor	Equipment
20'x20' square	3318	6589	341.35	237	SF	\$2.28	\$6.65	\$ -	CY	\$ 109.00	\$37.00	\$ 18.45	#7 and below	174.00	Ton	\$ 800.00	\$ 1,000.00	\$ -	\$ 566,906.11
24'x24' square	5092	1204	754.44	301	SF	\$2.28	\$6.65	\$ -	CY	\$ 109.00	\$37.00	\$ 18.45	#8 and above	38.30	Ton	\$ 800.00	\$ 650.00	\$ -	\$ 543,375.14
22' dia. circular	599	12920	58.52	34	LF	\$8.15	\$9.70	\$ -	CY	\$ 109.00	\$37.00	\$ 18.45						\$ 20,315.78	
Totals	12357			469															\$ 1,130,597.02

Shear Wall Schedule																		
RS Means 2010																		
Type	Length (ft.)	Area (sq. ft.)	Volume (CY)	Formwork				Concrete				Reinforcing				Total Cost		
				Units	Material	Labor	Equipment	Units	Material	Labor	Equipment	Type	Weight (tons)	Units	Material		Labor	Equipment
22' Area	1432	131922	2443	SF	\$3.43	\$865	\$ -	CY	\$109.00	\$30.50	\$ 10.85	#7 and below	98.00	Ton	\$ 800.00	\$ 915.00	\$ -	\$ 2,174,926.81
\$ 2,174,926.81																		

Floor/Roof Schedule				RS Means 2010									
Family and Type	Level	Volume (cu. ft.)	Area (sq. ft.)	Units	Formwork			Units	Concrete			Total Cost	
					Material	Labor	Equipment		Material	Labor	Equipment		
8' Two-Way Flat Slab	Level 1	27952	41928	SF	\$ 4.43	\$ 4.33	\$ -	CY	\$109.00	\$ 11.75	\$ 35.25	\$ 528,789.72	
8' Two-Way Flat Slab	Level 2	31056	46384	SF	\$ 4.43	\$ 4.33	\$ -	CY	\$109.00	\$ 11.75	\$ 35.25	\$ 587,510.31	
7' Two-Way Flat Slab	Level 3	26836	46004	SF	\$ 4.43	\$ 4.33	\$ -	CY	\$109.00	\$ 11.75	\$ 35.25	\$ 558,045.56	
7' Two-Way Flat Slab	Level 4	27035	46345	SF	\$ 4.43	\$ 4.33	\$ -	CY	\$109.00	\$ 11.75	\$ 35.25	\$ 562,182.01	
7' Two-Way Flat Slab	Level 5	27034	46344	SF	\$ 4.43	\$ 4.33	\$ -	CY	\$109.00	\$ 11.75	\$ 35.25	\$ 562,169.88	
7' Two-Way Flat Slab	Level 6	26916	46142	SF	\$ 4.43	\$ 4.33	\$ -	CY	\$109.00	\$ 11.75	\$ 35.25	\$ 559,719.55	
7' Two-Way Flat Slab	Level 3	5369	9204	SF	\$ 4.43	\$ 4.33	\$ -	CY	\$ 1.37	\$ 0.38	\$ 0.04	\$ 80,982.98	
7' Two-Way Flat Slab	T/Parapet	29511	50590	SF	\$ 4.43	\$ 4.33	\$ -	CY	\$ 1.37	\$ 0.38	\$ 0.04	\$ 445,124.86	
Totals		201708	333141									\$ 3,884,525.08	

Cost Comparison

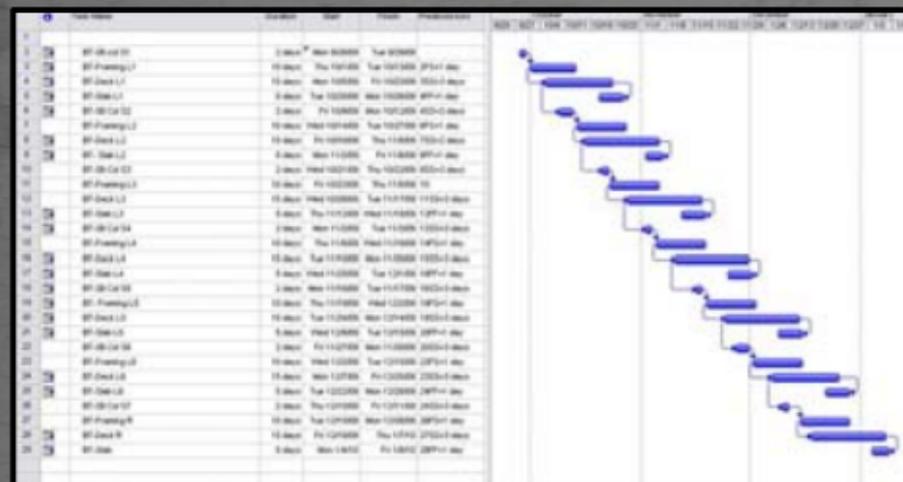
Structural System Cost	
Original Steel Design	
Slabs	\$ 1,771,988
Columns	\$ 1,987,166
Framing	\$ 3,217,304
Total	\$ 6,976,458

Structural System Cost	
Concrete Redesign	
Slabs	\$ 3,884,525
Columns	\$ 1,130,597
Framing	\$ 835,630
Walls	\$ 2,174,927
Total	\$ 8,025,679

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Schedule Comparison

Steel



Total = 102 days

Concrete



Total = 189 days

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Conclusion

Goal #1

Eliminate net tension at the foundation level

- No longer would need tension only mini-piles underneath spread footings

Goal Accomplished!

Goal #2

Improve vibration performance of floor system

- Meet standards established for sensitive equipment

Goal Accomplished!

Recommendations

- A concrete redesign can not be recommended at this point

- Uncertainty due to **COST**

- Uncertainty due to **SCHEDULE**

- Uncertainty due to **ARCHITECTURE**

Presentation Outline

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Acknowledgements

Princeton Health Care System

Turner Construction

Chris Auer
Miles Cava

Penn State AE Faculty/Staff

Dr. Linda Hanagan
Dr. Andres Lepage
Dr. Louis Geschwinder
Dr. Ali Memari
Prof. Parfitt
Prof. Holland
Corey Wilkinson

O'Donnell & Naccarato Structural Engineers

Michael Miller

Severud Associates

Steve Reichwein
Matthew Peitz

McNamara/Salvia Inc.

Bob McNamara

My parents!

My friends!

My fellow classmates!

Thank you for listening!

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