SHA HEADQUARTERS

707 N. Calvert St. | Baltimore, MD



Stephanie Kunkel | www.engr.psu.edu/ae/thesis/portfolios/2011/slk5061 | Mechanical Option

Dr. Bahnfleth | October 27, 2010

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EXECUTIVE SUMMARY

The objective of Technical Report II is to determine the results of an entire building block load energy analysis of the Maryland State Highway Administration (SHA) Headquarters - 707 Building. Trane TRACE 700 Version 6.2 was utilized to calculate the office building load data, as well as the yearly energy consumption, of the 707 building. TRACE inputs were selected from the building design specifications and drawings as well as additional information provided by the design engineer.

The generated block load energy model for the 707 building calculated the total annual energy consumption for cooling and heating loads to be 44.305 MBtu/year. The total load calculated by the design engineer was 42.232 MBtu/year, which indicates that the load energy consumptions are within 4.9% of each other. The annual utility cost that was totaled for the consumed electricity and natural gas was \$200,808 or 1.17 \$/sf. In order to provide a redesigned mechanical system with reduced energy consumptions, the current features of the building's utility usage must be analyzed.

MECHANICAL SYSTEM SUMMARY

The 707 building's mechanical system is comprised of two low pressure central station air handling units (AHUs) serving the central core of the building and one high pressure central station AHU serving the central core of the building. Cooling is provided by a chilled water plant, utilizing a centrifugal chiller and an updraft cooling tower, while heating is provided by two low pressure steam boilers and a steamto-hot water heat exchanger. Overall, the components of the system include 3 constant volume built-up AHUs, 534 perimeter induction units with no operating fans on the 6 office levels, 18 VAV boxes that serve individual areas, a chilled water/hot water indoor unit, and a chilled water/steam indoor unit.

SYSTEM DESIGN LOAD ESTIMATION

To simulate the design load energy consumption of the Maryland State Highway Administration (SHA) 707 Building located in Baltimore, MD, Trane TRACE 700 Version 6.2 was implemented. Operator experience and previously performed analyses were determinants for using TRACE for this energy study. A yearlong energy evaluation was executed to find the peak design heating and cooling loads of the system. A schematic of the system is located in Appendix B.

Block Load Elements

There are multiple advantages for a block load analysis to be performed, including model calculation time reduction, manageable model file sizes, and accurate results. The inputs, such as room areas, equipment characteristics, and building construction materials, were taken from the building design specifications and drawings; additional information was provided by the design engineer.

Load Sources and Modeling Information

Occupants, ventilation, infiltration, artificial lights, electrical and mechanical equipment, ambient conduction/convection and direct solar gain are the core load sources for the 707 building model. TRACE data templates are located in Appendix A.

Design Occupancy and Ventilation

As design occupancy was provided for each space in the 707 building, the ASHRAE recommended occupancies were not utilized. The low-rise office schedule in TRACE was used to determine the fraction of cooling needed during the weekdays; Table 1 depicts these times and percentages. TRACE produced all ventilation rates used in the energy analysis in accordance with ASHRAE Standard 62.1 - 2007.

•	•	
Start Time	End Time	Percentage
Midnight	7 a.m.	0
7 a.m.	8 a.m.	30
8 a.m.	11 a.m.	100
11 a.m.	Noon	80
Noon	1 p.m.	40
1 p.m.	2 p.m.	80
2 p.m.	5 p.m.	100
5 p.m.	6 p.m.	30
6 p.m.	9 p.m.	10
9 p.m.	Midnight	5

Table 1: Weekday Cooling Design for People Loads

Infiltration

0.2 cfm/ft² of the wall for cooling and 0.4 cfm/ft² of the wall for heating are the typical infiltration rates used for office space in the 707 simulation.

Electrical Loads

Since it is required to "use lights and equipment electrical loads on a W/sf basis," the typical office space heat gain from recessed fluorescent, non-vented 80% load to space lighting was calculated to be 1.45 W/ft² by the design engineer. The lighting schedule of a low-rise office building was selected in TRACE; the weekday schedule timings and percentages can be seen in Table 2 below. The miscellaneous loads were 1 W/ft² to account for medium sized computer loads in the open office space.

Start Time End Time Percentage Midnight 7 a.m. 5 7 a.m. 8 a.m. 80 8 a.m. 10 a.m. 90 10 a.m. Noon 95 Noon 80 2 p.m. 2 p.m. 4 p.m. 90 4 p.m. 5 p.m. 95 80 5 p.m. 6 p.m. 6 p.m. 7 p.m. 70

8 p.m.

9 p.m.

10 p.m.

Midnight

7 p.m.

8 p.m.

9 p.m.

10 p.m.

Table 2: Weekday Cooling Design for Lighting Loads

Weather Information

The weather data was taken from the 2009 ASHRAE Handbook of Fundamentals (HOF), and they represent the 0.4% and 99.6% values, respectively. Below, Table 3 shows these values used in the building analysis. Actual weather conditions that were used in TRACE are displayed in the TRACE schedules in Appendix C. The entire Baltimore, MD weather data from ASHRAE 2009 HOF can also be found in Appendix C.

60

40

30

20

ASHRAE Values	Summer Design Cooling (0.4%)	Winter Design Heating (99.6%)
OA Dry Bulb (°F)	93.9	12.9
OA Wet Bulb (°F)	78.1	_

Table 3: ASHRAE Weather Data – Baltimore, MD

System Load Analysis Results

Below, Table 4 indicates cooling, heating, supply, and ventilation rates for the TRACE block load compared to the original loads calculated by the design engineer. The block load values are greater than those of the original calculations; this is most likely due to the simplified load estimations and assumptions of the block load. Specific information for every single room/space must be known and analyzed exactly to obtain the most accurate cooling and heating loads for 707. Nonetheless, even with the simplifications that were made for the block load, the findings show a plausible portrayal of the loads that the design engineer calculated.

Table 4: Block Loads vs. Original Loads and Ventilation

	Cooling (ft²/ton)	Heating (Btu/h*ft²)	Supply Air (cfm/ft²)	Ventilation Air (cfm/ft²)
707 Block Load	405.4	27.9	0.85	0.15
707 Original	535.2	21.6	0.37	0.14

SYSTEM ENERGY CONSUMPTION & OPERATING COSTS

A year-long energy simulation was composed by the TRACE model that was used to find the building design cooling and heating loads. Cooling is provided by a chilled water plant operated by electricity, while heating is provided by two low pressure steam boilers and a steam-to-hot water heat exchanger.

System Energy Classification

According to the energy analysis results, the 707 building consumes 1,743,765 kWh of energy annually. The breakdown of this energy consumption is shown in both Table 5 and Figure 1 below. Typical for an office building in this region, space heating and lighting are large energy consumers. Since there are no fans within any of the 534 induction units for the cooling system, the amount of energy expended is reduced when compared to a standard office building.

	Energy (kBtu/yr)	Total Energy (%)
Lighting	2951.2	35
Space Heating	2533.5	30
Receptacles	1986.7	24
Space Cooling	566.2	7
Heat Rejection	310.4	4

Table 5: Energy Consumption Breakdown

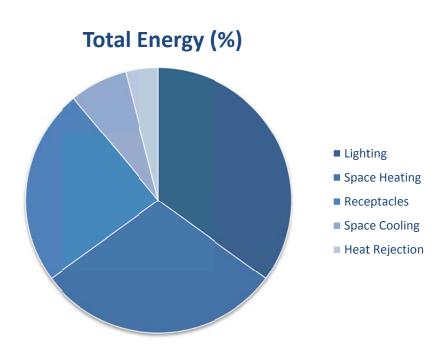


Figure 1: Energy Consumption Pie Chart

A monthly breakdown of the electrical and natural gas energy consumption can be seen in Figures 2 and 3, respectively. Typically, winter months and peak summer months consume the most energy, since the building is most heavily heated and cooled during those times. Since the heating system runs on natural gas and not electricity, Figure 2 shows the greatest electrical energy use during the summer months when the maximum AHU use occurs. Similarly, Figure 3 displays peaks in energy of the natural gas usage in the winter months.

Monthly Energy Consumption

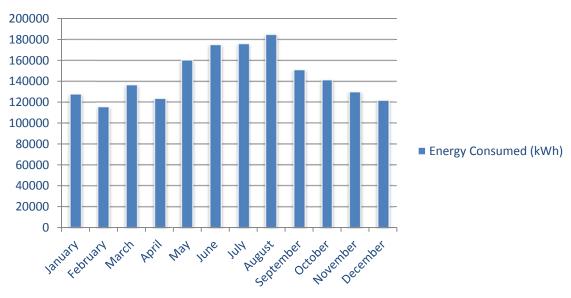


Figure 2: Monthly Electrical Energy Consumption Chart

Monthly Energy Consumption

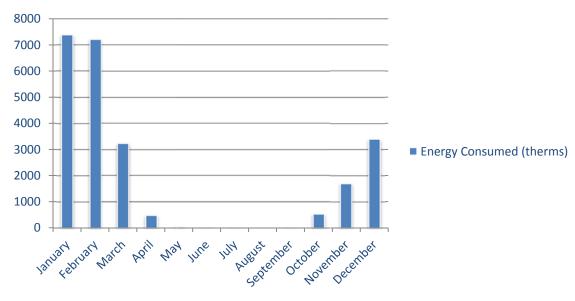


Figure 3: Monthly Natural Gas Energy Consumption Chart

Building Energy Cost Analysis

Knowing the monthly energy usages, an annual building operating cost analysis can be performed. Tables 5 and 6 display the utility rates for both electricity and natural gas, respectively, from the Baltimore Gas and Electric Company (BGE) website. These values were manually inserted into TRACE in the form of utility schedules, seen in Table 7, so that the energy consumption could be calculated in a yearlong energy simulation. Table 7 below shows the schedule of BGE Off-Peak, Mid-Peak, and Peak rates.

Table 5: BGE Electric Rates

	Demand Charge	Peak	Mid-Peak	Off-Peak
	(\$/kW)	(\$/kWh)	(cents/kWh)	(cents/kWh)
Electricity	3.95	0.1155	0.0927	0.0882

Table 6: BGE Natural Gas Rates

	Up to first 10,000 therms (\$/therm)	Above 10,000 therms (\$/therm)
Natural Gas	0.198	0.095

Table 7: Schedule of BGE Rates

Start Time	End Time	Rate
11 p.m.	7 a.m.	Off-Peak
7 a.m.	10 a.m.	Mid-Peak
10 a.m.	8 p.m.	Peak
8 p.m.	11 p.m.	Mid-Peak

The total annual utility cost that was totaled for the consumed electricity and natural gas is \$200,808 or 1.17 \$/sf. TRACE's monthly breakdown of this analysis is shown in Figure 4. As displayed below, the highest monthly cost occurred in August. The reasoning for the drastic cost differentiations between the winter and summer months is most likely due to the low natural gas rate.

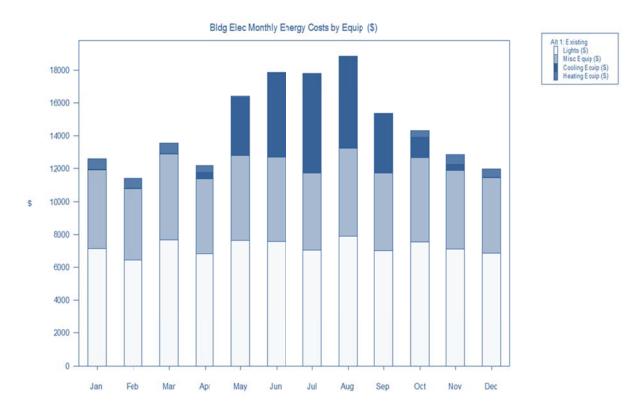


Figure 4: Monthly Building Electricity Costs by Equipment Chart

Environmental Impact Analysis

As well as the energy consumption assessment, the environmental impact of the emissions from the building is another vital element to consider. Average annual carbon dioxide, sulfur dioxide, nitrogen oxide emissions, and particulates were calculated manually. Using the given regional emissions coupled with the delivered electric energy for the 707 building location and emissions profiles associated with the boiler, the annual existing emissions footprint was determined. The assessed emissions summaries for the 707 building are shown in Tables 8 and 9, below.

Emission	Eastern Emission Factors (lbm/kWh)	Tot	al Electricity Usage (kWh)	Total Emissions for Delivered (lbm/yr)
CO ₂	1.64			2,859,775
SO _x	8.57E-3		1 7/2 7/5	14,944
NO _X	3.00E-3		1,743,765	5,231
PM10	9.16E-5			160

Table 8: Combustion Emissions Produced by Electricity

According to the Regional Gridemission factors 2007.pdf,

The PM factors are for direct emissions and do not include the effect of particulate formation in the atmosphere from chemical reactions of sunlight with emissions of NOx, SO_x, [and CO₂]. The PM composition and emission levels are complex functions of boiler firing configuration, boiler operation, pollution control equipment, and fuel properties.

Emission Natural Gas Natural Gas Usage Conversion Factor Total Emissions for Delivered (Btu/ft³) (lbm/1000ft³) (MBtu/year) (lbm/yr) 11.6 508.850 CO_2 SO_{X} 1.22 53,517 1010 44.305 NO_X 1.64E-2 719 PM10 8.17E-4 36

Table 9: Combustion Emissions Produced by Natural Gas

As learned in the Penn State Building Thermal Load Simulation and Energy Utilization Estimation course, only about 30% of original electricity produced is delivered to a building, where an efficient boiler delivers the energy more directly. The emissions from electricity are significantly greater than those from the natural gas because the majority of the building energy comes from electricity.

Building Energy and Cost Analysis Results

The generated block load energy model for the 707 building calculated the total annual energy consumption for cooling and heating loads to be 44.305 MBtu/year. The total load calculated by the design engineer was 42.232 MBtu/year, which indicates that the load energy consumptions are within 4.9% of each other. No energy cost analysis was run by the design engineer, therefore results could not be compared.

An estimated operating cost was determined by using individual utility consumptions. The total annual utility cost that was totaled for the consumed electricity and natural gas is \$200,808 or 1.17 \$/sf. The final operating cost per square foot will provide a unit of measurement that can be used to compare the building's energy performance to the redesign. The same combustion emissions analysis for the operation of the redesign will be performed in order to quantify the emissions footprint enhancements of the redesigned building.

REFERENCES

ANSI/ASHRAE (2007), Standard 62.1-2007, Ventilation for Acceptable Indoor Air Quality. American Society of Heating, Refrigerating, and Air Conditioning Engineers, Inc., Atlanta, GA, 2007.

ANSI/ASHRAE (2007), Standard 90.1-2007, Energy Standard for Buildings Except Low-Rise Residential Buildings. American Society of Heating, Refrigerating, and Air Conditioning Engineers, Inc., Atlanta, GA, 2007.

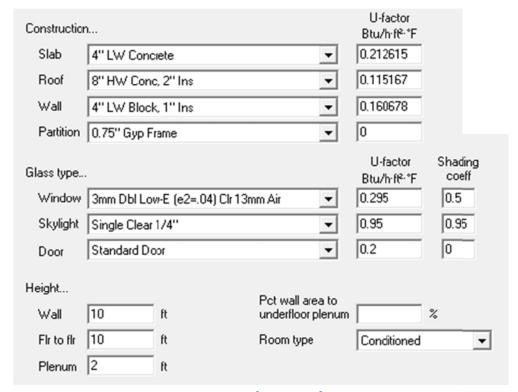
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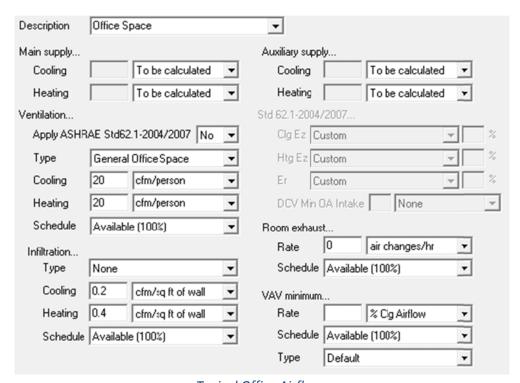
Johnson, Mirmiran & Thompson (JMT). Engineering Reports and TRACE Documents.

RegGridemissionfactors2007.pdf.

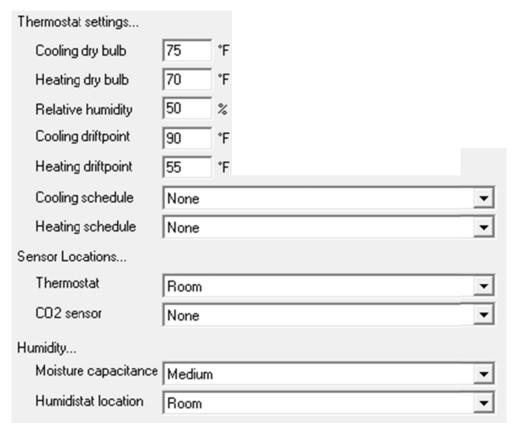
APPENDIX A - TRACE DATA TEMPLATES



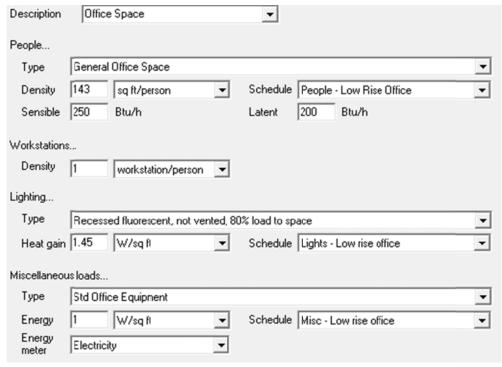
Construction Information for 707



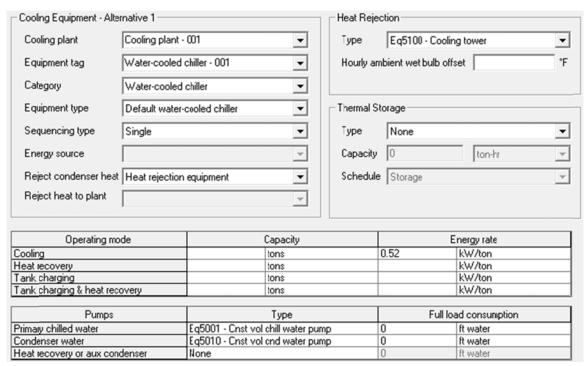
Typical Office Airflows



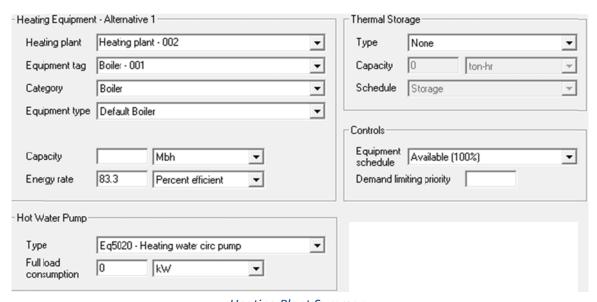
Thermostat Settings for 707 Office Space



Typical Office Internal Loads

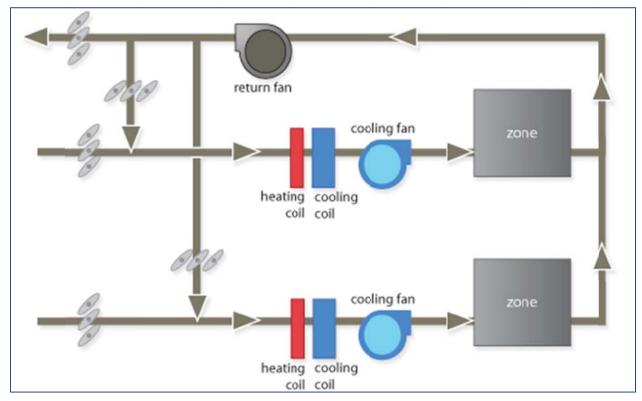


Cooling Plant Summary



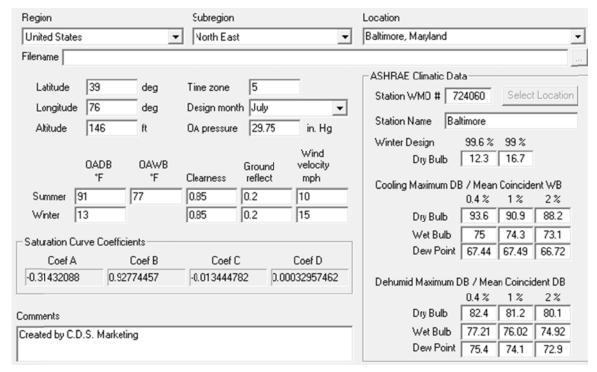
Heating Plant Summary

APPENDIX B - TRACE SYSTEM SCHEMATIC



System Schematic

APPENDIX C - WEATHER INFORMATION



Weather Conditions for Baltimore, MD

2009 ASHRAE Handbook - Fundamentals (IP)

Lat: 39.17N Long: 76.68W

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Period: 82-06

BALTIMORE BLT-WASHNGTN INT'L, MD, USA

Time Zone: -5.00 (NAE)

WMO#: 724060 WBAN: 93721

0-144	Here	- 00		Humi	diffication DP	MCDB and	d HR			Coldest mont	h WS/MCE	OB OB	MCWS	PCWD
Coldest Month	Heatir	g us	99.6%		99%		0.4%		1%		to 99.6% DB			
Month	99.6%	99%	DP	HR	MCDB	DP	HR	MCDB	WS	MCDB	WS	MCDB	MCWS	PCWD
1	12.9	17.3	-3.3	4.6	17.8	1.3	5.9	22.1	26.2	31.6	24.2	32.1	8.7	290

StdP: 14.61

Annual Cooling, Dehumidification, and Enthalpy Design Conditions

Elev: 154

Haman	Hottest		Cooling DB/MCWB						Evaporation WB/MCDB						MCWS/PCWD	
Hottest	Month	0	4%	1	%		20%	0.	4%	1	%	2	%	to 0.4	% DB	
Month	DB Range	DB	MCWB	DB	MCMB	DB	MCWB	WB	MCDB	WB	MCDB	WB	MCDB	MCWS	PCWD	
7	18.7	93.9	74.9	91.2	74.2	88.5	73.1	78.1	88.6	76.8	86.5	75.6	84.3	10.2	280	
			Dehumidific	ation DP/M0	CD8 and HR	2					Enthalp	y/MCDB			Hours	
	0.4%			1%			2%		0.4	4%	1	%	2	%	8 to 4 &	
DP	HR	MCDB	DP	HR	MCDB	DP	HR	MCDB	Enth	MCDB	Enth	MCDB	Enth	MCDB	55/69	
75.3	133.3	82.1	74.1	127.9	80.8	73.0	123.1	79.8	41.5	89.1	40.2	86.5	39.1	84.5	723	

Extreme Annual Design Conditions

Extreme Annual WS		M	ean	Standard	deviation	n=5	years	n=10	years	n=20	years	n=50	years
% 5%	WB	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max
.2 17.3	84.6	5.1	98.0	6.3	3.3	0.6	100.3	-3.1	102.2	-6.7	104.0	-11.3	106.4
T			6 5% WB Min	6 5% WB Min Max	6 5% WB Min Max Min	6 5% WB Min Max Min Max	6 5% WB Min Max Min Max Min	6 5% WB Min Max Min Max Min Max	6 5% WB Min Max Min Max Min Max Min	6 5% WB Min Max Min Max Min Max Min Max	6 5% WB Min Max Min Max Min Max Min Max Min Max Min	6 5% WB Min Max Min Max Min Max Min Max Min Max Min Max	6 5% WB Min Max Min Max Min Max Min Max Min Max Min Max Min

		Annual	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
	Tavg	55.9	33.9	36.9	44.2	54.2	63.6	72.7	77.6	75.7	68.3	56.8	47.3	37.8
Temperatures, Degree-Days and Degree-Hours	Sd	30.3	10.07	8.67	9.29	8.30	7.49	6.31	5.08	5.20	6.95	7.72	8.51	9.29
	HDD50	1726	507	376	231	45	1	0.51	0	0	0.33	22	152	392
	HDD65	4567	964	787	649	339	119	12	0	2	45	275	532	843
		3861	8	9	50	171	424	680	855	796	550	232	71	15
	CDD50 CDD65	1228	0	0	4	15	77	242	390	333	145	21	1	
		11317	0	1	42	195	792	2240	3853	2963	1071	148	11	0
	CDH74			_	-	57						23		1
	CDH80	4315	0	0	8	5/	267	849	1669	1125	317	23	0	0
Monthly Design Dry Bulb and Mean Coincident Wet Bulb Temperatures	0.4%	DB	65.2	69.3	80.0	86.9	90.9	94.6	98.0	96.9	92.6	83.2	75.3	68.
		MCWB	57.7	56.2	62.2	66.7	71.5	74.5	76.5	75.9	72.8	68.9	63.6	60.
	2%	DB	59.5	61.4	71.1	79.6	86.8	91.3	94.7	92.6	87.1	78.1	69.8	62.
		MCWB	54.5	53.5	58.1	63.2	69.3	73.9	75.7	75.0	71.7	66.9	60.2	55.
	5%	DB	53.0	55.5	64.7	74.1	82.6	88.2	91.8	89.2	83.4	74.0	65.3	56.
		MCWB	46.8	47.5	54.1	60.3	67.9	73.0	74.9	73.8	70.1	64.3	58.7	51.
	10%	DB	47.6	50.4	59.4	69.3	78.1	85.1	88.7	86.1	80.2	70.2	61.4	51.
		MCWB	42.7	44.3	50.1	57.3	65.5	71.8	74.0	72.5	69.0	62.5	55.6	46.
Monthly Design Wet Bulb and Mean Coincident Dry Bulb Temperatures	0.4%	WB	60.1	60.1	64.6	68.9	74.8	78.8	80.2	79.4	77.0	72.2	66.5	62.
		MCDB	63.2	66.0	76.5	80.5	86.0	88.3	91.3	90.0	85.0	77.8	70.8	67.
	2%	WB	55.0	53.7	60.2	65.7	72.1	76.5	78.4	77.5	75.0	69.8	63.5	57.
		MCDB	58.6	58.7	68.8	75.7	82.8	85.9	89.4	88.0	82.1	75.5	67.9	61.
	5%	WB	47.9	49.1	55.7	62.4	69.7	75.2	77.2	76.2	73.3	66.6	60.1	52.
		MCDB	50.9	54.0	62.1	71.4	79.4	84.2	87.6	85.0	79.2	71.9	64.1	55.
	10%	WB	43.3	45.1	51.5	59.3	67.4	73.7	76.0	74.9	71.7	63.8	56.7	47.
		MCDB	47.2	50.2	58.5	67.2	75.4	81.7	85.2	82.5	77.2	68.8	60.6	50.
Mean Daily Temperature Range		MDBR	15.5	16.7	18.4	20.3	20.2	19.6	18.7	18.3	18.6	19.8	18.6	16.
	5% DB	MCDBR	22.7	24.8	26.8	27.7	26.2	23.2	22.4	21.7	22.1	23.8	23.5	22.
		MCWBR	17.1	17.3	16.6	14.6	12.2	9.6	8.1	8.3	9.7	13.7	16.1	17.
	5% WB	MCDBR	20.1	21.3	23.7	24.0	22.7	19.6	19.1	18.6	17.7	19.3	19.6	19.
		MCWBR	17.2	17.0	16.5	14.0	11.7	9.2	8.2	8.2	9.1	12.5	16.2	17.
Clear Sky Solar Irradiance	taub		0.319	0.353	0.411	0.417	0.474	0.546	0.552	0.580	0.421	0.370	0.342	0.3
	taud		2.373	2.188	1.997	2.036	1.892	1.746	1.769	1.681	2.164	2.286	2.350	2.4
	Ebn,noon		269	272	266	273	258	239	237	225	261	264	258	26
	Edh.noon		30	40	52	53	62	72	69	74	44	36	31	27

ASHRAE 2009 HOF Weather Data for Baltimore, MD