# Seth M. Moyer

# Office Building





# Structural Option

# Advisor: Dr. Thomas E. Boothby





- > Business/Office Space
- > 85,075 SF
- > Top of Parapet: 74'-5"
- > March 2012 April 2013
- > \$11 Million
- > Design-Bid-Build





Project Site

- > Architectural Partnership
- Elliott + Assoc. Architects > Architect of Record
  - Silling Assoc., Inc.
- > General Contractor
- High Construction Co. > Structural/MEP/Civil
  - Larson Design Group





# Plan Layout





Foundations
Spread, Combined and Strip

# **Foundation Plan**



> Foundations > Framing

- Spread, Combined and Strip
- 4" NWC on Composite Deck
- on Open Web Steel Joists
- Wide Flange Beams and Columns



# **Typical Framing Plan**

> Foundations > Framing > Lateral System

- Spread, Combined and Strip

- 4" NWC on Composite Deck
- on Open Web Steel Joists
- Wide Flange Beams and Columns
- 16 "K" Braced Frames



### **Bracing Details**



> Bracing not Fully Triangulated

> Bending Moments in Columns

> Effectively Act as Moment Frames



> Replace Braced with Moment Frames

> Design Frame Members for Drift and Check for Strength Requirements

> Design/Detail FR Moment Connections



> No Braces Above/Below Windows

> Options for Façade

> Opportunity to Open Building Up



> Enclosure Redesign

> Analyze Barrier Performance

> Assess Mechanical Loads and Systems Impact



> Pinned Column Bases

> H/500 Drift Limit

> Potentially Very Flexible System

> 10-year vs. 700-year MRI Wind Speeds

> Force Multiplier:  $-(76mph/115mph)^2=0.44$ 

> D + 0.5L + 0.44W







(2)-

(4)—

(8)-

(9)-

> Building Introduction > Structural Overview > Proposal > Structural Depth > Breadth Studies Conclusion

# **Existing Braced Frame Layout**

# **Proposed Moment Frame Layout**







### **ETABS Braced Frames Model**

### **ETABS Moment Frames Model**









### N-S Frames at Grids A and K







### Second-Order Analysis

### > Building Periods Shortened:

Office Building Modes		
Mode	Period (s)	Direction
1	0.4125	N-S (Y)
2	0.3998	E-W (X)
3	0.3238	Rotation (Z)

> 22% Increase in Seismic Base Shear

> Iterative Based on P- $\Delta$  Combo: -1.2D + 0.5L + 0.5S

> 20% Stiffness Reduction

 $\rightarrow \Delta_{2nd}/\Delta_{1st} < 1.7$ 

> Wind Still Controls Lateral

### > Direct Analysis Method in ETABS



> FR Bolted Flange-Plated Connections

> Bolted Single-Plate Shear Tabs

> Several Critical/Representative Joints Selected for Design and Detailing

> Local Flange Bending

> Local Web Yielding

> Local Web Crippling

> Panel Zone Shear Yielding

# Column Stiffening Checks





(E)  $(\kappa)$ W18X35 W18X35 W18X35 W18X35 W14x233 W24x84 · W18X35 W18X35 W18X35 W18X35 TORY4 1/2" (TYP) -W18X35 W18X35 W18X35 W18X35 STORY: W18X55 W18X55 W18X55 W18X55 STORY2 1 1/2" (TYP) ≥ ᠳ᠊ᢍ᠊ᢍ᠊ᢍ W24X84 W24X84 W24X84 V24X84 STORY TYP 3/16 3/16

J-1 at Level 2









> Assess Impact on Mechanical Loads and Equipment

### View of Southern Facade

> Replace IMPs with All-Glazed Curtain Wall System

> Analyze Barrier Performance



> Compared Kawneer Trifab VG 451T, Kawneer 1600 Wall System 1 and Others

> Building Introduction > Structural Overview > Proposal > Structural Depth > Breadth Studies > Conclusion

Selected Kawneer 1600 Wall System 1 with 1" Vision and Spandrel IGUs:



View of Southern Facade

**Product Description** 

1/4" Oldcastle BuildingEnvelope<sup>TM</sup> SunGlass® Low-E #2 1/2" Black Anno Spacer, Argon Filled

1/4" Clear Float

1/4" Oldcastle BuildingEnvelope<sup>TM</sup> SunGlass® Low-E #2

1/2" Black Anno Spacer, Argon Filled

1/4" Clear Float with Ceramic Frit #4





Mullion Spacing

- > Kawneer 1600 Spans 13'-4" b/w Floor **Elevations in Original Layout**
- > C&C Corner Zone Max Pressure: -42.7psf
- > 2'-8" OC Max Vertical Aluminum

- > 18" Wide Vertical Spandrel Strips at Grids Conceal Columns Beyond
- > 3'-0" Tall Horizontal Spandrel Strips
- > Rows of SunGlass Tinted Vision Glass Extend Vertically 10'-4" from Floors



Hide Floor System and Large MF Beams





### Proposed Enclosure Layout



### Wall Section at IMP

### > Kingspan 400 V-Wave IMPs Wall Section - $R_T$ : 26.3 hr-ft<sup>2</sup>-°F/Btu

> Kawneer 451T - Vision Glass Wall Section -  $R_{T}$ : 3.85 hr-ft<sup>2</sup>-°F/Btu





> Kawneer 1600 – Vision Glass Wall Section -  $R_T$ : 3.35 hr-ft<sup>2</sup>-°F/Btu

### Wall Section at Spandrel Glass

### > Kawneer 1600 – Spandrel Glass Wall Section - $R_T$ : 17.9 hr-ft<sup>2</sup>-°F/Btu



> Existing:

> Proposed: - 1600 Vision: 38,276 SF - 1600 Spandrel: 11,359 SF

Mechanical Systems Impact

> 70% Increase in Conductive Enclosure and Solar Loads

> 10 20-Ton Condensing Units with 174 Tons of Demand

> Existing Enclosure Portion of Total Load is 55%

> Redesign Causes 40% Increase in Total Demand

- IMPs: 23,649 SF - 451T: 19,175 SF - 1600 Spandrel: 3,457 SF - 1600 Vision: 3,355 SF



> Additional Steel Frame Weight: 168,000 lbs

> \$61,000 Added to Cost of Lateral System

> Potential Cost Saving Opportunities: - Fix Column Bases - Relax Drift Limit

- PR vs. FR Moment Connections

> 40% Increase in Total Demand Requires an Additional 80 Tons of Capacity

> Minimum Additional Mechanical Equipment Cost of \$240,000

Significant Impact of Redesign on Building's Mechanical Systems