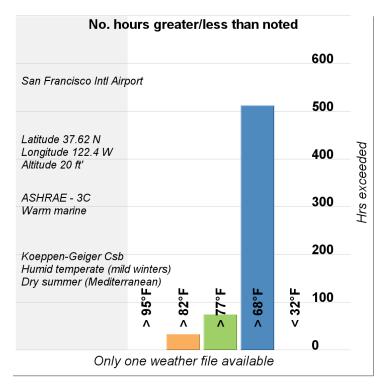
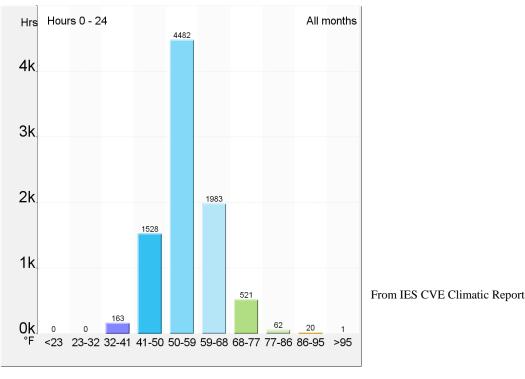
SUPPORTING Documents

APPENDIX A: DESIGN CONDITIONS

WEATHER DATA:



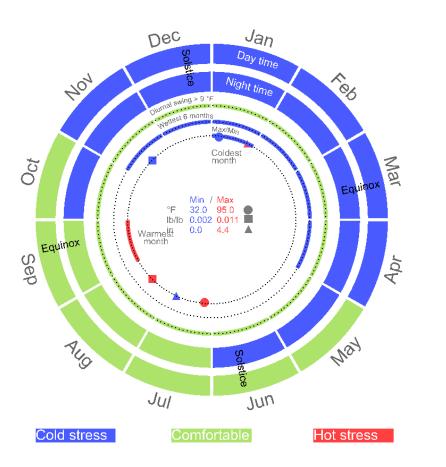
As can be seen in the graphs to the left, San Francisco's location is ideal for passive conditioning methods. The majority of the time, the temperature is between 50°F and 59°F. It is because of this reasonable climate that natural ventilation was a crucial design aspect in the mechanical system. By incorporating natural ventilation into the design we were able to see dramatic energy savings.



DESIGN DATA:

HDD:	3016
CDD:	2883
*Taken from ASHRAE	

ASHRAE Locality: 3C *Taken from IES CVE Climatic Report



Coldest Month:JanuaryWarmest Month:September*Taken from IES CVE Climatic Report

The above graphic was a crucial instrument in the beginning phases of the design process. This graphic effectively displays numerous design criteria such as hottest/coolest months in the year, maximum and minimum temperatures, and typical day/nighttime comfort conditions.

At first glance it is easy to see that the most saving could potentially be obtained in the summer months where the benefits of natural ventilation could be exploited. The circle graph shows that the outside ambient conditions are considered comfortable in the months from May to October. In addition, it indicates that there are not any months with hot stress, indicating that the heating load of the building will be more influential than the cooling load.

APPENDIX B: COMBINED HEAT AND POWER

CO₂ AND FUEL CONSERVATION CALCULATIONS:

Below can be found the formulas/equations that were used to calculate the Carbon and Fuel reductions associated with incorporating a CHP System. The calculation method was taken from "Fuel and carbon dioxide emissions savings calculations methodology for CHP system" prescribed by the EPA.

Formula 1: Fuel Savings from CHP

 $\mathbf{F}_{\mathbf{S}} = (\mathbf{F}_{\mathbf{T}} + \mathbf{F}_{\mathbf{G}}) - \mathbf{F}_{\mathbf{CHP}}$

- F_s Total Fuel Savings (Btu)
- F_T Fuel Use from Displaced On-site Thermal Production (Btu)
- F_G Fuel Use from Displaced Grid Electricity (Btu)
- F_{CHP} Fuel Used by CHP System (Btu)

Formula 2: CO₂ Savings from CHP

 $\mathbf{C}_{\mathbf{S}} = (\mathbf{C}_{\mathbf{T}} + \mathbf{C}_{\mathbf{G}}) - \mathbf{C}_{\mathbf{CHP}}$

- C_s Total CO₂ Emissions Savings (lbs.CO₂)
- C_T Fuel Use from Displaced On-site Thermal Production (lbs.CO₂)
- C_G Fuel Use from Displaced Grid Electricity (lbs.CO₂)
- C_{CHP} CO₂ Emissions from the CHP System (lbs.CO₂)

Formula 3: Fuel Use from Displaced On-Site Thermal Production

$\mathbf{F}_{\mathrm{T}} = \mathbf{CHP}_{\mathrm{T}} / \mathbf{\eta}_{\mathrm{T}}$

- F_T Fuel Use from Displaced On-Site Thermal Production (Btu)
- CHP_T CHP System Thermal Output (Btu) * CHP_T = F_{CHP} *45% (Heat Recovery Efficiency)
- η_{T} Efficiency of the Thermal Equipment

Formula 4: CO₂ Emissions from Displaced On-Site Thermal Production

$C_T = F_T * EF_F * (1*10^{-6})$

- C_T CO₂ Emissions from Displaced On-Site Thermal Production (lbs. CO₂)
- F_T Thermal Fuel Savings (BTU)
- EF_F Fuel Specific CO₂ Emission factor (lbs. CO₂/MMBtu)
- $1*10^{-6}$ Conversion factor from Btu to MMBtu

Formula 5: Displaced Grid Electricity from CHP

$\mathbf{E}_{\mathrm{G}} = \mathbf{CHP}_{\mathrm{E}} \,/ \, (\mathbf{1}\text{-}\mathbf{L}_{\mathrm{T\&D}})$

- E_G Displaced Grid Electricity (kWh)
- $CHP_{E} \quad \ \ \text{- CHP System Electricity Output (kWh)}$
- $L_{T\&D}$ $\,$ Transmission and Distribution Losses $\,$

Formula 6: Fuel Use from Displaced Grid Electricity

$\mathbf{F}_{\mathbf{G}} = \mathbf{E}_{\mathbf{G}} * \mathbf{H} \mathbf{R}_{\mathbf{G}}$

- F_G Fuel Use from Displaced Grid Electricity (Btu)
- E_G Displace Grid Electricity from CHP (kWh)
- HR_G Grid Electricity Heat Rate (Btu/kWh) per subregion *taken from www.epa.gove/cleanenergy/documents pdf file Appendix B

Formula 7: CO2 Emissions from Displaced Grid Electricity

 $\mathbf{C}_{\mathbf{G}} = \mathbf{E}_{\mathbf{G}} * \mathbf{E}\mathbf{F}_{\mathbf{G}}$

- C_G CO_2 Emissions from Displaced Grid Electricity (lbs. CO_2)
- E_G Displace Grid Electricity from CHP (kWh)
- EF_G Grid Electricity Emission Factor (CO₂/kWh) per subregion

Formula 8: CO2 Emissions from CHP System

$C_{CHP} = F_{CHP} * EF_F$

1,395,837(lbs CO₂) = 11,930,234,483(Btu) x 117(CO₂/MMBtu)

- C_{CHP} CO₂ Emissions from CHP System (lbs. CO₂)
- F_{CHP} Fuel used by CHP System (Btu)
- EF_F Fuel Specific Emission Factor (lbs. CO₂/MMBtu)

PROCEDURE:

CO2 and Fuel Conservation Known Quantities

	Quantity	Units
CHP _E	1,014,000	kWh
F _{CHP}	11,930,234,483	Btu
CHP _T	5,368,605,517	Btu
$\mathfrak{y}_{\mathrm{T}}$	80%	
EF _F	117	lbs. CO ₂ /MMBtu
L _{T&D}	0	
HR _G	5,774	Btu/kWh
EF_G	953	lbs. CO ₂ /MWh

Formula 1: $\mathbf{F}_{\mathbf{S}} = (\mathbf{F}_{\mathbf{T}} + \mathbf{F}_{\mathbf{G}}) - \mathbf{F}_{\mathbf{CHP}}$

635 (MMBtu)	= (6,710 + 5,854) - 11,930 (MBtu)
Formula 2: $C_S = (C_T + C_G) - C_{CHP}$	
355,663 (CO ₂)	= (785,159 + 966,342) - 1,395,837 (CO ₂)
Formula 3: $\mathbf{F}_{\mathrm{T}} = \mathbf{CHP}_{\mathrm{T}} / \boldsymbol{\eta}_{\mathrm{T}}$	
6,710,756,897 (Btu)	= 5,368,605,517(Btu)/.8
Formula 4: $C_T = F_T * EF_F * (1*10^{-6})$	
785,159 (CO ₂)	= 6,710,756,897(Btu) x 117 (CO ₂ /MMBtu) * 1*10 ⁶
Formula 5: $\mathbf{E}_{\mathbf{G}} = \mathbf{CHP}_{\mathbf{E}} / (1 - \mathbf{L}_{\mathbf{T\&D}})$	
1,014,000(kWh)	= 1,014,000(kWh) / (1 - 0)
Formula 6: $\mathbf{F}_{\mathbf{G}} = \mathbf{E}_{\mathbf{G}} * \mathbf{H} \mathbf{R}_{\mathbf{G}}$	
5,854,836,000 (Btu)	= 1,014,000(kWh) x 5,774(Btu/kWh)
Formula 7: $C_G = E_G * EF_G$	
966,342 (CO ₂)	= 1,014,000(kWh) x .953(CO ₂ /kWh)
Formula 8: $C_{CHP} = F_{CHP} * EF_F$	
1,395,837 (CO ₂)	= 11,930,234,483(Btu) x 117(CO ₂ /MMBtu)

COMBINE HEAT AND POWER SYSTEM DESIGN:

Max Load Capacities									
Max Heating Capacity	2,100	kBtu/hr							
Max Cooling Capacity	7,380	kBtu/hr							
65 kW Capstone N	licroturbines								
Electrical Efficiency	29%								
Generation Capacity	627	kW							
Quantity	10								
Actual Capacity	650	kW							
Energy Prod	uction								
Generation Capacity	650	kW							
Operating Hours	1,560	hrs/yr							
Generated Power	1,014,000	kWh/yr							
Power Consumption	3,815,944	kWh/yr							
Electrical Capacity Met	33%								
Heat Recovery									
Heat Recovery Efficiency	45%								
Heat Recovery	1,842	Btu/hr							
Capacity Met	88%								

The combined heat and power system (CHP) was sized off of the cooling load since it has the largest capacity. All information necessary for the computation was taken from Capstone's C65 Natural Gas Microturbine Performance Specification Data Sheet. The above table summarizes the resulting plant size, electrical generation capacity, yearly electrical demand satisfied, and thermal hot water capacity met.

СНР РАУВАСК:

The following calculations estimate the time it will take in order to see a full return on the installed CHP system. Taken into account for this calculation are the savings associated with California's CHP/Cogeneration Incentive Program. From this program we were able to receive back \$0.48/W. This translated into a direct rebate/savings of \$312,000. The annual operation and maintenance (O&M) cost of \$.012/kWh was obtain from the EPA Overview document, *Table III: Summary Table of Typical Cost and Performance Characteristics by CHP Technologies*.

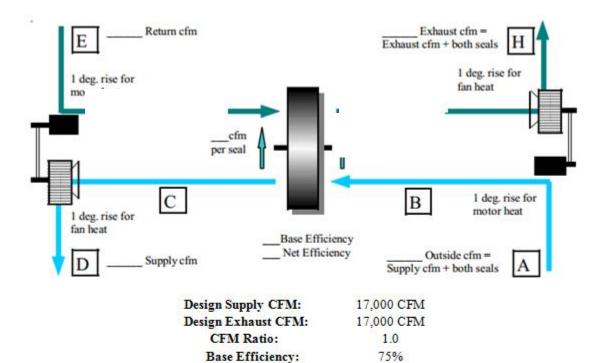
CHP System Payback Period									
Year	Capital Investment	Yearly Maintenance	Spark Spread	Difference					
1	503,000	12,168	101,400	-413,768					
2	0	12,168	101,400	-324,536					
3	0	12,168	101,400	-235,304					
4	0	12,168	101,400	-146,072					
5	0	12,168	101,400	-56,840					
6	0	12,168	101,400	32,392					
7	0	12,168	101,400	121,624					
8	0	12,168	101,400	210,856					
9	0	12,168	101,400	300,088					
10	0	12,168	101,400	389,320					
11	0	12,168	101,400	478,552					
12	0	12,168	101,400	567,784					
13	0	12,168	101,400	657,016					
14	0	12,168	101,400	746,248					
15	0	12,168	101,400	835,480					
16	0	12,168	101,400	924,712					
17	0	12,168	101,400	1,013,944					
18	0	12,168	101,400	1,103,176					
19	0	12,168	101,400	1,192,408					
20	0	12,168	101,400	1,281,640					
21	0	12,168	101,400	1,370,872					
22	0	12,168	101,400	1,460,104					
23	0	12,168	101,400	1,549,336					
24	0	12,168	101,400	1,638,568					
25	0	12,168	101,400	1,727,800					

After running the 25 year analysis it was determined that the CHP system would see a full return in just over 5 years.

APPENDIX C: ENTHALPY WHEEL

ENTHALPY WHEEL/SENSIBLE AND LATENT LOAD CALCULATIONS:

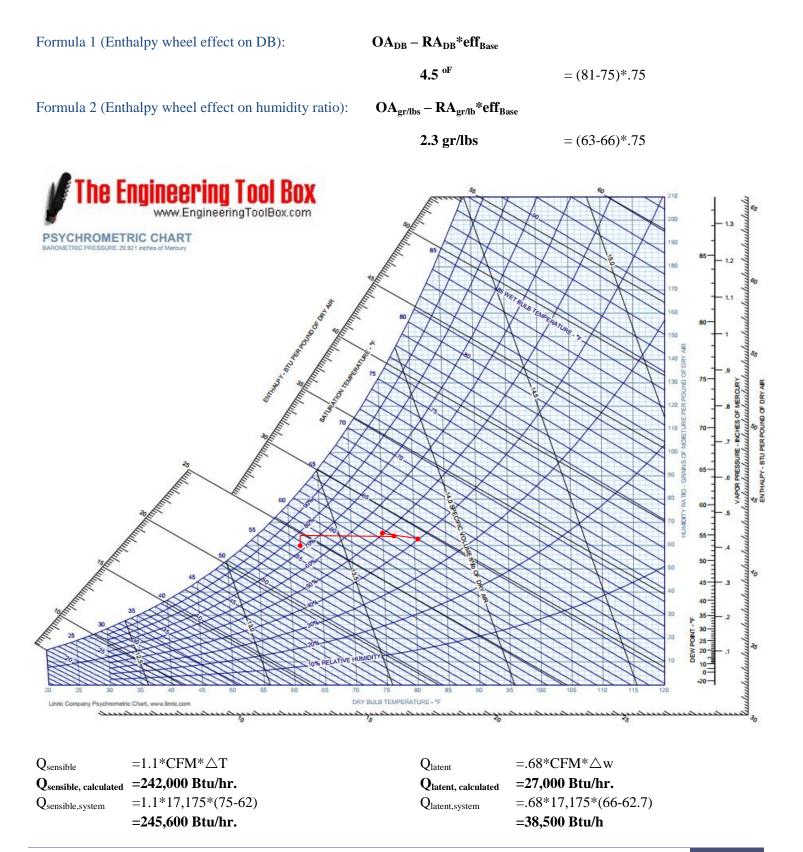
The following section shows the calculations for the enthalpy wheel that was utilized to satisfy the latent load. Also presented are the sensible and latent load values for a typical office floor. The enthalpy wheel calculations were performed via the methods prescribed by the Berner Energy Recovery document found at www.bernerenergy.com. Below is a typical schematic of an enthalpy wheel that will be used to help perform the calculations.



Model No.	CFM	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	
9617	16,000	0.75	0.80	0.83	0.86	0.88	0.91	0.93	0.94	
9017	16,500	0.75	0.80	0.83	0.86	0.88	0.93	0.92	0.94	
	17,000	0.75	0.80	0.83	0.86	0.88	0.90	0.92	0.95	
	17,500	0.74	0.79	0.82	0.86	0.88	0.90	0.92	0.95	
	18,000	0.73	0.78	0.83	0.85	0.87	0.90	0.93	0.95	
Quantity		A	(OA)	D	(SA)	1	E (RA)		H (EX)	
Dry Bulb			81		62		75		75	
Wet Bulb			64		63		63		63	
% Relative H	lumidity		39		-		50		50	
Gr/lbs			63	6	52.7		66		66	

EFFICIENCY OF THE WHEEL AT WHEEL RATIO

Enthalpy Wheel Capacity Procedure:



APPENDIX D: VENTILATION CALCULATIONS

Room Number R	toom Name	Occupancy Categoery (ASHRAE 62.1)	Area A _z (sf)	Area Outdoor Air Rate R _a (Table 6.1)	Occupant Density P _z (#people)	People Outdoor Air Rate R _p (CFM/person)	Breathing Zone Outdoor Air Flow V _{bz} = R _p P _z +R _a A _z (CFM)	Zone Air Distribution Effectiveness E _z (Table 6.2)	Zone Outdoor Air Flow V _{oz} =V _{bz} /E _z
B411 Elevator	- Lobby	Lobby	121	0.06	0.6	5	10	0.8	13
B409 Fireman	s Service Lobby	Lobby	191	0.06	1.0	5	16	0.8	20
B306 Elevator	Lobby	Lobby	221	0.06	1.1	5	19	0.8	23
B300 Fireman	s Service Lobby	Lobby	191	0.06	1.0	5	16	0.8	20
B303 Service L	Lobby	Lobby	109	0.06	0.5	5	9	0.8	12
B206 Elevator	Lobby	Lobby	221	0.06	1.1	5	19	0.8	23
B200 Firemans	s Service Lobby	Lobby	191	0.06	1.0	5	16	0.8	20
B203 Service L	Lobby	Lobby	109	0.06	0.5	5	9	0.8	12
B106 Elevator	Lobby	Lobby	104	0.06	0.5	5	9	0.8	11
B100 Fireman	s Service Lobby	Lobby	187	0.06	0.9	5	16	0.8	20
B103 Service L	Lobby	Lobby	99	0.06	0.5	5	8	0.8	11
103 Service L	Lobby	Lobby	105	0.06	0.5	5	9	0.8	11
200 Fireman	s Service Lobby	Lobby	193	0.06	1.0	5	16	0.8	21
203 Service L	Lobby	Lobby	101	0.06	0.5	5	9	0.8	11
B112 Engineer	rs Office	Office Space	500	0.06	3.0	5	45	0.8	56
B119 Valet Off	fice	Office Space	90	0.06	1.0	5	10	0.8	13
110 Loading [Dock Office	Office Space	100	0.06	1.0	5	11	0.8	14
101 Elevator	Lobby	Lobby	350	0.06	1.8	5	30	0.8	37
111 Retail		Sales	400	0.12	6.0	7.5	93	0.8	116
100 Lobby		Main Entry Lobby	3600	0.06	36.0	5	396	0.8	495
113 Retail		Sales	625	0.12	9.4	7.5	145	0.8	182
215 Lobby		Lobby	1584	0.06	7.9	5	135	0.8	168
209 Restaura	int	Restaurant dinning room	4330	0.18	303.1	7.5	3053	0.8	3816
208 Corridor		Corridor	450	0.06	0.0	0	27	0.8	34
508 Private O	Office	Office Space	100	0.06	1.0	5	11	1.2	9
509 Private O	Office	Office Space	100	0.06	1.0	5	11	1.2	9
510 Private O	Office	Office Space	100	0.06	1.0	5	11	1.2	9
511 Executive	e Office	Office Space	200	0.06	1.0	5	17	1.2	14
512 Copy Roc	om	Occupiable Storage	100	0.06	1.0	5	11	1.2	9
513 Private O	Office	Office Space	100	0.06	1.0	5	11	1.2	9
514 Server Ro	oom	Media Center	100	0.12	0.0	5	12	1.2	10
515 Copy Roc	om	Occupiable Storage	100	0.06	1.0	5	11	1.2	9
516 Private O	Office	Office Space	100	0.06	1.0	5	11	1.2	9
517 Private O	Office	Office Space	100	0.06	1.0	5	11	1.2	9
518 Executive	e Office	Office Space	200	0.06	1.0	5	17	1.2	14
519 Private O	Office	Office Space	100	0.06	1.0	5	11	1.2	9
520 Private O	Office	Office Space	100	0.06	1.0	5	11	1.2	9
521 Private O	Office	Office Space	100	0.06	1.0	5	11	1.2	9
522 Conferer	nce	Conference/Meeting	190	0.06	9.5	5	59	1.2	49
523 Conferer	nce	Conference/Meeting	190	0.06	9.5	5	59	1.2	49
501 Elevator	Lobby	Lobby	350	0.06	1.8	5	30	1.2	25
500 Open Off	fice	Office Space	10250	0.06	51.3	5	871	1.2	726

AEI Team No. 05-2014

APPENDIX E: LOAD CALCULATIONS

AHU-1 - LOBB	Y Cooling Loads					Air Side Cooling				
Room Number	Room Name	Occupancy Category (ASHRAE 62.1)	Area A _z (sf)	Internal Cooling Load (BTU/hr)	Internal Cooling Load (TONS)	Room Air Set Point (F)	Supply Air Flow (CFM)	Supply Air Temperature (F)	Air Side Cooling Capacity (BTU/hr)	Capacity Satisfied
111	Retail	Retail - Sales	441	2,643	0.22	75	185	62	2643	Confirmed
113	Retail	Retail - Sales	743	17,000	1.42	75	1189	62	17000	Confirmed
100	Lobby	Lobby	9362	651,012	54.25	75	45525	62	651012	Confirmed
TOTAL			9,362	670,655	56	75	46,899	62	670,655	

AHU-2 - PODIUM Cooling Loads

Air Side Cooling

Room Room Name Jumber	Occupancy Category (ASHRAE 62.1)	Area A _z (sf)	Internal Cooling Load (BTU/hr)	Internal Cooling Load (TONS)	Room Air Set Point (F)	Supply Air Flow (CFM)	Supply Air Temperature (F)	Air Side Cooling Capacity (BTU/hr)	Capacity Satisfied
B411 Womens Locker Room	Restroom	608	477	0.04	75	22	55	477	Confirmed
B415 Mens Locker Room	Restroom	612	323	0.03	75	15	55	323	Confirmed
B421A Service Corridor	Corridor/ Transition	776	227	0.02	75	10	55	227	Confirmed
B411 Elevator Lobby	Lobby	121	3,825	0.32	75	174	55	3825	Confirmed
B409 Firemans Service Lobby	Lobby	191	6,349	0.53	75	289	55	6349	Confirmed
B306 Elevator Lobby	Lobby	221	6,586	0.55	75	299	55	6586	Confirmed
B300 Firemans Service Lobby	Lobby	191	6,123	0.51	75	278	55	6123	Confirmed
B303 Service Lobby	Lobby	109	2,894	0.24	75	132	55	2894	Confirmed
B206 Elevator Lobby	Lobby	221	6,612	0.55	75	301	55	6612	Confirmed
B200 Firemans Service Lobby	Lobby	191	6,125	0.51	75	278	55	6125	Confirmed
B203 Service Lobby	Lobby	109	3,016	0.25	75	137	55	3016	Confirmed
B119 Valet Office	Enclosed Office	87	174	0.01	75	8	55	174	Confirmed
B106 Elevator Lobby	Lobby	104	2,602	0.22	75	118	55	2602	Confirmed
B100 Firemans Service Lobby	Lobby	187	6,108	0.51	75	278	55	6108	Confirmed
B103 Service Lobby	Lobby	99	2,616	0.22	75	119	55	2616	Confirmed
B112 Engineers Office	Enclosed Office	639	1,151	0.10	75	52	55	1151	Confirmed
110 Loading Dock Office	Enclosed Office	97	185	0.02	75	8	55	185	Confirmed
103 Service Lobby	Lobby	105	2,952	0.25	75	134	55	2952	Confirmed
105 Electrical	Electrical/Mechanical	135	579	0.05	90	15	55	579	Confirmed
107 Exit Passageway	Corridor/ Transition	285	397	0.03	75	18	55	397	Confirmed
108 Exit Vestibule	Corridor/ Transition	62	85	0.01	75	4	55	85	Confirmed
M206 Mechanical Platform	Electrical/Mechanical	1,972	32,488	2.71	90	844	55	32488	Confirmed
208 Corridor	Corridor/ Transition	471	745	0.06	75	34	55	745	Confirmed
205 Electrical	Electrical/Mechanical	135	1,108	0.09	90	29	55	1108	Confirmed
200 Firemans Service Lobby	Lobby	193	7,394	0.62	75	336	55	7394	Confirmed
206 Mechanical Room	Electrical/Mechanical	272	1,592	0.13	90	41	55	1592	Confirmed
203 Service Lobby	Lobby	101	3,782	0.32	75	172	55	3782	Confirmed
TOTAL		5,243	73,099	6		4,145		73,099	

AEI Team No. 05-2014

Mechanical Design

AHU-3 - RESTAURANT	Cooling Loads
--------------------	---------------

Air Side Cooling

Room Number	Room Name	Occupancy Category (ASHRAE 62.1)	Area A _z (sf)	Internal Cooling Load (BTU/hr)	Internal Cooling Load (TONS)	Room Air Set Point (F)	Supply Air Flow (CFM)	Supply Air Temperature (F)	Air Side Cooling Capacity (BTU/hr)	Capacity Satisfied
209A Kito	chen	Food Preperation	1300	23,844	1.99	80	867	55	23844	Confirmed
209 Res	staurant	Dining Area - Family	3400	58,903	4.91	75	2677	55	58903	Confirmed
TOTAL			4,700	82,747	7		3,544		82,747	

AHU-4 - OFFICE Peripheral Cooling Loads

Air Side Cooling

Room Number	Room Name	Occupancy Category (ASHRAE 62.1)	Area A _z (sf)	Internal Cooling Load (BTU/hr)	Internal Cooling Load (TONS)	Room Air Set Point (F)	Supply Air Flow (CFM)	Supply Air Temperature (F)	
508 Pr	ivate Office	Office Space	100	2,388	0.20	75	167	62	
509 Pr	ivate Office	Office Space	100	2,353	0.20	75	165	62	
510 Pr	ivate Office	Office Space	100	2,373	0.20	75	166	62	
511 Ex	ecutive Office	Office Space	200	4,784	0.40	75	335	62	
512 Co	opy Room	Occupiable Storage	100	2,645	0.22	75	185	62	
513 Pr	ivate Office	Office Space	100	2,676	0.22	75	187	62	
514 Se	erver Room	Media Center	100	5,356	0.45	75	375	62	
515 Cc	opy Room	Occupiable Storage	100	2,646	0.22	75	185	62	
516 Pr	ivate Office	Office Space	100	2,639	0.22	75	185	62	
517 Pr	ivate Office	Office Space	100	2,679	0.22	75	187	62	
518 Ex	ecutive Office	Office Space	200	7,225	0.60	75	505	62	
519 Pr	ivate Office	Office Space	100	3,679	0.31	75	257	62	
520 Pr	ivate Office	Office Space	100	3,949	0.33	75	276	62	
521 Pr	ivate Office	Office Space	100	3,591	0.30	75	251	62	
501B El	ectrical	Electrical	100	800	0.07	90	26	62	
501A Te	elecomm	Electrical	100	800	0.07	90	26	62	
<u> </u>	pen Office	Office Space	2,563	40,046	3.34	75	2,800	62	
TOTAL			4,363	90,629	8		6,278		

AHU-5 - OFFICE Core Cooling Loads

Air Side Cooling

Room Number	Room Name	Occupancy Category (ASHRAE 62.1)	Area A _z (sf)	Internal Cooling Load (BTU/hr)	Internal Cooling Load (TONS)	Room Air Set Point (F)	Supply Air Flow (CFM)	Supply Air Temperature (F)	Air Side Cooling Capacity (BTU/hr)	Capacity Satisfied
522 Co	onference	Conference/Meeting	200	4,200	0.35	75	294	62	4,200	Confirmed
523 Co	onference	Conference/Meeting	200	4,213	0.35	75	295	62	4,213	Confirmed
501 Ele	evator Lobby	Lobby	350	18,412	1.53	75	1,288	62	18,412	Confirmed
506A Me	en's Restroom	Restroom	270	4,408	0.37	75	308	62	4,408	Confirmed
506B Wo	omen's Restroom	Restroom	270	4,452	0.37	75	311	62	4,452	Confirmed
500 Op	oen Office	Office Space	7,689	120,139	10.01	75	8,401	62	120,139	Confirmed
TOTAL			8,979	155,824	13		10,897		155,824	

AEI Team No. 05-2014

Air Side Cooling
Capacity (BTU/hr)

Capacity Satisfied

2,388	Confirmed
2,353	Confirmed
2,373	Confirmed
4,784	Confirmed
2,645	Confirmed
2,676	Confirmed
5,356	Confirmed
2,646	Confirmed
2,639	Confirmed
2,679	Confirmed
7,225	Confirmed
3,679	Confirmed
3,949	Confirmed
3,591	Confirmed
800	Confirmed
800	Confirmed
40,046	Confirmed
90,629	

APPENDIX F: DUCT SIZING

			Room Airflow (CFM)	Duct Airflow (CFM)	Duct Length (ft)	Friction Loss	Duct Velocity	Duct Size
Duct A				1407.9	140.0	0.28	1300	13x12
	500	Perimeter Open Office	1,407.9	1407.9	140.0	0.28	1300	13X12
Duct B								
	508	Private Office	167.9					
	509	Private Office	165.5					
	510	Private Office	166.8	1,398.2	70.0	0.15	1300	13x12
	511	Executive Office	336.6	1,390.2	70.0	0.15	1300	12X12
	512	Copy Room	188.5					
	513	Private Office	186.4					
	514	Server Room	186.5					
Duct C				1,407.9	140.0	0.3	1300	13x12
	500	Perimeter Open Office	1,407.9	1,407.5	140.0	0.5	1300	19/12
Duct D								
	519	Private Office	262.8					
	520	Private Office	257.4					
	521	Private Office	246.7	1,728.5	70.0	0.15	1300	13x12
	515	Copy Room	186.5		70.0	0.15	1300	
	516	Private Office	186.0					
	517	Private Office	189.1					
	518	Executive Office	400.0					
Duct E								
	500	Open Office	500.0					
	501	Elevator Lobby	1,294.6	2,005.7	65.0	0.11	1300	17x12
	501A	Telecom	52.6	2,005.7	03.0		1300	
	501B	Electrical	50.4					
	504	Stair 2	108.1					
Duct F								
	500	Open Office	500.0					
	502	Stair 1	94.5					
	502A	Stair 1 Vestibule	82.7	1,302.5	110	0.25	1300	11x12
	503	Service Lobby	31.7					
	522	Conference	296.7					
	523	Conference	296.9					
Direct Su								
		Open Office	7,447.3					
	507	Fan Room	172.7					

between panels.

The duct sizing was vital to clash detection and integration. The supply ducts could not be any taller than 13 inches because the raised access flooring is only 14 inches off of the slab. Therefore, the ducts needed to be wider in many cases, but still had to fit within the 24 inches

APPENDIX G: WATER USAGE

Level	Men's Toilets	Women's Toilets	Urinals	Faucets
B4	1	3	2	6
B3	0	0	0	0
B2	0	0	0	0
B1	0	0	0	0
L01	1	1	0	2
L02	1	1	0	0
L05-L30	50	100	50	100
TOTAL	53	105	52	108

Rain Water Collection													
	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Annual
Rainfall (in)	4.50	4.61	3.26	1.46	0.70	0.16	0.00	0.06	0.21	1.12	3.16	4.56	23.80
Collection Capacity	35,882	36,759	25,994	11,642	5,582	1,276	0	478	1,674	8,931	25,197	36,360	189,774

	Water Use (Baseline)								
	# of Units	Gallons Per Flush	Building Occupants	Occupant Uses/Day	FTE		Yearly Use (Gal/Unit)	Total Use (Gal/Month)	
Toilet - Men	53	1.6	712.5	1	712.5		1,140	5,035	
Toilet - Women	105	1.6	712.5	3	2,137.5		3,420	29,925	
Urinal	52	1.0	712.5	2	1425		1,425	6,175	
Total Non-Potable								41,135	
		Gallons Per Minute				Total Uses (min)			
Faucet	108	0.5	1425	3	4275	2137.5	1,069	9,619	
TOTAL								50,754	

	Water Use (Proposed)								
	# of Units	Gallons Per Flush	Building Occupants	Occupant Uses/Day	FTE		Yearly Use (Gal/Unit)	Total Use (Gal/Month)	
Toilet - Men	53	1.0	712.5	1	712.5		713	3,147	
Toilet - Women	105	1.0	712.5	3	2,137.5		2,138	18,703	
Urinal	52	1.0	712.5	2	1425		1,425	6,175	
Total Non-Potable								28,025	
		Gallons Per Minute				Total Uses (min)			
Faucet	108	0.5	1425	3	4275	2137.5	1,069	9,619	
TOTAL								37,644	

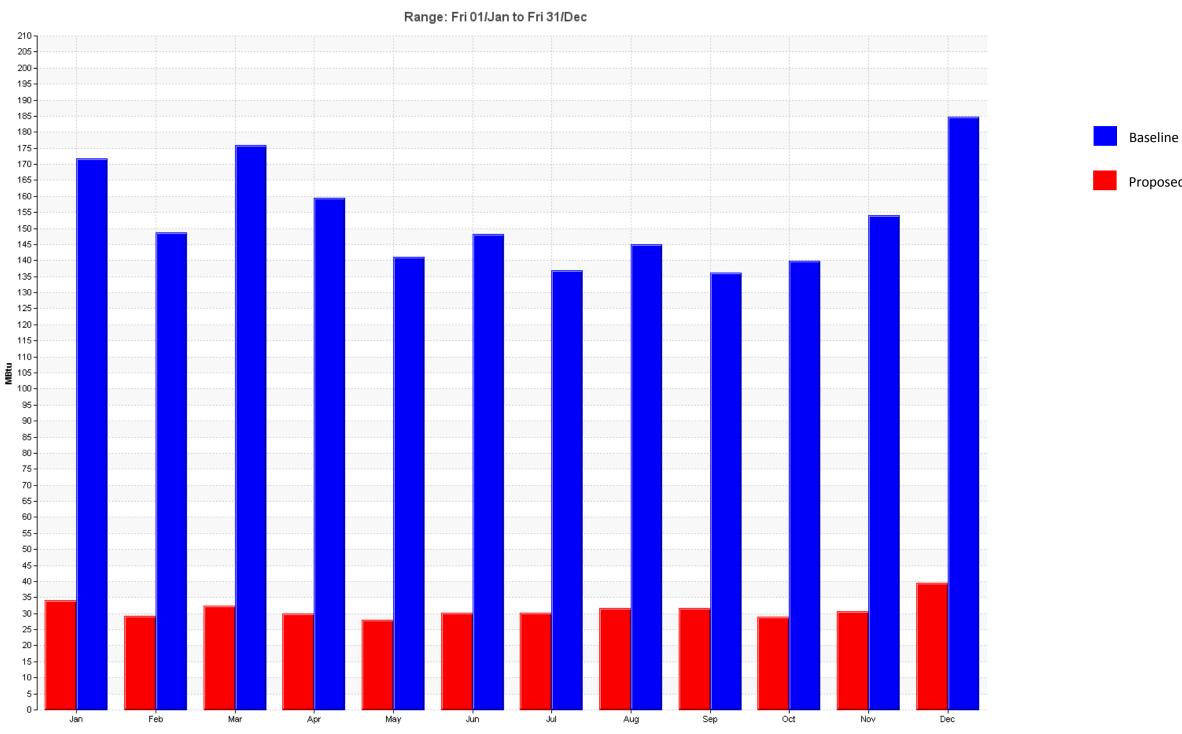
The water reduction calculations were based off of LEED 2009 water reduction guidelines. The baseline values were those set forth by the LEED guidelines, and the proposed values were taken from possible manufacturers' websites. A building full-time equivalent occupancy of 1,425 was assumed based on ASHRAE occupant density values.

The rainwater collection values were calculated based on a 15,990 sq ft. roof area. Monthly precipitation levels were found from the National Weather Service.

Total Use (Gal/ Year)
60,420
359,100
74,100
493,620
115,425
609,045
Total Use
(Gal/ Year)
37,763
224,438
74,100
336,300

115,425	
451,725	

APPENDIX H: ENERGY USE



We modeled our building in IES and were able to calculate our energy use. As can be seen in the graph above, energy use decreased significantly from the baseline every month.

Proposed

APPENDIX I: LEED

WATER EFFICIENCY 6/10

Prerequisite 1: Water Use Reduction

Water demand reduced by 26% (see Appendix G)

WE Credit 2: Innovative Wastewater Technologies

Option 1: Water use reduced by 56% (Appendix G and Table 9 in report) through rainwater collection and demand reduction

WE Credit 3: Water Use Reduction

Water use reduced by 56% (Appendix G and Table 9 in report)

ENERGY & ATMOSPHERE 26/35

Prerequisite 1: Fundamental Commissioning of Building Energy Systems

Budgeted for a commissioning authority

Prerequisite 2: Minimum Energy Performance

Option 1: Whole Building Energy Simulation – Used IES to simulate and achieved a savings of 53% (see Table 7 in report)

Prerequisite 3: Fundamental Refrigerant Management

Designed chilled water system

EA Credit 1: Optimize Energy Performance	19 Points
Achieved an overall energy use savings of 53% (see Table 7 in report)	
EA Credit 4: Enhanced Refrigerant Management	2 Points
Option 1: Did not use refrigerants	
EA Credit 5: Measurement and Verification	3 Points
Option 1: Budgeted for a measurement and verification plan	
EA Credit 6: Green Power – 35% from renewable sources	2 Points

Option 1: Determine Baseline Electricity Use – We used IES to determine the annual electricity demand of the site

4 Points

2 Points

INDOOR ENVIRONMENTAL QUALITY 4/15

IEQ Prerequisite 1: Minimum Indoor Air Quality Performance

Met both Case 1 and Case 2 because our building utilizes both natural and mechanical ventilation

IEQ Prerequisite 2: Environmental Tobacco Smoke (ETS) Control

Option 1: We are prohibiting smoking on the entire property, inside and outside

IEQ Credit 1: Outdoor Air Delivery Monitoring	1 Point					
Case 1 and Case 2: We have provided for CO ₂ for all spaces						
IEQ Credit 6.2: Controllability of Systems - Thermal Comfort 1 Point						
Because of our underfloor system, the occupants have control over the vent closest to their desks						
IEQ Credit 7.1: Thermal Comfort – Design	1 Point					
Our HVAC system was designed using ASHRAE Standard 55-2004						
IEQ Credit 7.2: Thermal Comfort – Verification	1 Point					
We had acted for a manitoring system						

We budgeted for a monitoring system

INNOVATION IN DESIGN 5/6

ID Credit 1: Innovation in Design

Path 1: Innovations in Design - Cogeneration, algae bioreactors

Path 2: Exemplary Performance – two incremental increases in EA Credit 1 (2 pts.), three incremental increases in WE Credit 3 (1 pt.)

TOTAL

41 POINTS

5 Points

APPENDIX J: DESIGN TOOLS

The design teams utilized a myriad of tool in order to analyze and develop the mechanical systems. The following tools are outlined below.



AUTODESK REVIT

- Duct Layout
- Visual System Modeling
- BIM



INTEGRATED ENVIRONMENTAL SOLUTIONS (IES)

- Load Calculation
- Energy Calculations
- System Analysis



AUTODESK CAD

• System layouts



MICROSOFT EXCEL

Design Calculations



AUTODESK INVENTOR

• Visual System Modeling



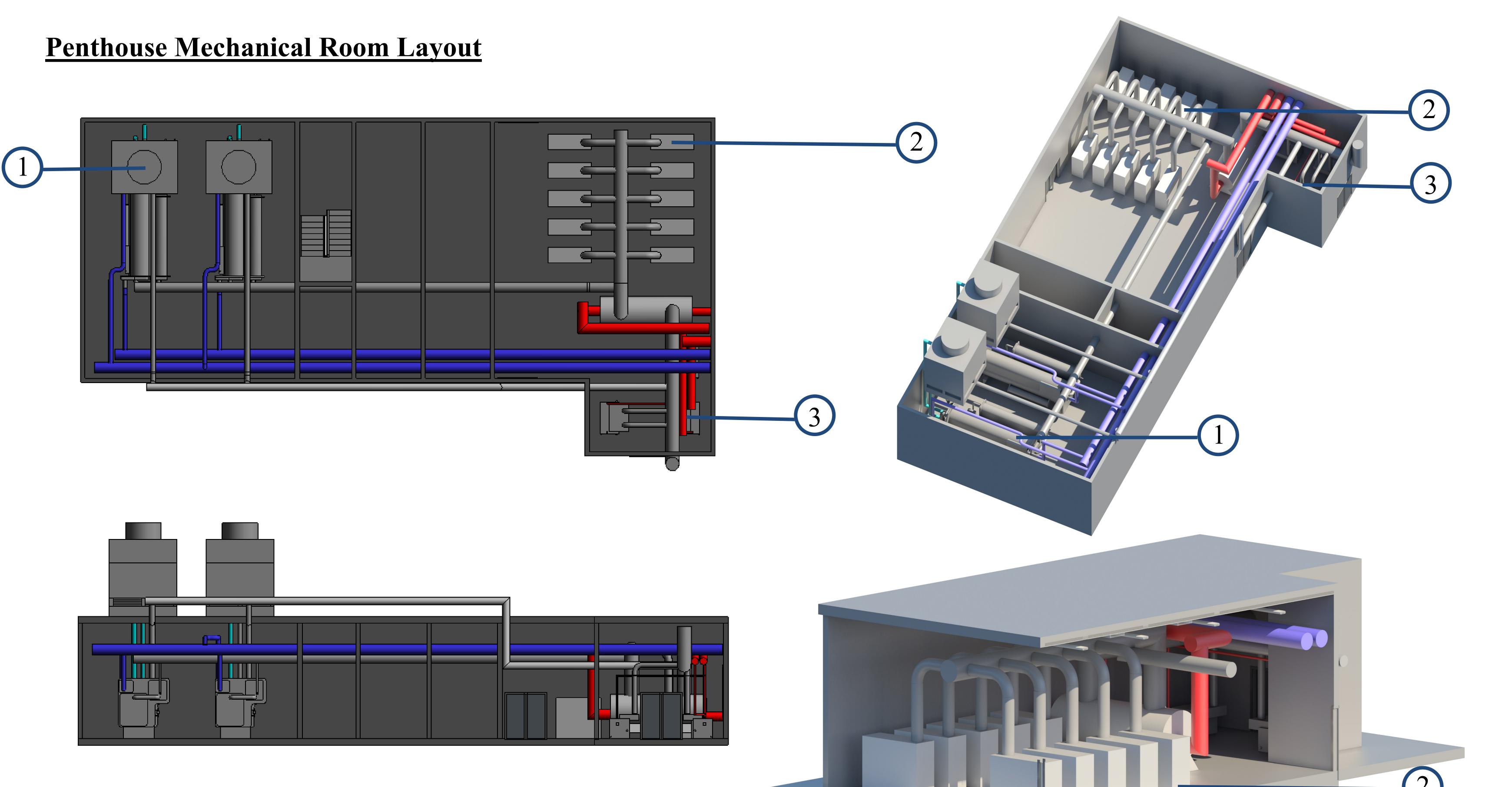
AUTODESK NAVISWORKS

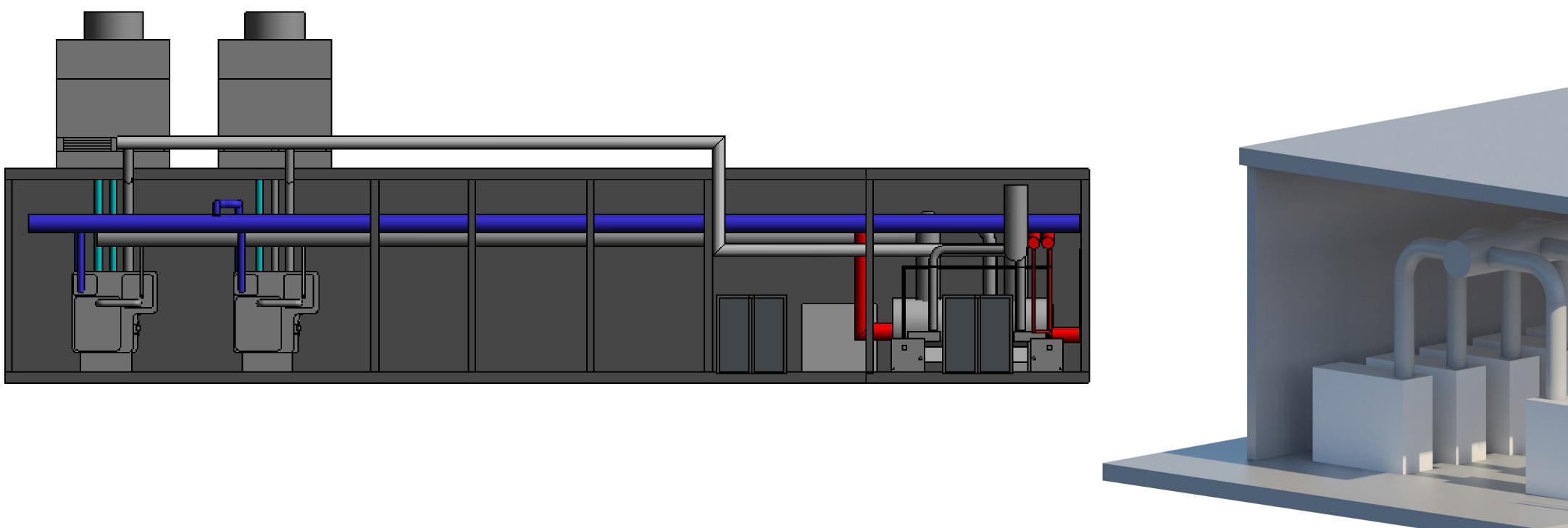
- BIM
- Clash Detection



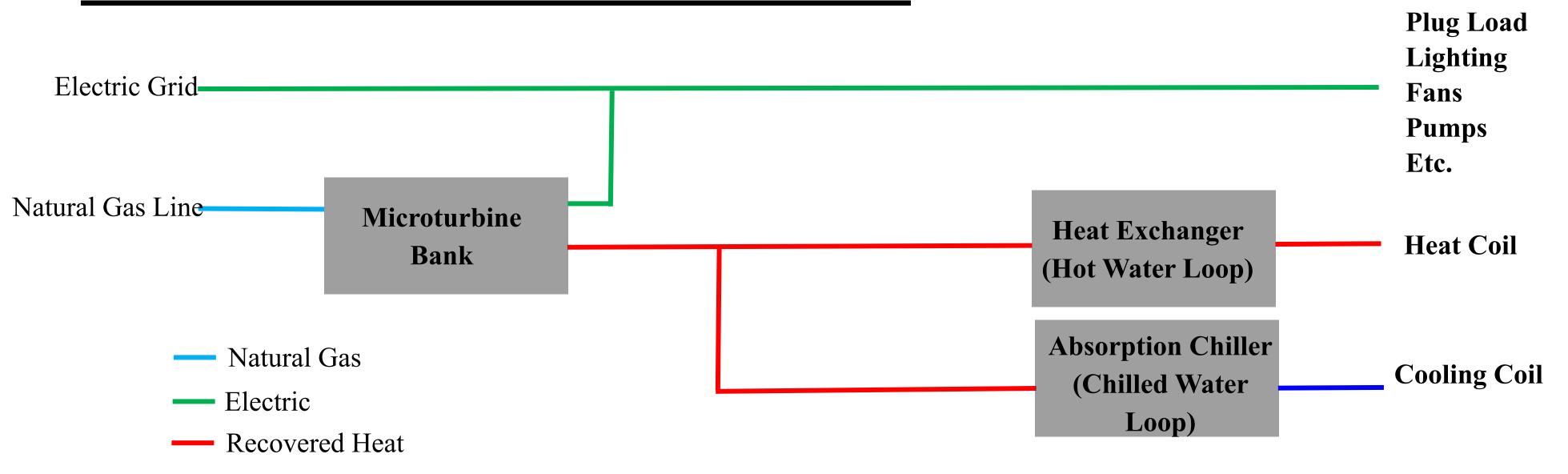
GOOGLE SKETCH UP

- Preliminary Design
- Model Creation Tool





Combined Heat and Power Schematic



2 3

Two 450 Ton Absorption Chillers

Ten 65 kW Microturbines (CHP System)

Three 750 MBH Natural Gas fired Boilers

Code

IBC 2009: Section 1015.3 Boiler Room:

In order to comply with the above code we had to ensure that "two exit access doorways" were placed in the Mechanical Penthouse Room. The exit doors are located on the north and south wall of the room along the western corridor.

Pent

M - 101



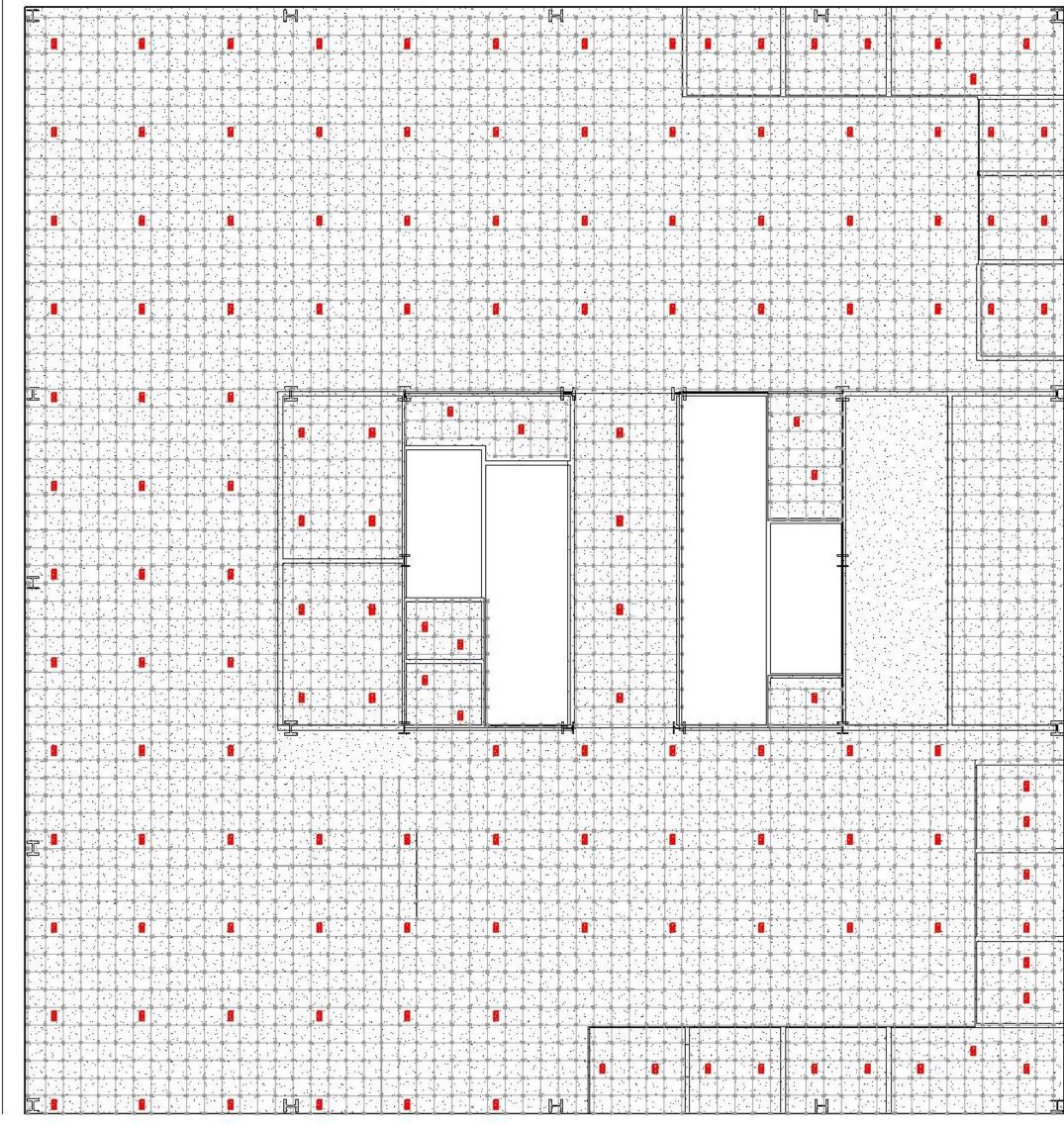
Mechanical

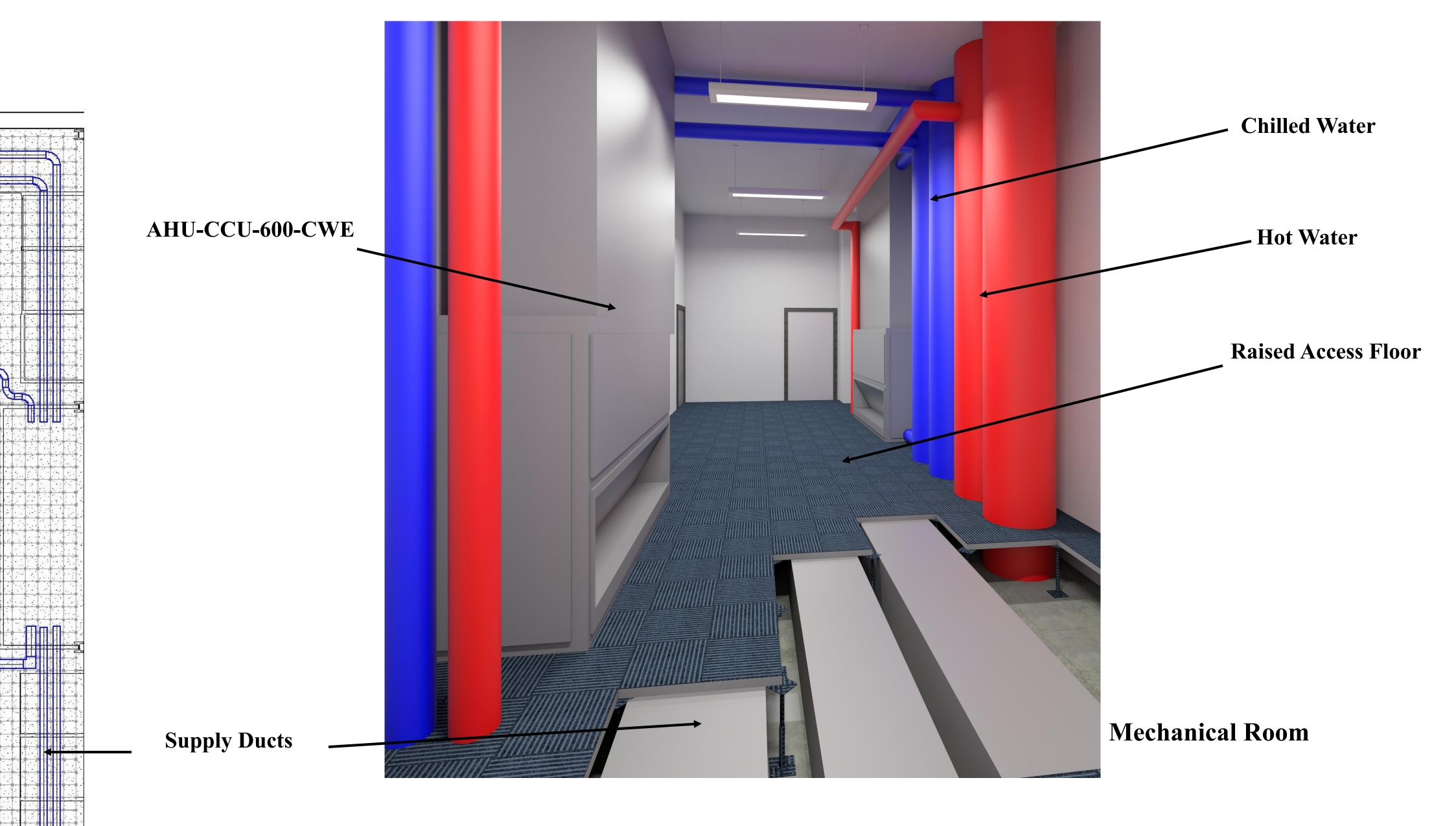
2014 Charles Pankow Foundation Annual Architectural Engineering Student Design Competition

	Description	Date
	AEI Team Numb 05-2014)er
nt	house Mechanica	l Room

Air Side Distribution Plan

T							1							1			1	1	1							1																		
									1												*			· .															1					
														+					+					· `. 									-		E		-	-		+				
							the second s							-																														
														1																	-												1	
												-				+		+	1				+		-		-				1		1										+	+
																	1	1			100																						1	1
											+															-															1			
-																		I					-							Ŧ												-		
								+	1					1	1		1		t																								1	
				-	_					-	-						+		+	+						-				-		-	-	-				-	-				+	-
								1						Ø			+		5	ŧ			*														ਮ					*		+
																+												_																
-											P									1				1	1				· · · · · · · · · · · · · · · · · · ·															
							_																	-		-										-								
						-						-											-		-										4- 	4								
				****													-																		*									•
					· · · · · ·				1								-													1														
-				Ļ					+					ļ	-		-													-														
																		•								:			П															
							+		+						+			1.1	1	1	1	i p				į					-													
																				ſ		-11 -11				. 1															. 2.2. 			
																		-																										
				-			1	-	-										+			-													Ē									
																							-									-	-		-		ſ			-		-	-	
																		-		-									Щ		14						T	4						
								1					 				-																											
																			-																						+			
										-					Ī	Ī		+		-	-		-				_							-			Ī					-	ł	
										t					1		1	1																										
									+										+										_									-				-		
									1					1							-										-		-									1	1	1
														+		1					· · · ·																							1
																	Ŧ																											
																1							-																					
						-			+			-		+	••••				-	-							Ē						-						-		-			-
			4						1					1		1			1		1									E	· •		+				+	+	-				*	+
<u> </u>					E																							+																
	-	1. T	T	1.		31	4		T	1-	TIR	Jn .		1		1.	1	1	1 4	1	L	T	T	·	FR	Л .				Ī	1	1	15	1.8		: HI	T	D D	T	1		T	T:	1

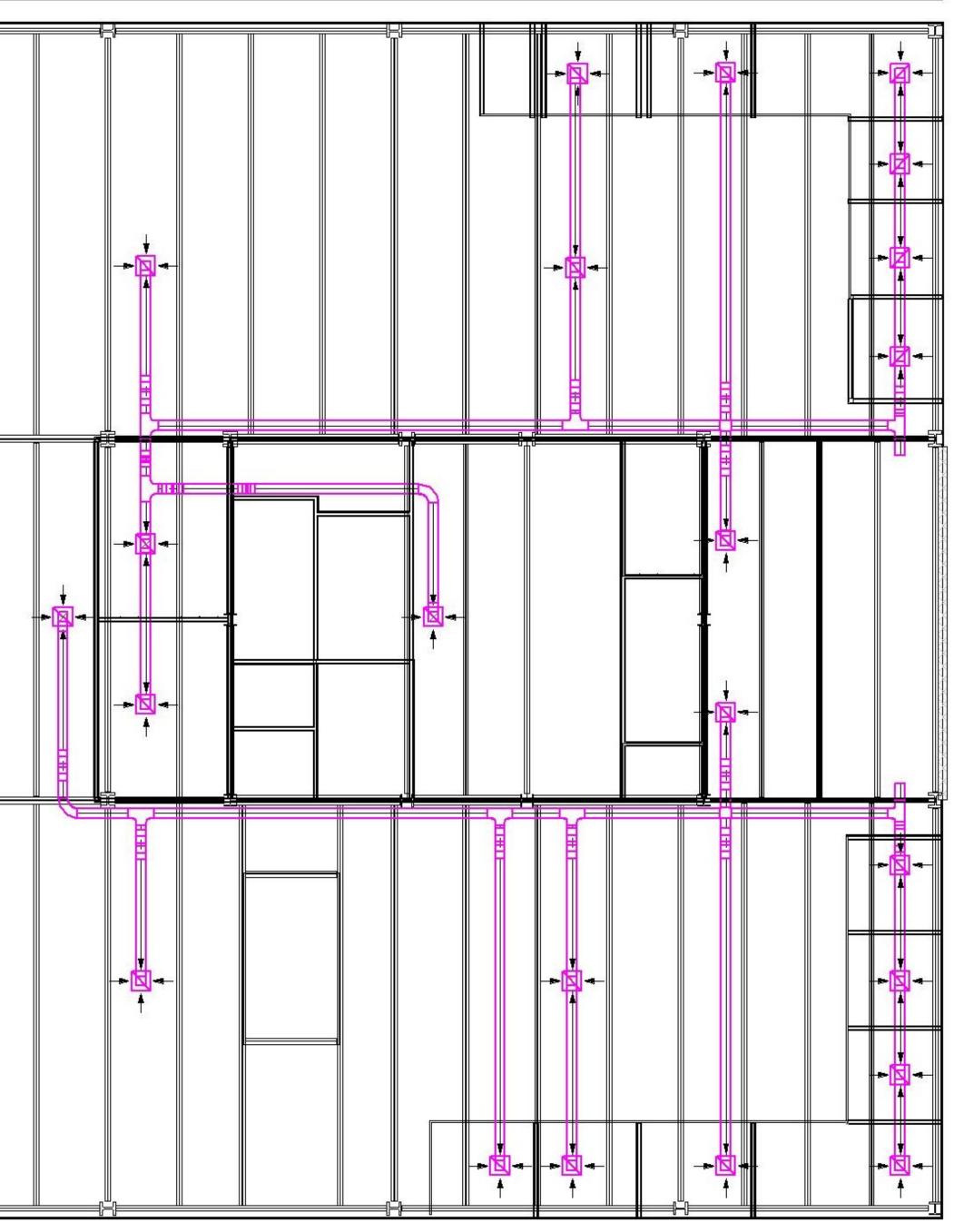




Supply Duct Plan

Floor Diffusers

Return Duct Plan



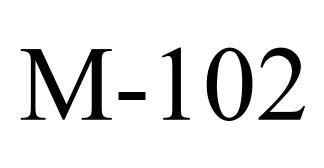


Mechanical

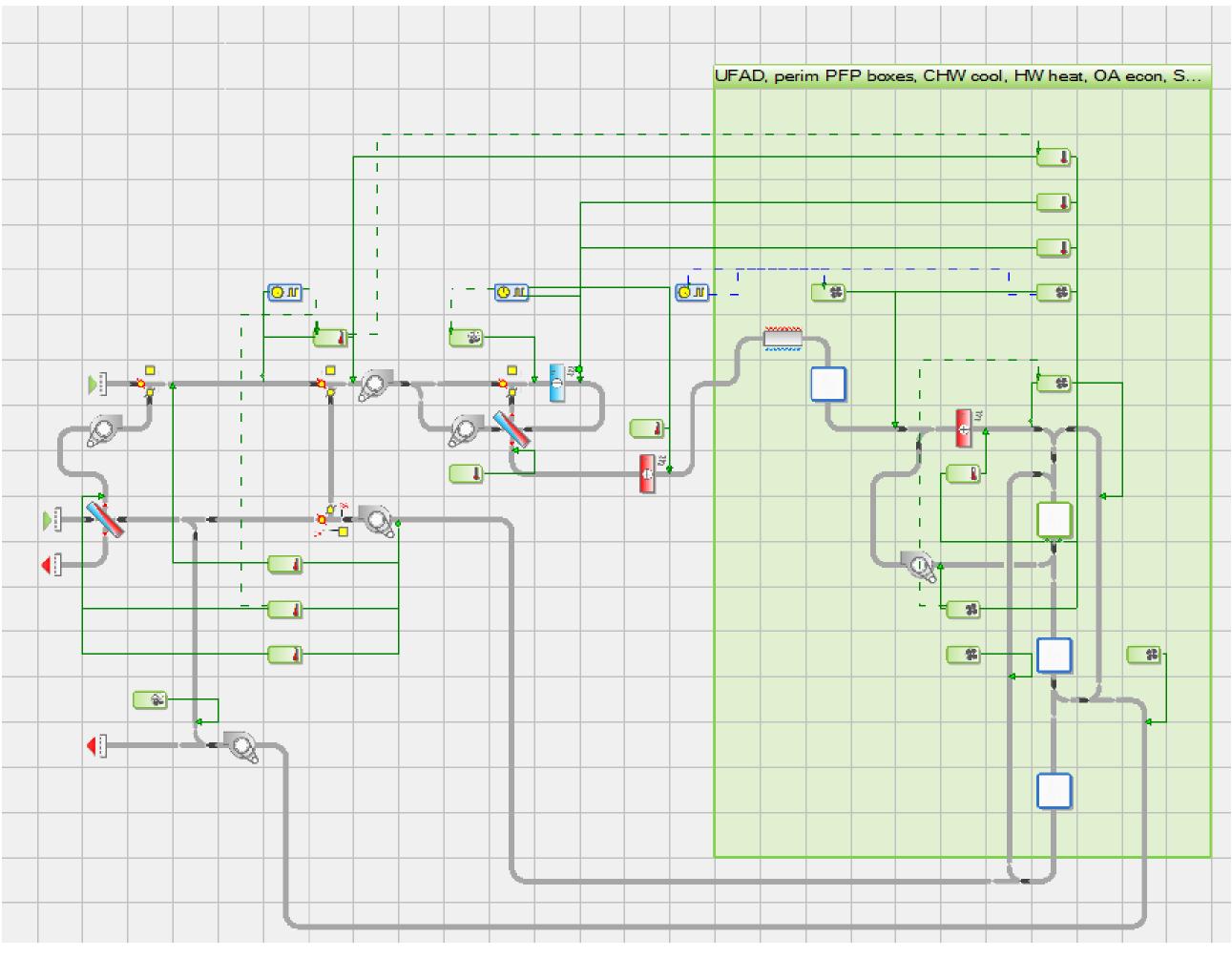
2014 Charles Pankow Foundation Annual Architectural Engineering Student Design Competition

Description	Date
AEI Team Num 05-2014	ber

Air Side Distribution Plan

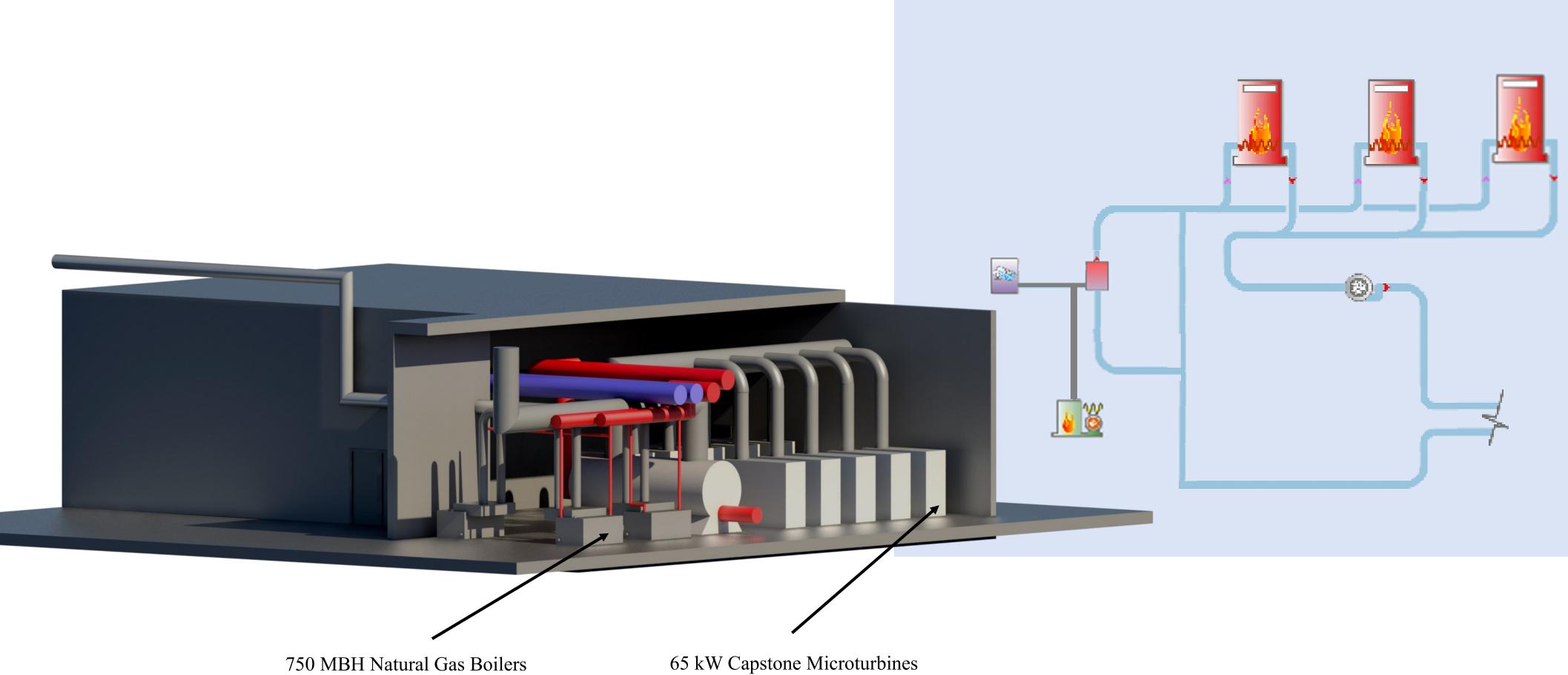


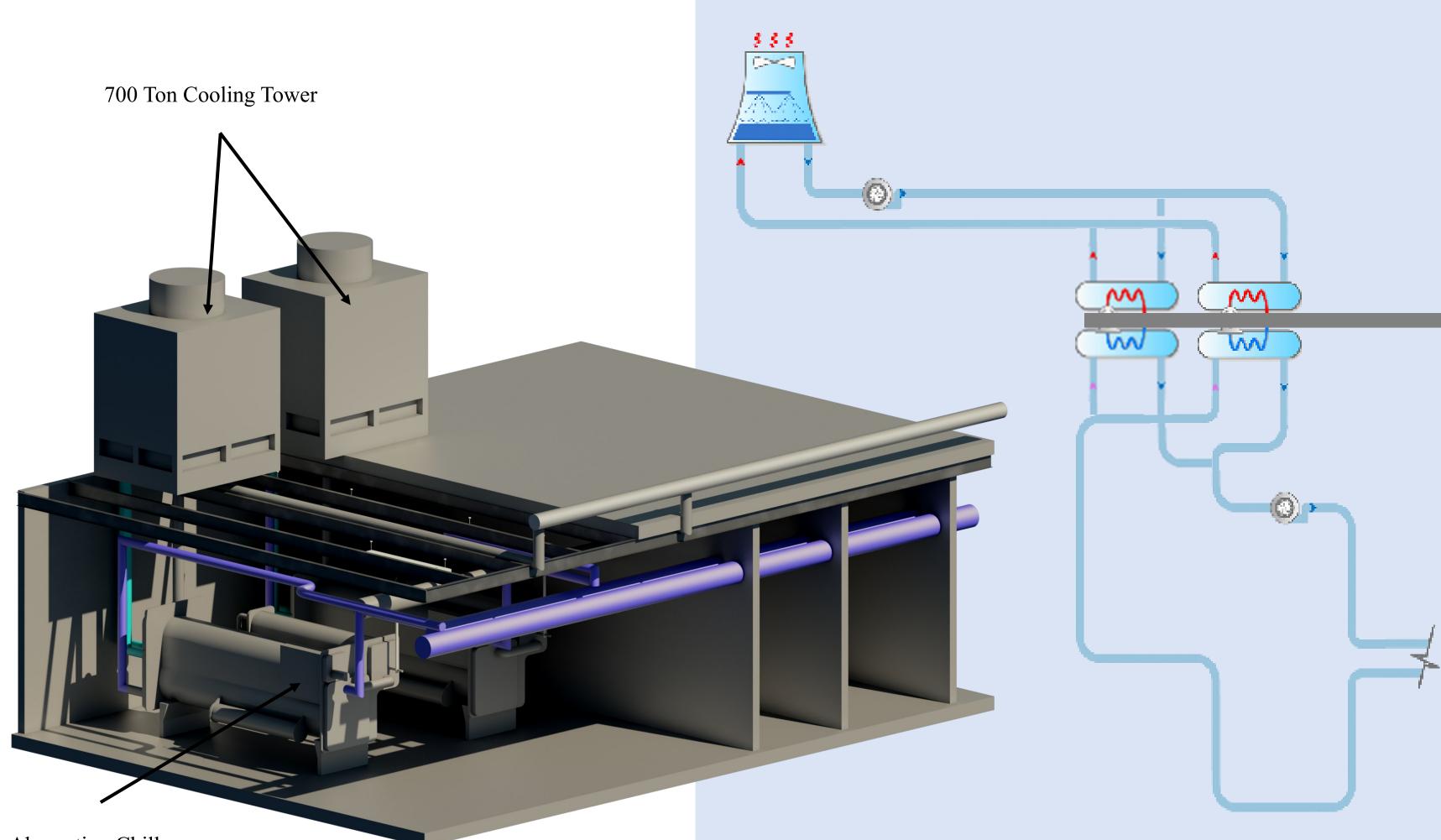
Air Distribution and Hot/Chilled Water Loops



Underfloor Air Distribution System (UFAD)

UFAD: UFAD supply air plenum; parallel fan-powered reheat boxes; occupied and stratified zones; re-mixing path and control to de-stratify zone when stirred by fan-powered reheat box. Enthalpy wheel to help with humidity control.





450 Ton Absorption Chillers

Hot Water Loop

Chilled Water Loop

No

Images for the hot water and chilled water loop were taken from IES's Apache HVAC Systems Simulation Interface.

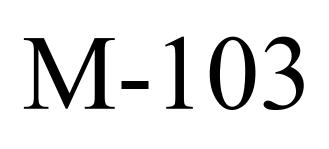


Mechanical

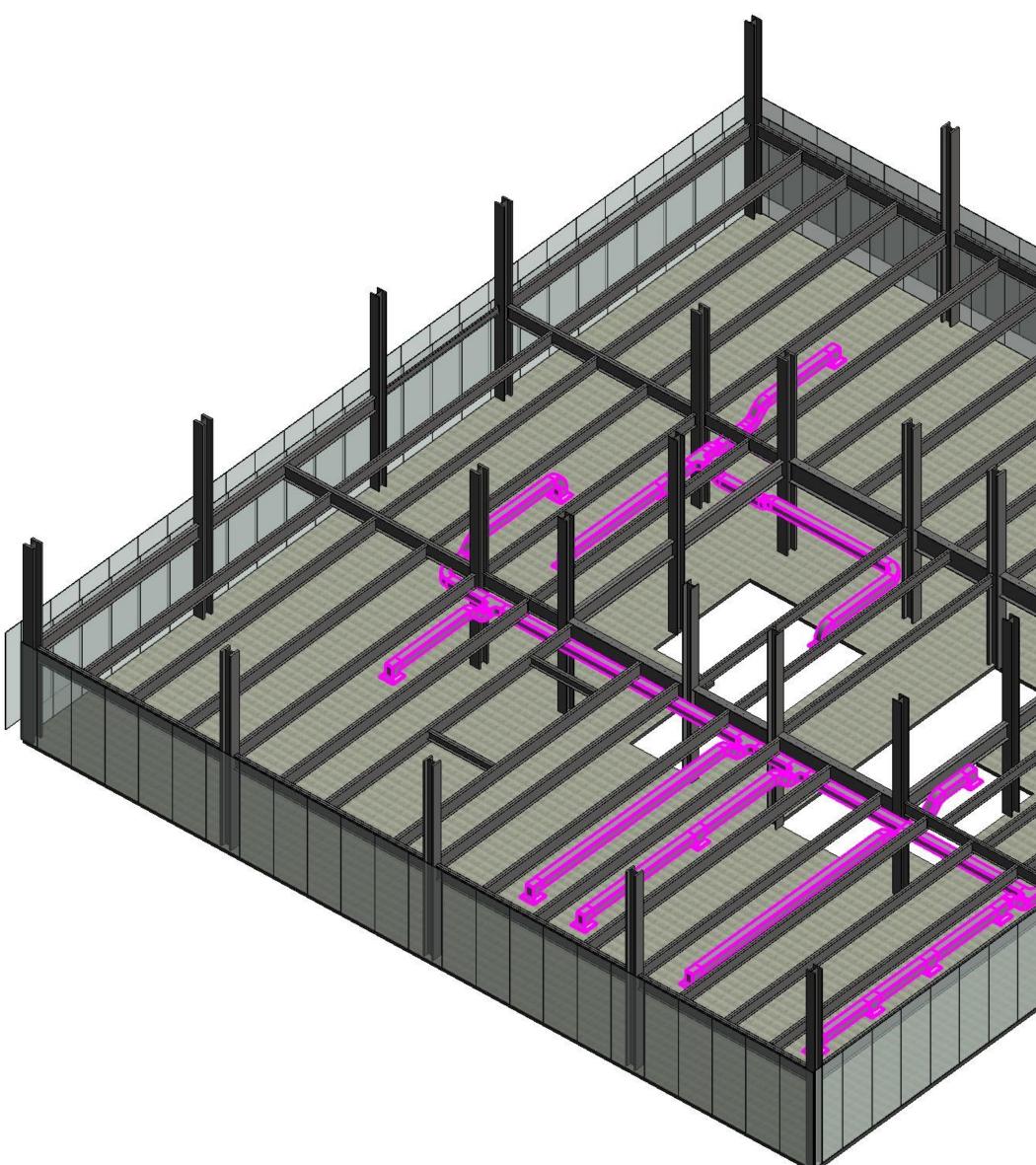
2014 Charles Pankow Foundation Annual Architectural Engineering Student Design Competition

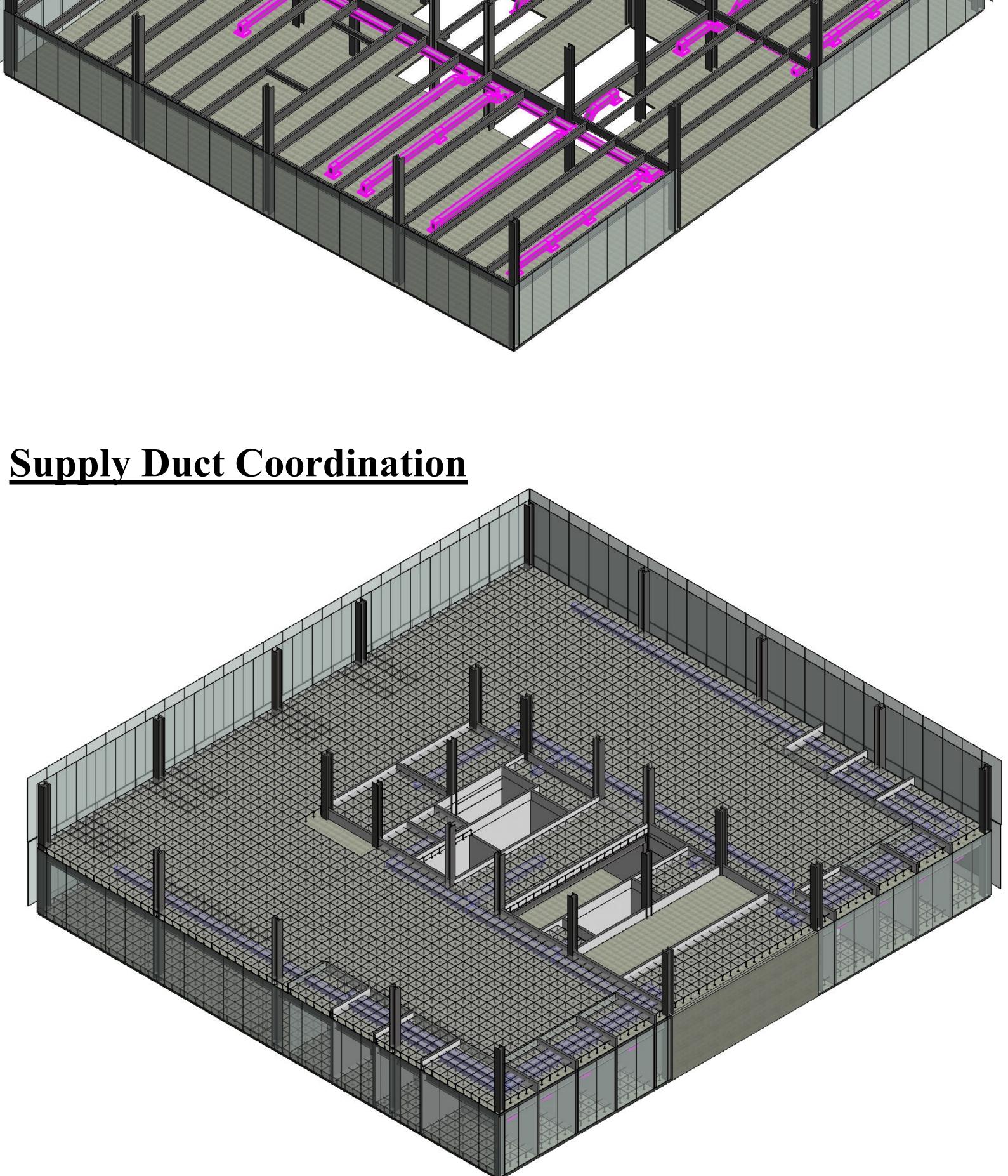
Description	Date
AEI Team Numb	ber
05-2014	

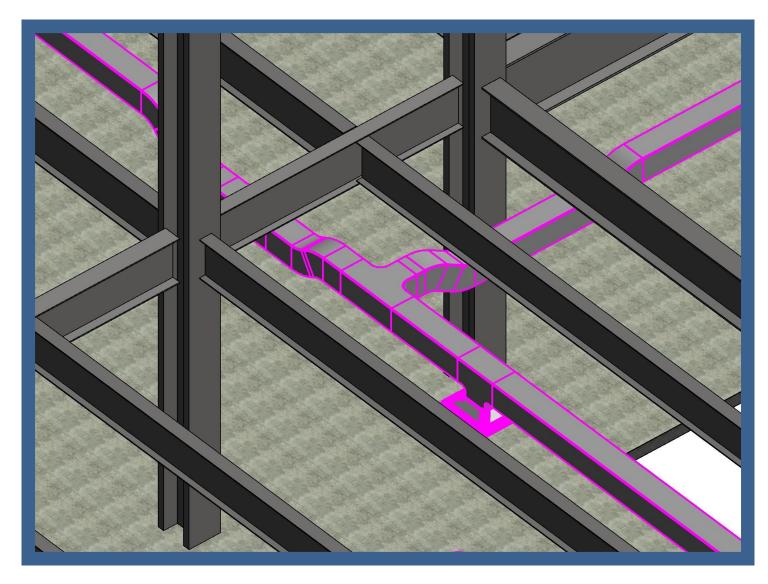
Air Distribution and Water Loops



Return Duct Coordination

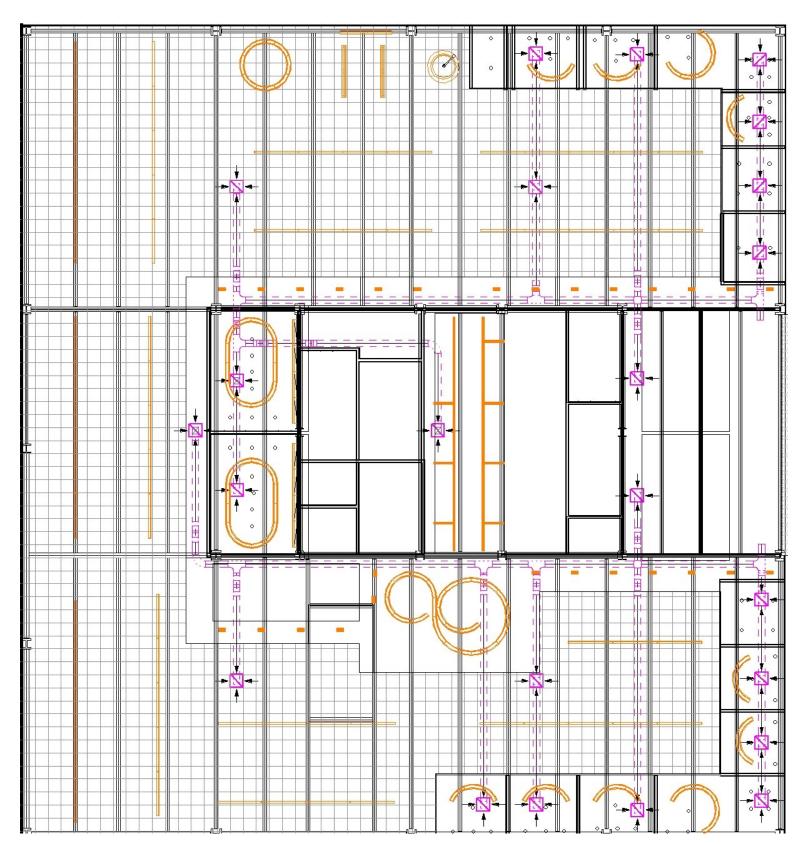


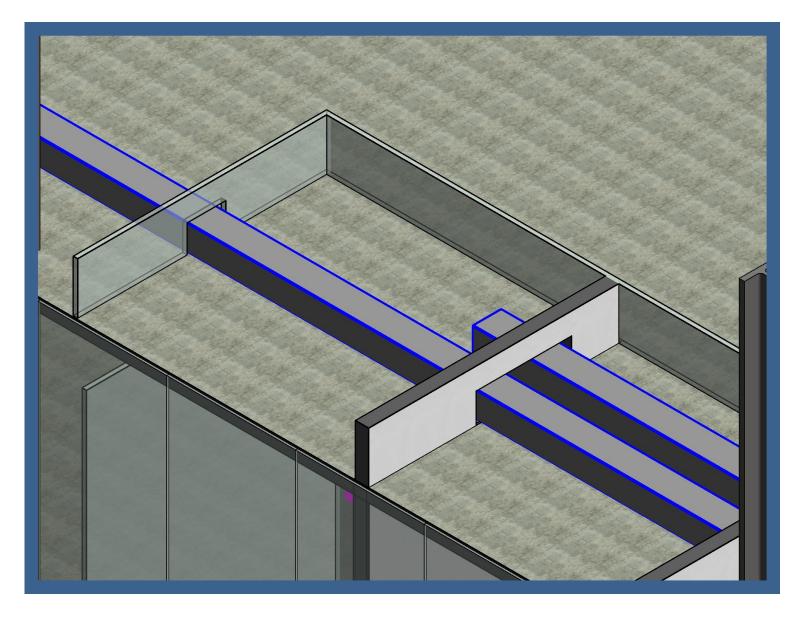




Structural Members

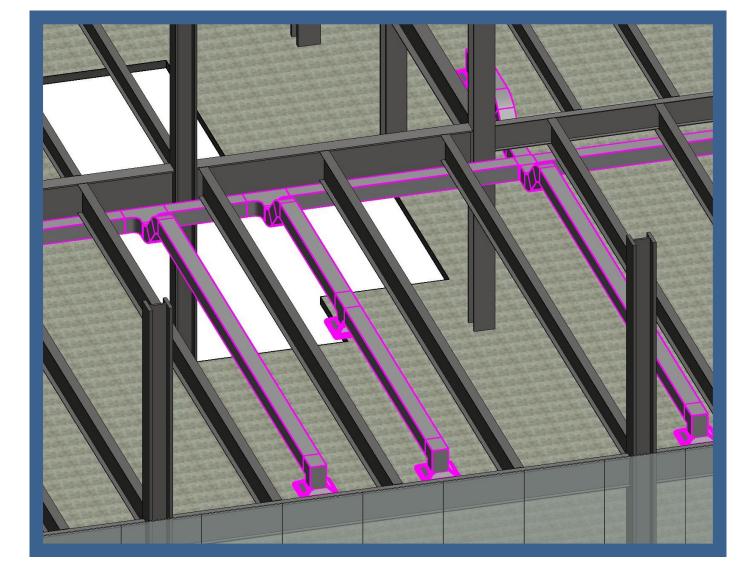
Because we do not have a drop ceiling in the majority of the space, most of the duct had to be run between beams as seen in the image to the left. This also meant that in some areas the duct did need to be dropped below the beams (and hidden with a bulkhead) so a great deal of time and consideration went into choosing the correct locations and coordinating transitions as can be seen above.





Wall Cutouts

Because the duct needed to run from room to room and the walls extend down to the slab, cutouts were added to walls where needed to allow for the duct.

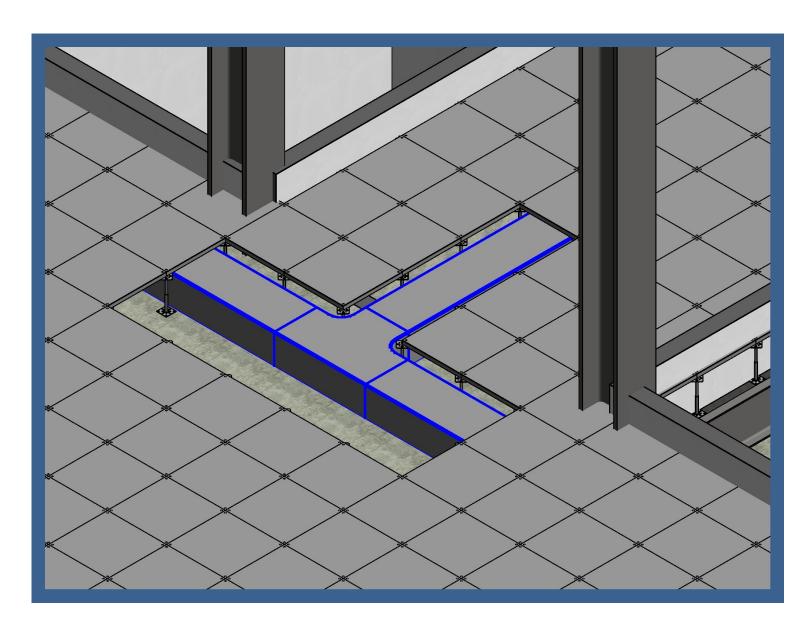


Return Diffuser Coordination

The diffusers needed to be placed in such a pattern that they did not clash with any of the lighting in the space. In addition, we placed the diffusers in the middle of acoustical tiles to ensure a consistent look across the space. The duct was not a concern because it was above the ceiling.



Diffusers



Raised Access Floor

When designing the duct system, we needed to make sure that all duct fit within the 24" x 24" x 14" space created by each panel of the raised access flooring.

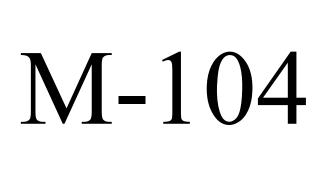


Mechanical

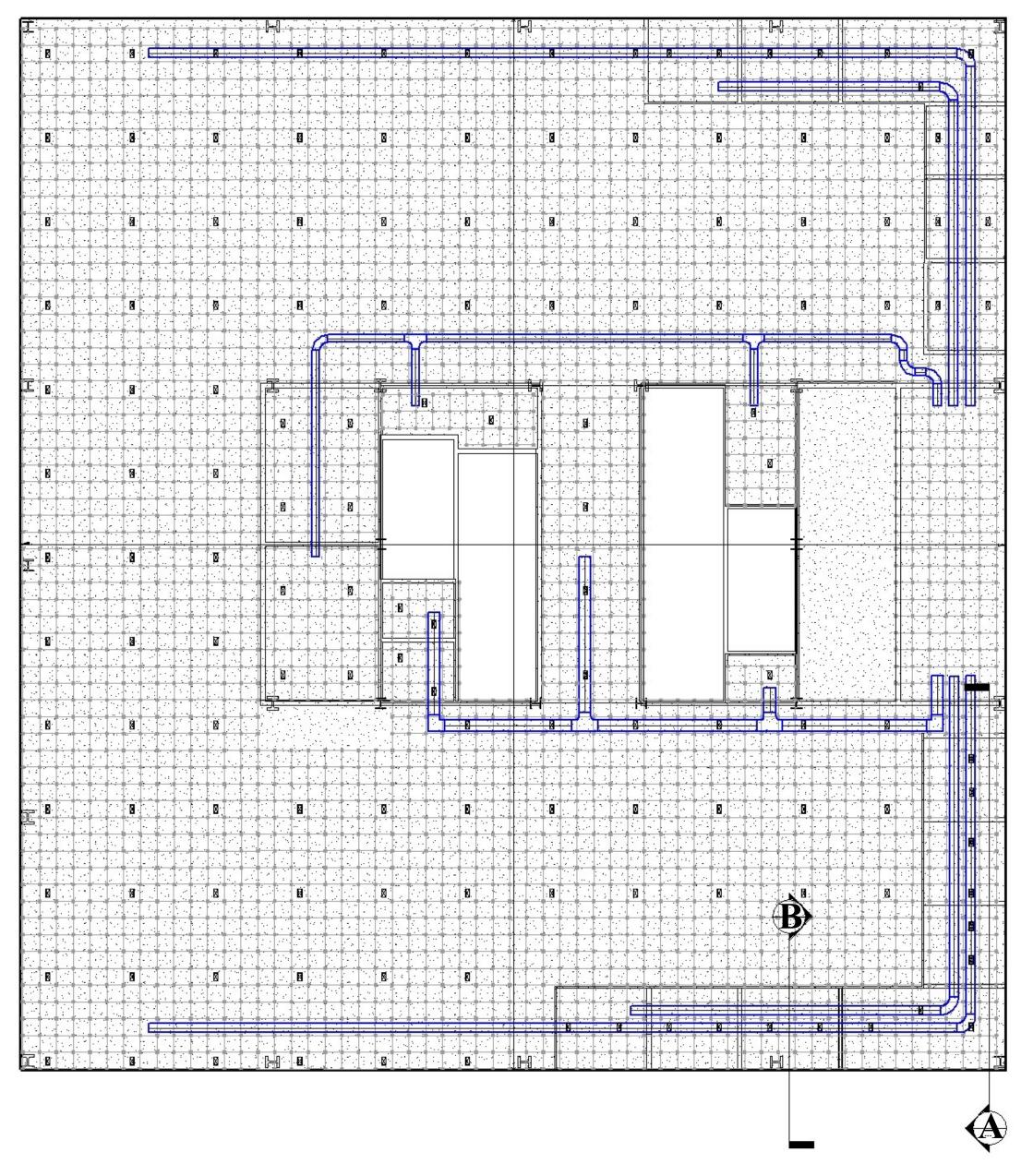
2014 Charles Pankow Foundation Annual Architectural Engineering Student Design Competition

Description	Date
AEI Team Nun	ider
05-2014	

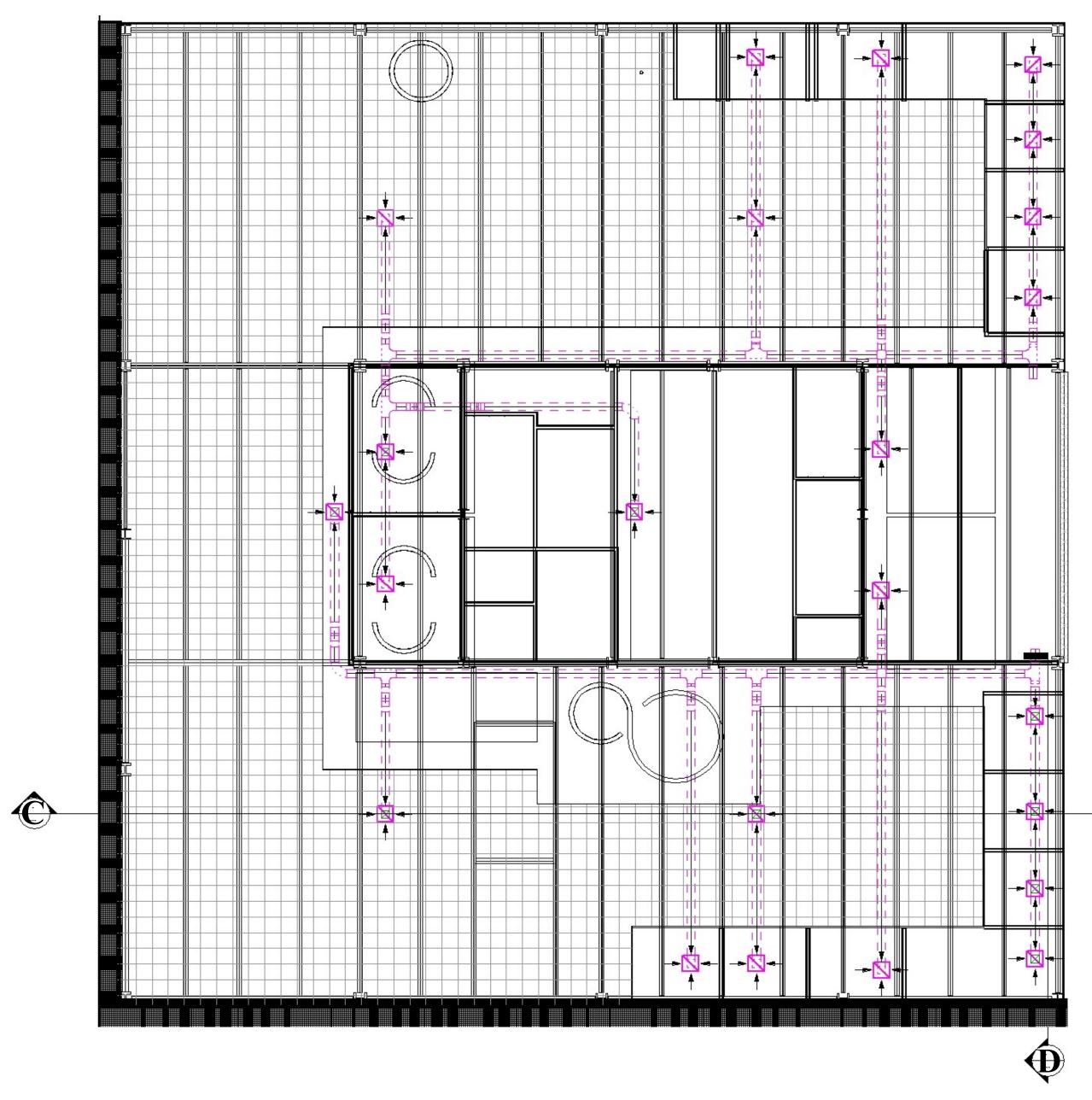
3D Duct Coordination

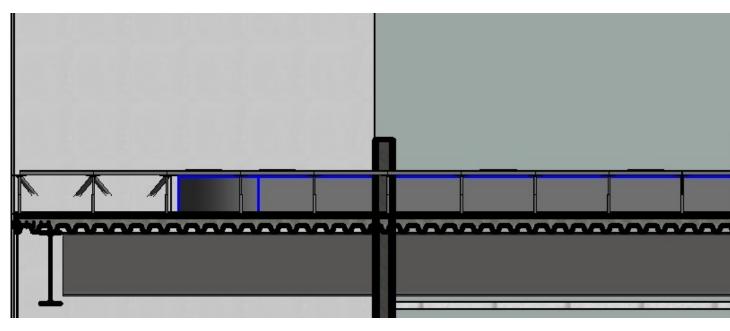


Supply Duct Sections

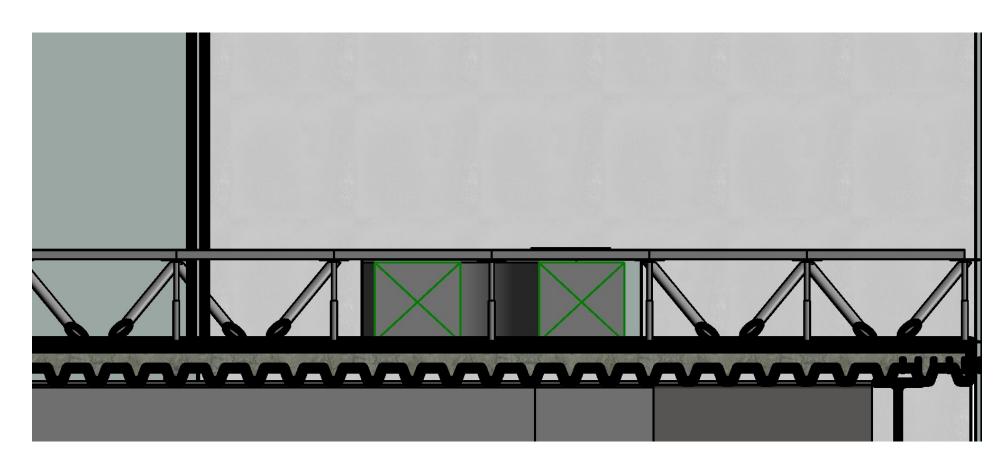


Return Duct Sections

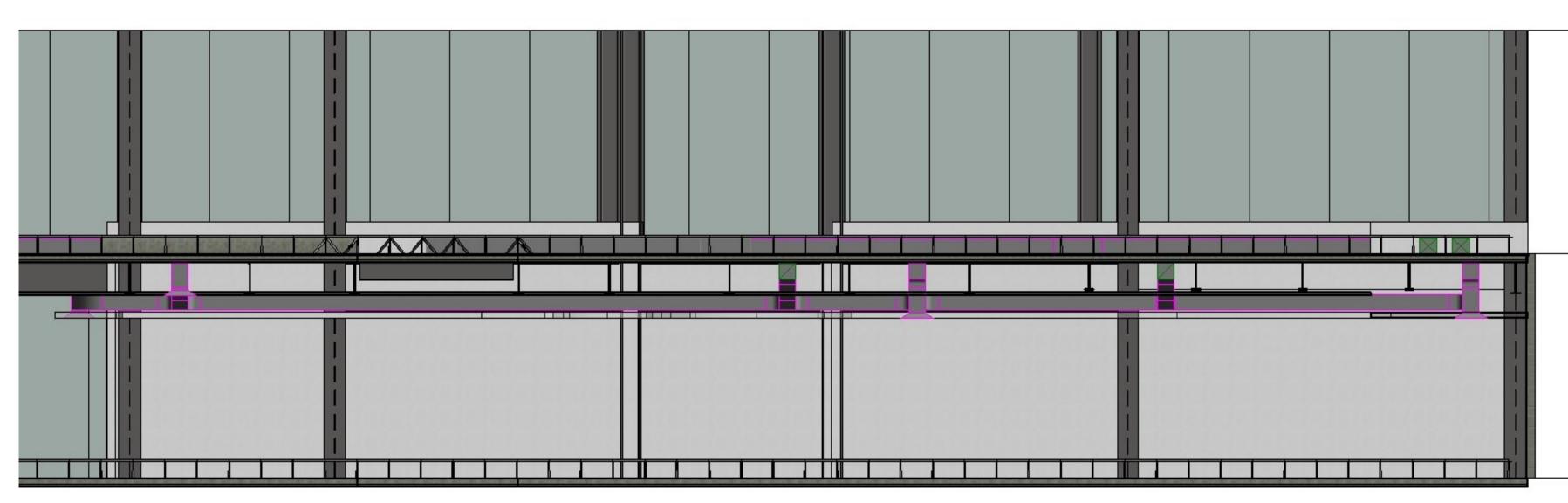




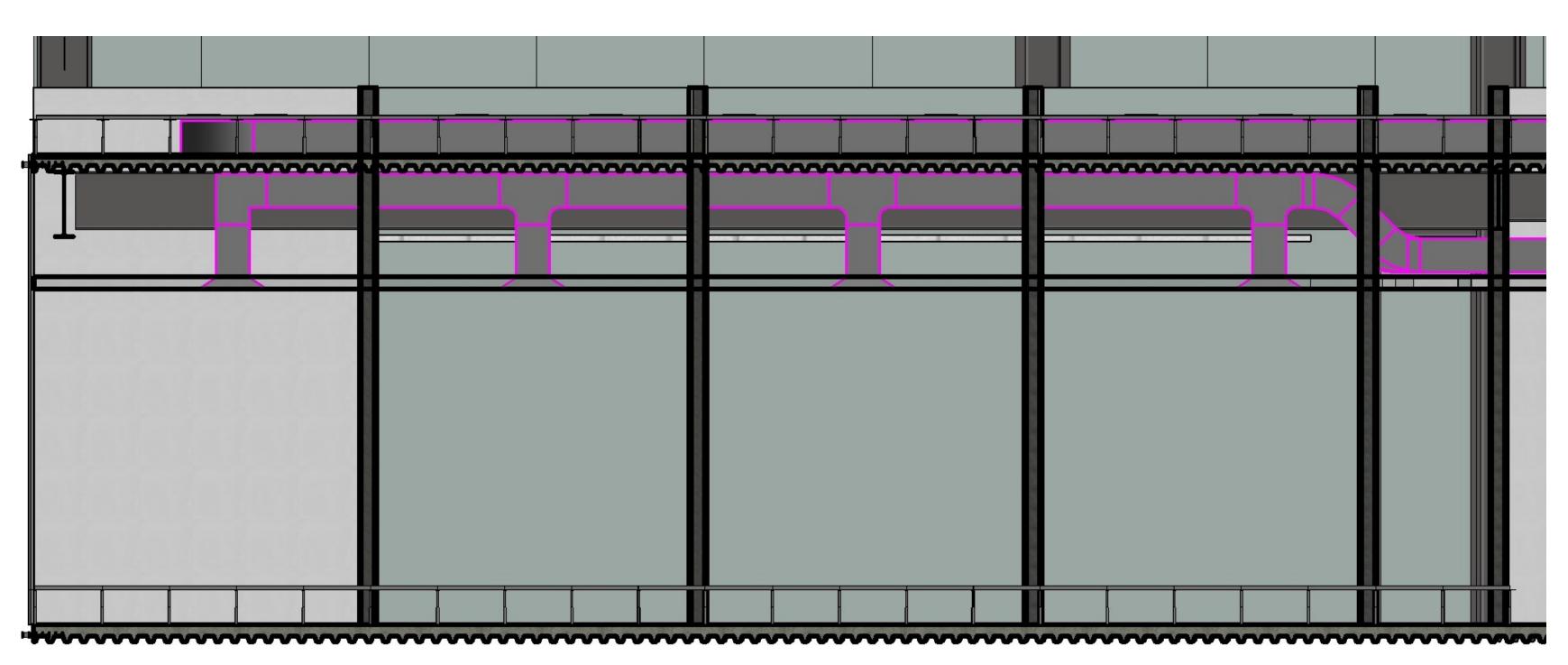
Section A



Section **B**



Section C



Section D

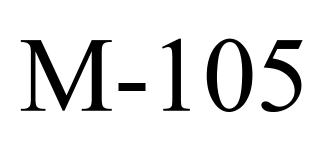


Mechanical

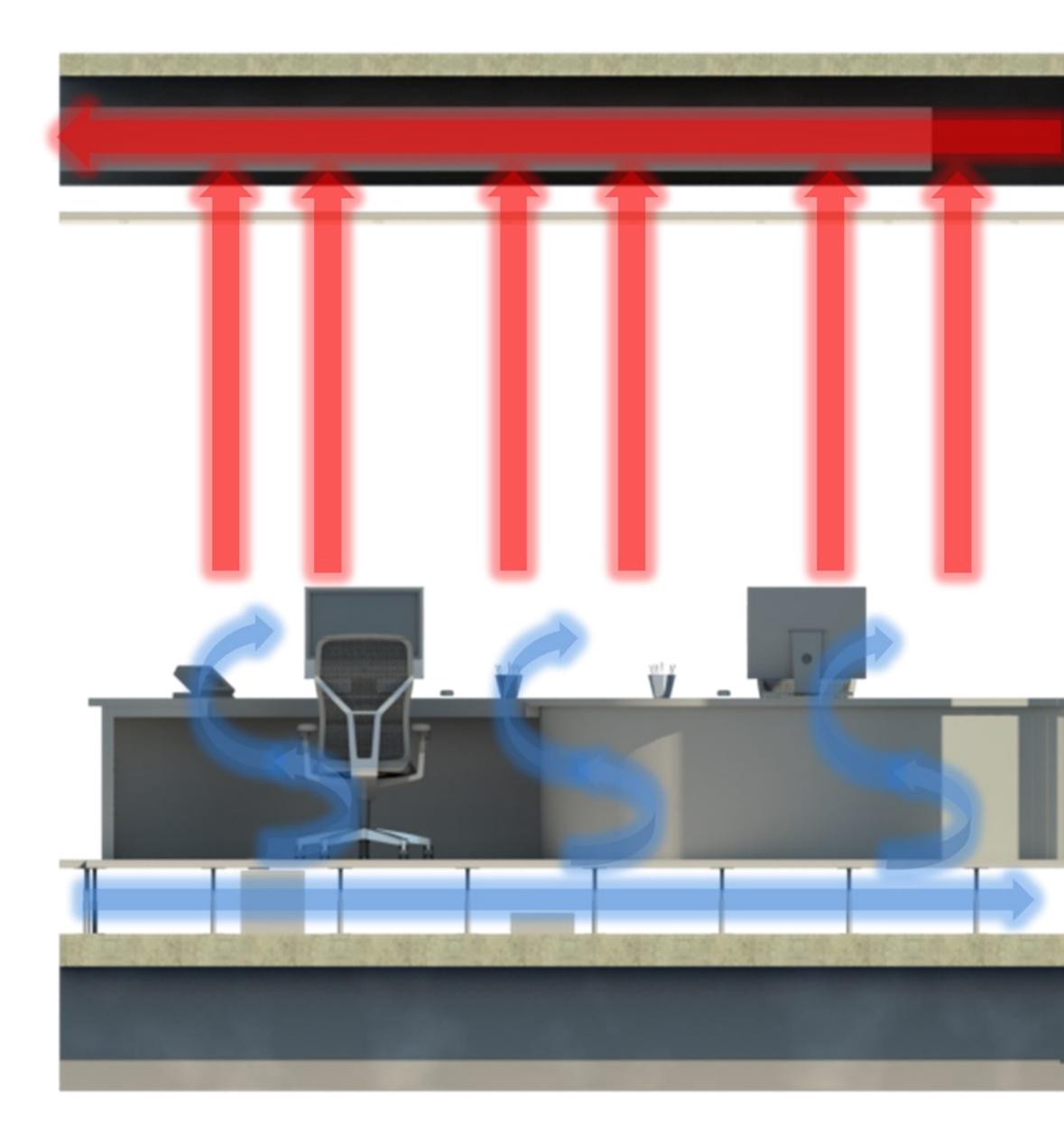
2014 Charles Pankow Foundation Annual Architectural Engineering Student **Design** Competition

Description	Date
AEI Team Num	ber
05-2014	

Duct Sections

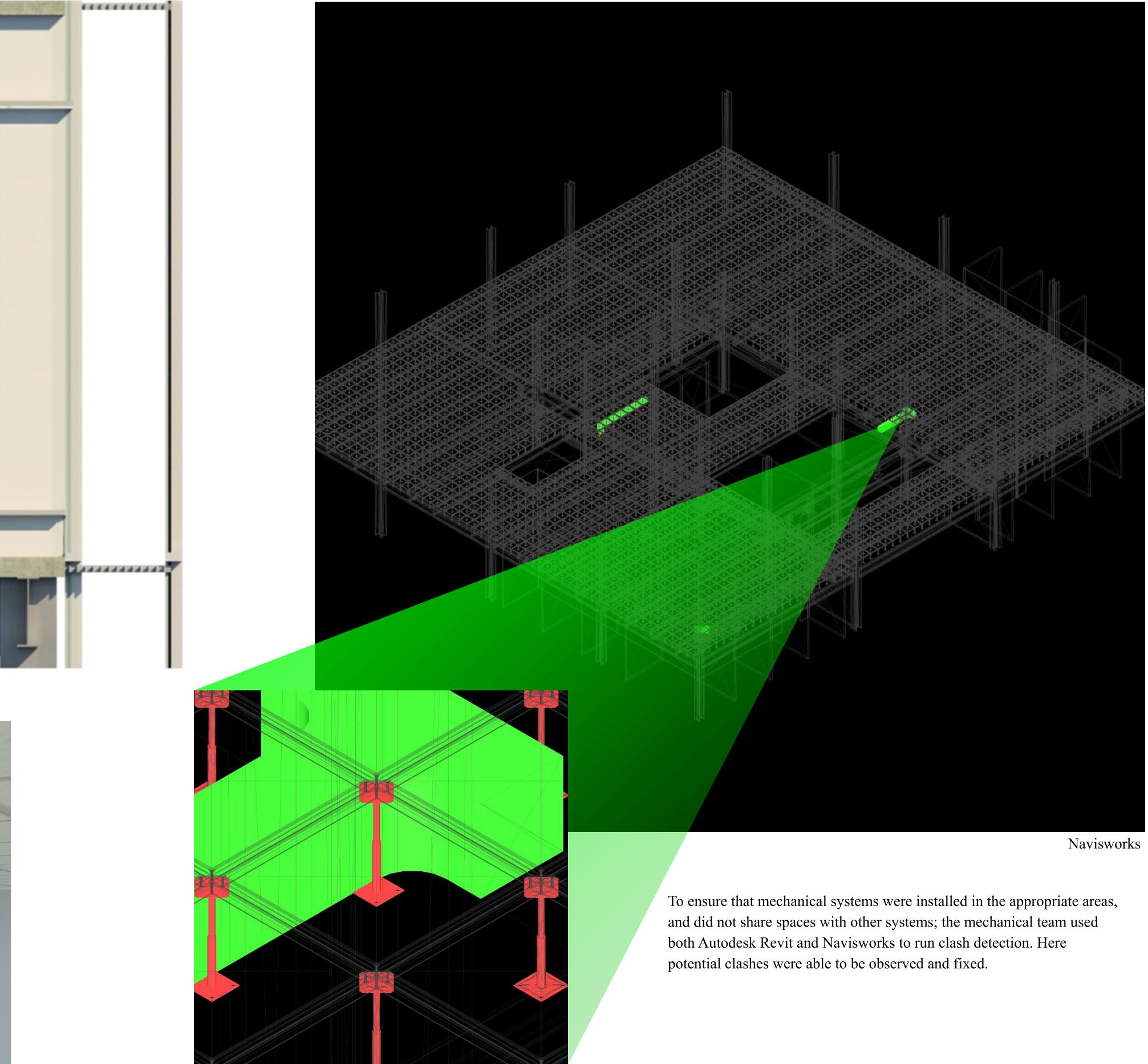


Underfloor Air Distribution Schematics





Underfloor Air Distribution Clash Detection



2 (4)

Raised Access Floor (RAF)

Data Cable Tray

3 Supply Air Duct

Seismic Bracing

5 Supply Diffuser

Autodesk Revit

5



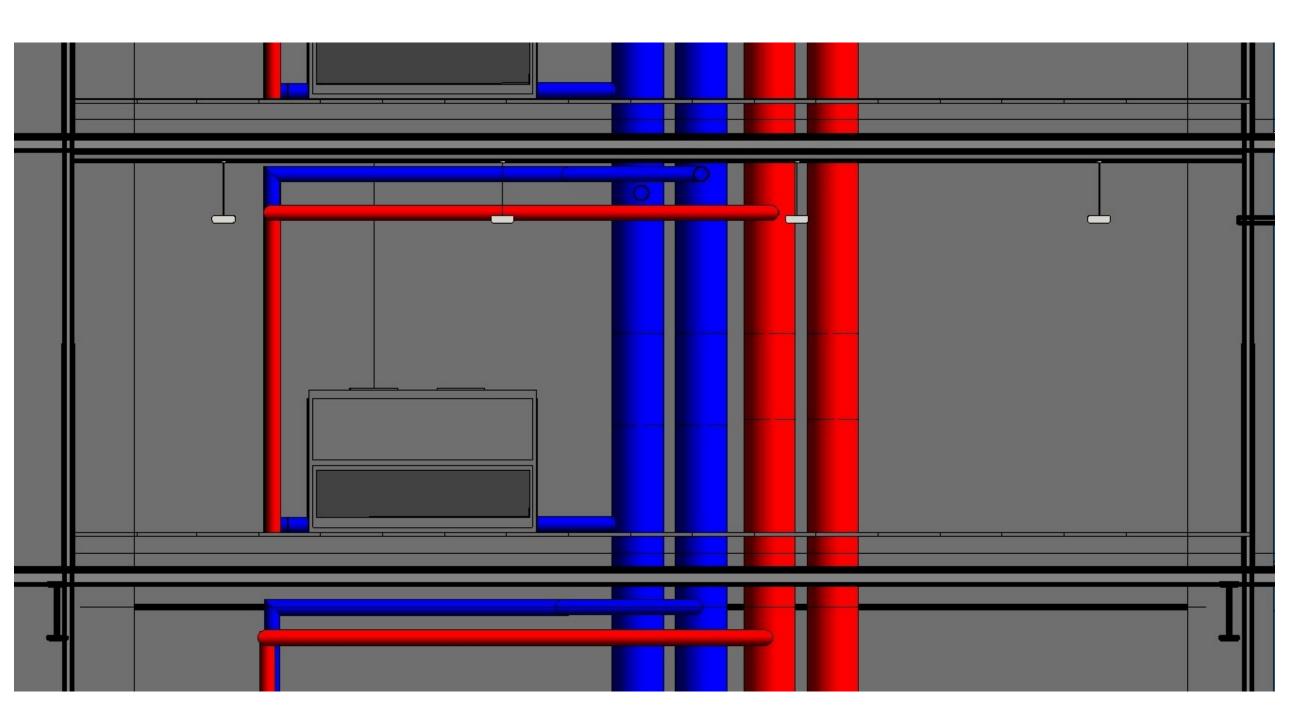
Mechanical

2014 Charles Pankow Foundation Annual Architectural Engineering Student Design Competition

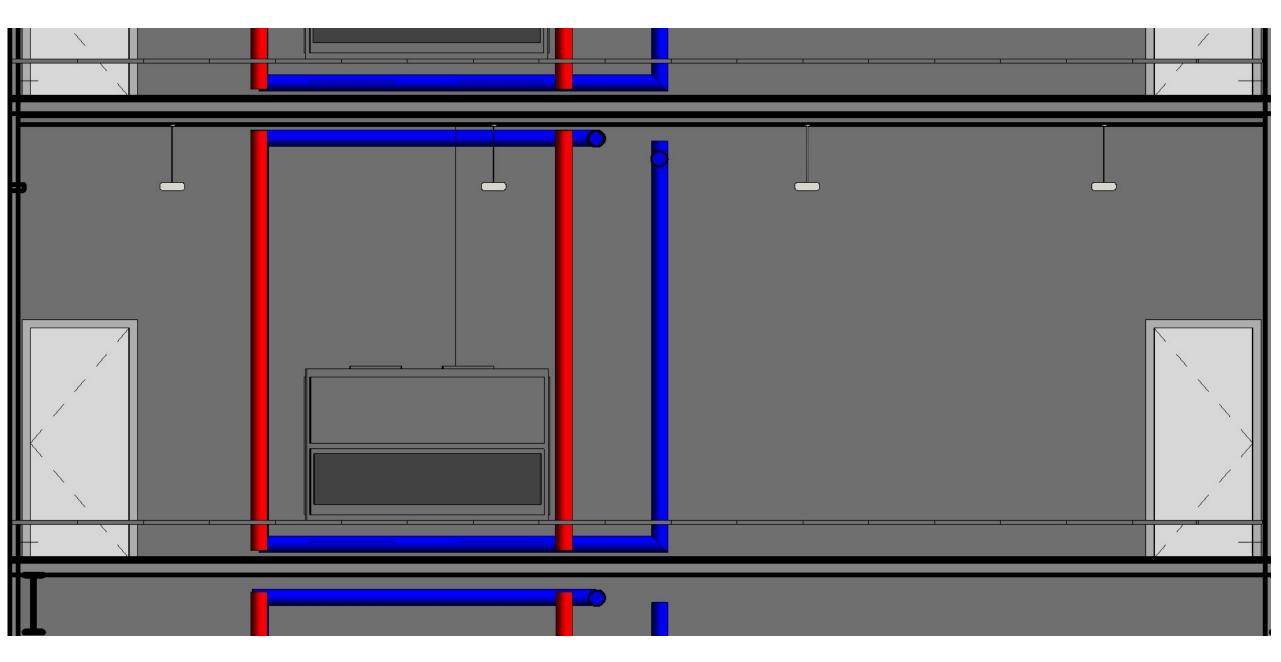
0.	Description	Date
A	EI Team Nui	mber
	05-2014	

$\mathbf{M}\text{-}\mathbf{106}$

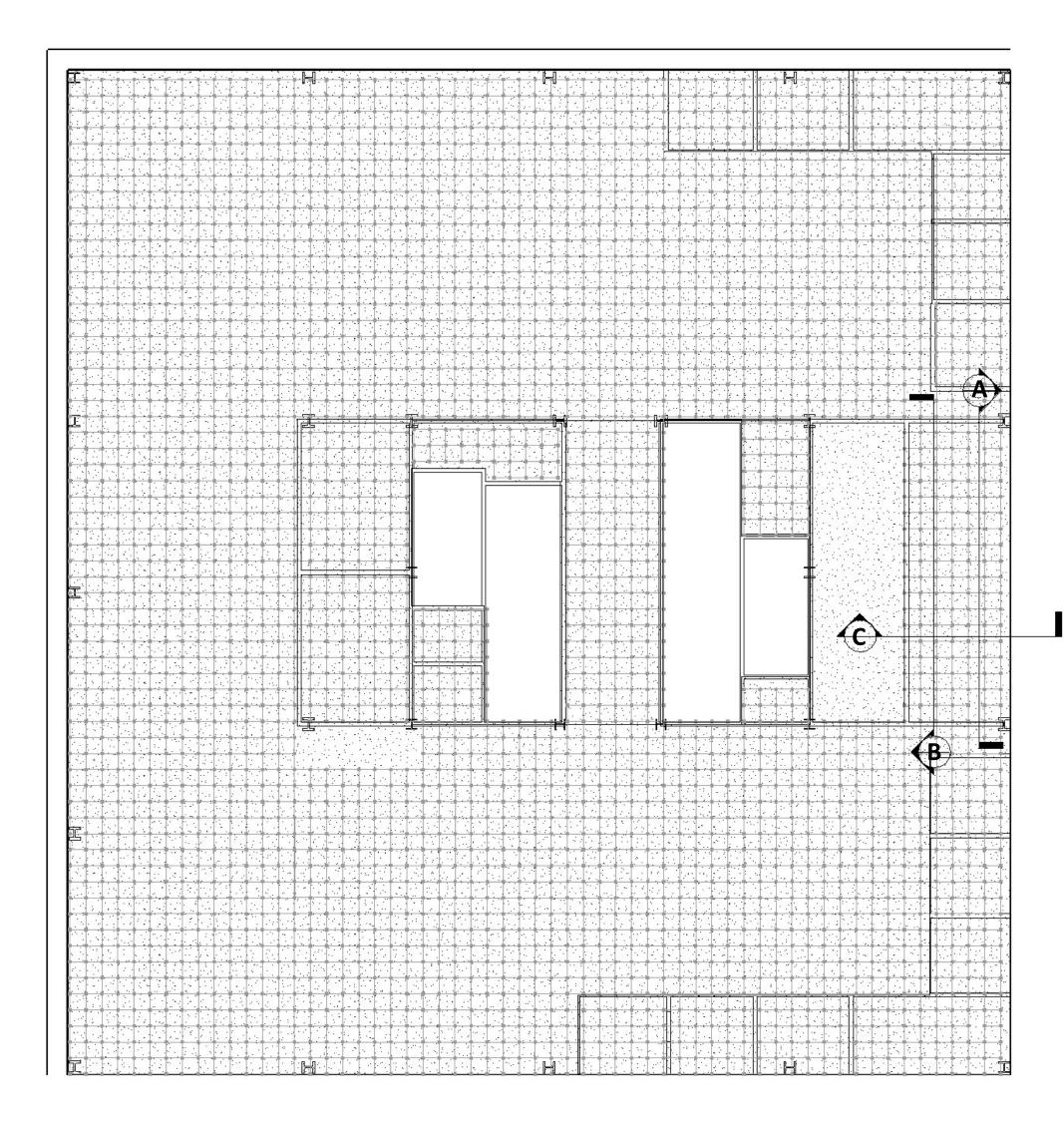
Mechanical Room



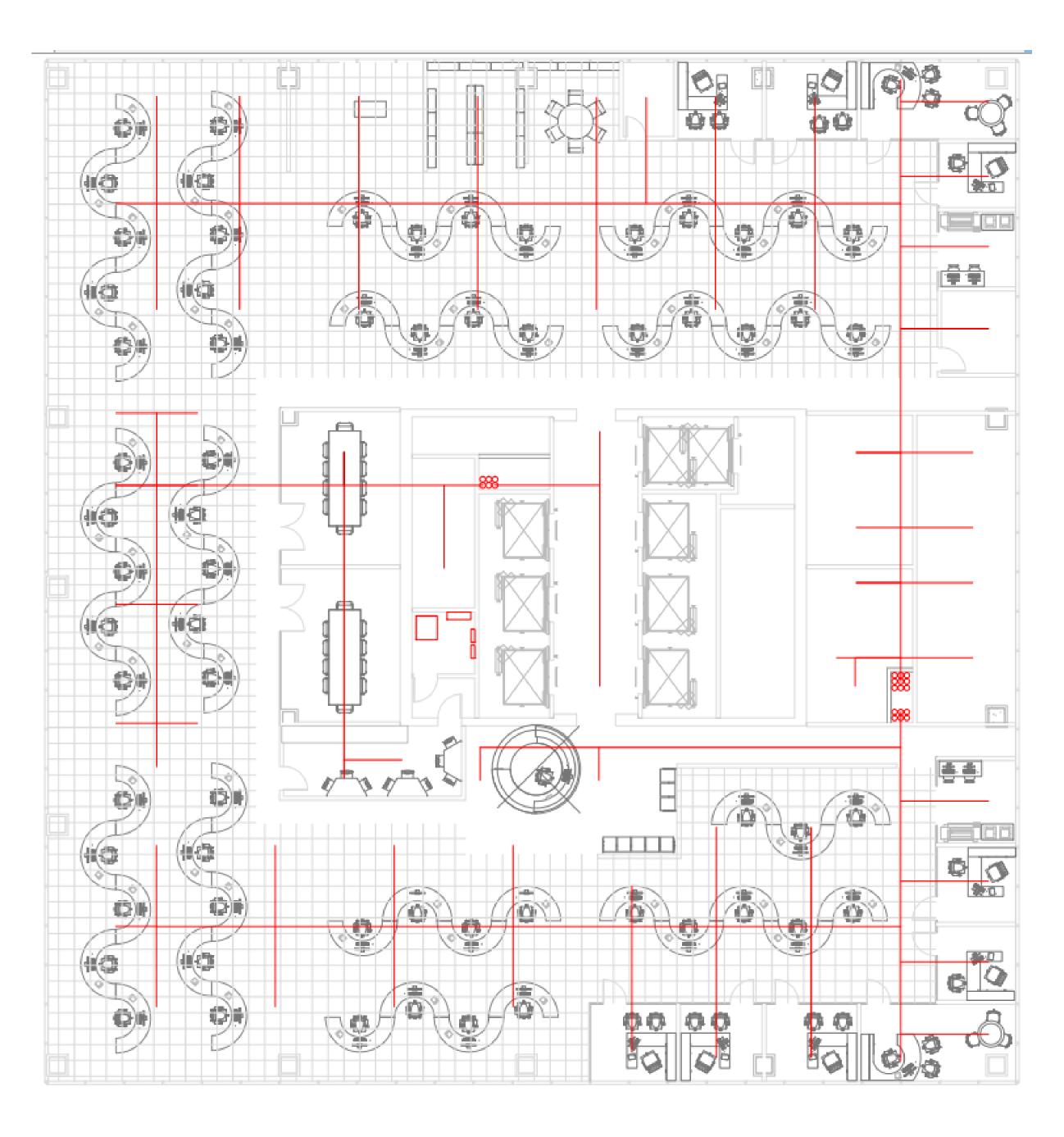
Section A

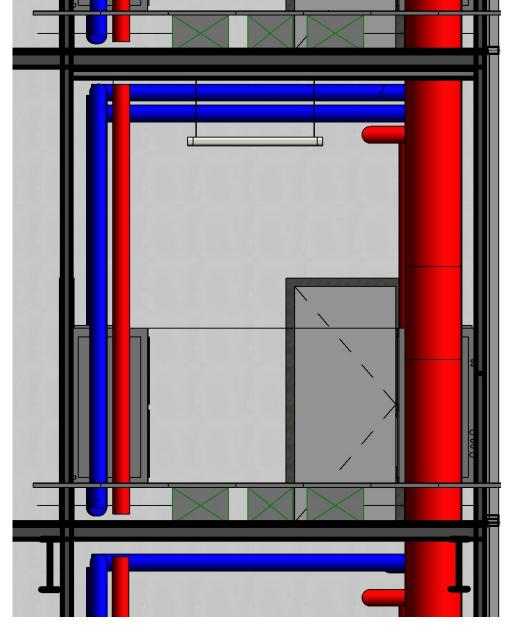


Section **B**



Fire Protection Plan





Section C

We chose a gaseous fire suppression system to help achieve our goal of immediate occupancy. A gaseous fire suppression system does not cause the damage to electronics and other materials that a traditional water fire suppression system would. Not only does this save on replacement costs, but also eliminates the repair time usually needed after a sprinkler system is activated.

No



Mechanical

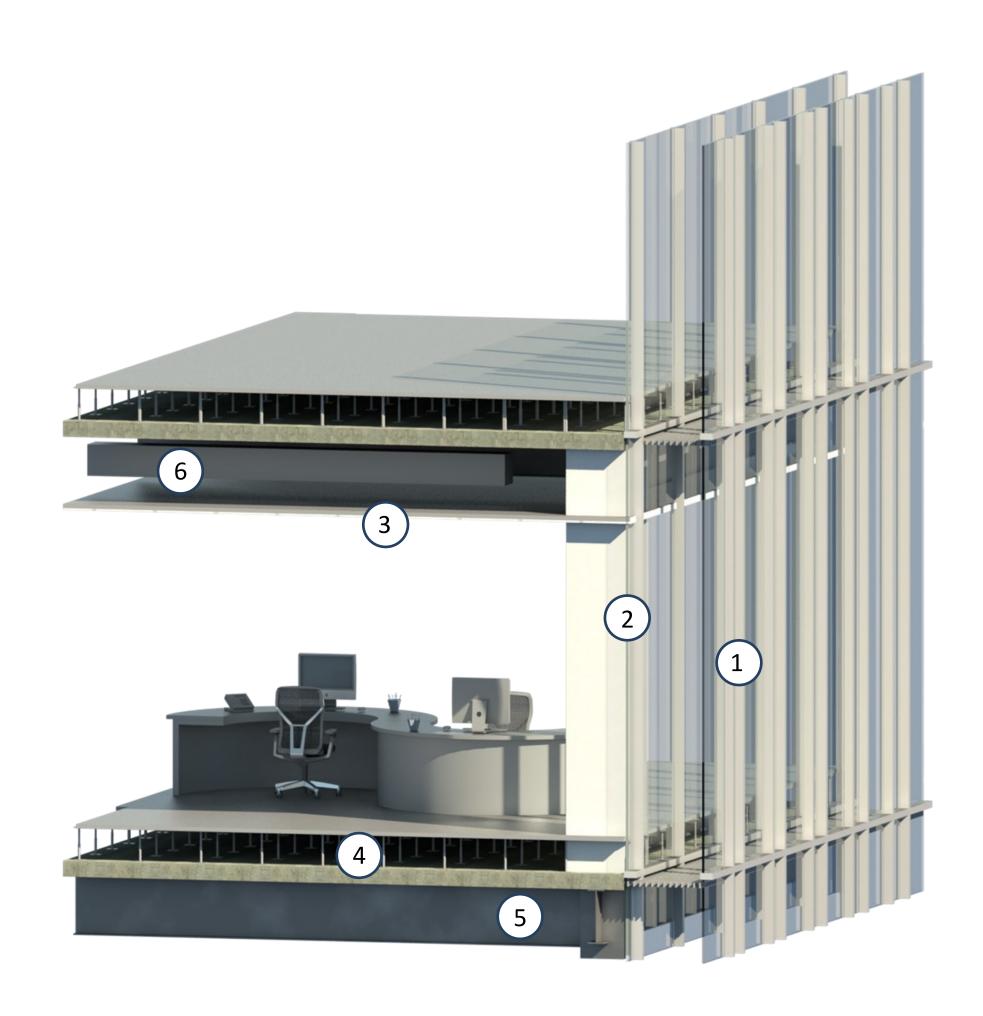
2014 Charles Pankow Foundation Annual Architectural Engineering Student Design Competition

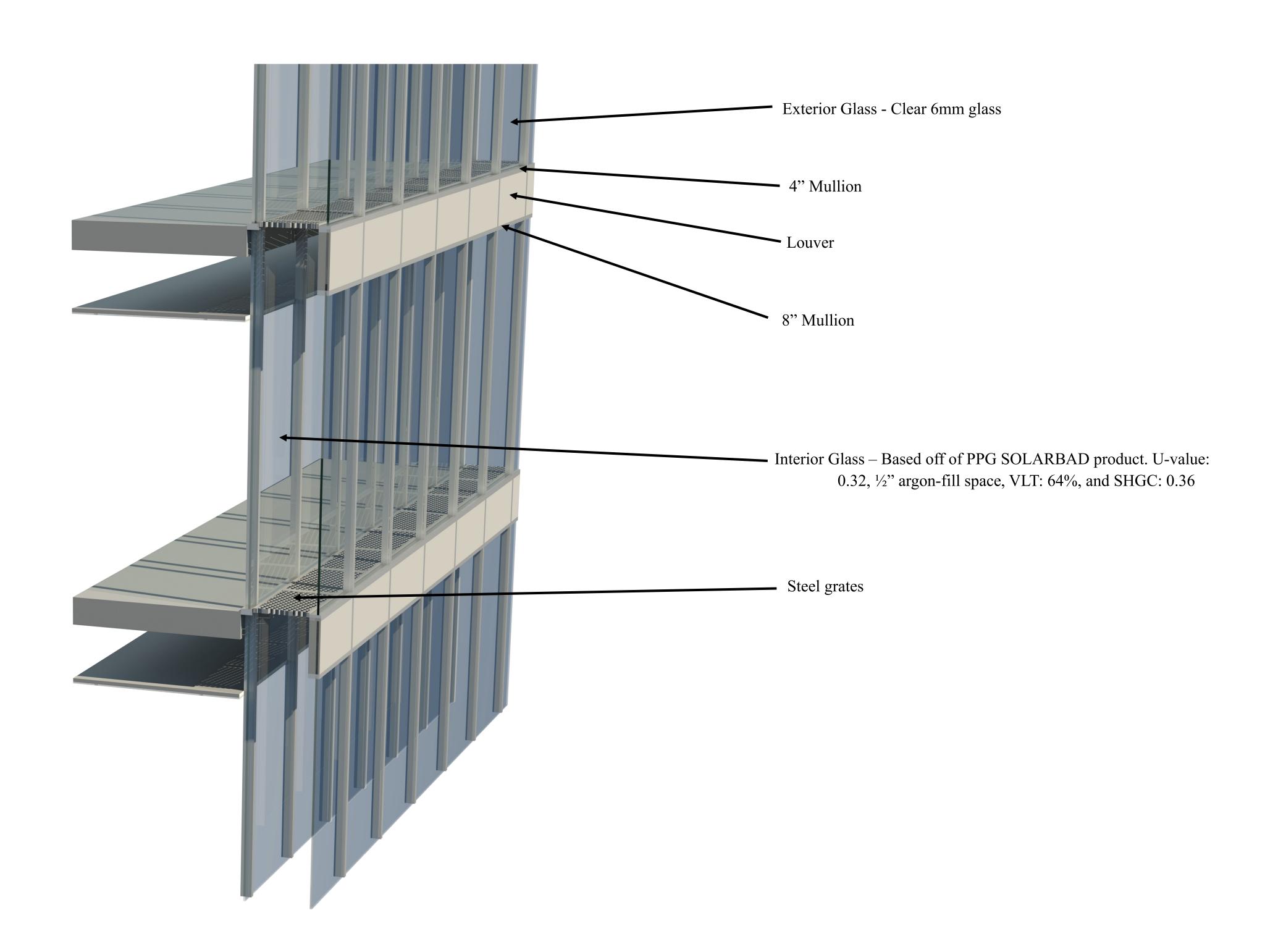
Description	Date
AEI Team Numb 05-2014)er

Piping

$\mathbf{M}\text{--}\mathbf{107}$

Double Facade



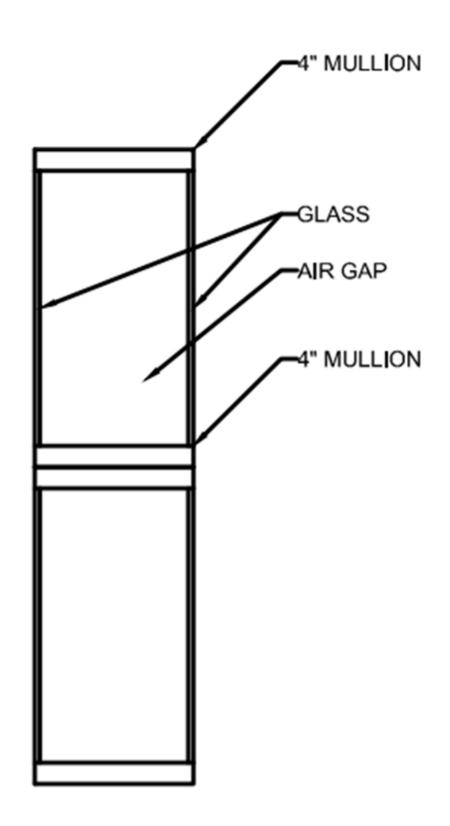


- 1 Double Façade System (DFS)
- 2 Daylight Control Retractable Shading
- (3) Daylight Dimming
- (4) Underfloor Ducts and Data Cables
- (5) Structural System
- 6 Return Duct

Collaboration:

DFS Mechanical: Energy Savings Electrical: Light Control Structural: Additional Imposed Weight **Retractable Shading** Mechanical: Effects Space Loads Electrical: Effects Surface Lighting Levels Daylight Dimming Mechanical: Effects Space Loads Construction: Additional Sensor Costs **Raised Access Floor** Mechanical: Coordinate with Electrical for Clash Electrical: Coordinate with Mechanical for Clash **Structural System** Mechanical: Coordinate with Structural for Clash Structural: Coordinate with all Disciplines for Loads Structural: Coordinated with System Clash

To ensure that all goals were satisfied, the disciplines had to confirm that all systems worked integrally with each other



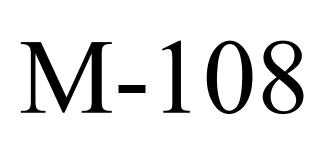


Mechanical

2014 Charles Pankow Foundation Annual Architectural Engineering Student **Design** Competition

0.	Description	Date
AI	EI Team Nun	nber
	05-2014	

Double Facade



Equipment Schedules

						SUPPLY FAN	N	ELE	CTRICAL D	ATA	BASIS	S OF DESIGN
TAG	LOCATION	AREA SERVED	COOLING CAPACITY (TONS)	HEATING CAPACITY (MBH)	AIR FLOW (CFM)	OA (CFM)	MOTOR HP	VOLTS/ PHASE/ HERTZ	FLA	МОР	MANUF	MODEL
AHU-1	Mechanical Platform	Lobby	60		24,000	845	2 @ 15	460-3-60	158.7	175.0	Carrier	50BVU-064
AHU-2	Podium	Podium	10		4,500	4,145	5	460-3-60	29.2	35	Carrier	50BRN-014
AHU-3	Mechancial Platform	Restaurant	10		4,000	3,761	3	460-3-60	25.6	30	Carrier	50BRN-012
AHU-4	Fan Room	Level 5 Office Peripheral	10		5,700	321	4.1	460-3-60	5.9	15	Stulz	CCU-300-CWE
AHU-5	Fan Room	Level 5 Office Core	20		11,500	668	4.1	460-3-60	10.1	15	Stulz	CCU-600-CWE
AHU-52	Fan Room	Level 30 Office Peripheral	10		5,700	321	4.1	460-3-60	5.9	15	Stulz	CCU-300-CWE
AHU-53	Fan Room	Level 30 Office Core	20		11,500	668	4.1	460-3-60	10.1	15	Stulz	CCU-600-CWE

			WATER DATA	A	ELECTI	RICAL	BASIS OF DESIGN			
TAG	COOLING CAPACITY (TONS)	RANGE (°F)	APPROACH (°F)	FLOW (GPM)	VOLT/ PHASE/ HERTZ	MOTOR HP	MANUF	MODEL		
CT-1	696	10	22	2100	480-3-60	2 @25	Evapco	AT-29-824		
TES:										

				WATER	DATA	ELECTRICAL	BASIS OF I	DESIGN
TAG	ТҮРЕ	MAX INPUT (MBH)	MAX OUTPUT (MBH)	EWT (°F)	LWT (°F)	VOLT/ PHASE/ HERTZ	MANUF	MODEL
B-1	Natural Gas	750	720	150	180		Cleaver-Brooks	CFC-750
B-2	Natural Gas	750	720	150	180		Cleaver-Brooks	CFC-750
В-3	Natural Gas	750	720	150	180		Cleaver-Brooks	CFC-750

			WATE	R DATA	ELECTRICAL VOLT/ PHASE/ HERTZ	BASIS OF DESIGN	
TAG	ТҮРЕ	Capacity (TONS)	EWT (°F)	LWT (°F)		MANUF	MODEL
CH-1	Absorption	450	56	44	460-3-60	Carrier	16-DF-045
CH-2	Absorption	450	56	44	460-3-60	Carrier	16-DF-045

TAC	CEN	Quantity/	GEDVICE	TYDE	SIZE (I	NCHES)		MAX	BASIS OF DESIGN	
TAG	CFM	Floor	SERVICE	ТҮРЕ	FACE	NECK	MOUNT	NC	MANUF	MODEL
NFD-5	100	120	Floor	Floor Diffuser	8"	-	Floor	15	Nailor	NFD
NFD-6	100	120	Floor	Floor Diffuser	8"	-	Floor	15	Nailor	NFD
NFD-29	100	120	Floor	Floor Diffuser	8"	-	Floor	15	Nailor	NFD
NFD-30	100	120	Floor	Floor Diffuser	8"	_	Floor	15	Nailor	NFD



Mechanical

2014 Charles Pankow Foundation Annual Architectural Engineering Student Design Competition

No.	Description	Date				
	AEI Team Numb	Der				
	05-2014					

Equipment Schedule

