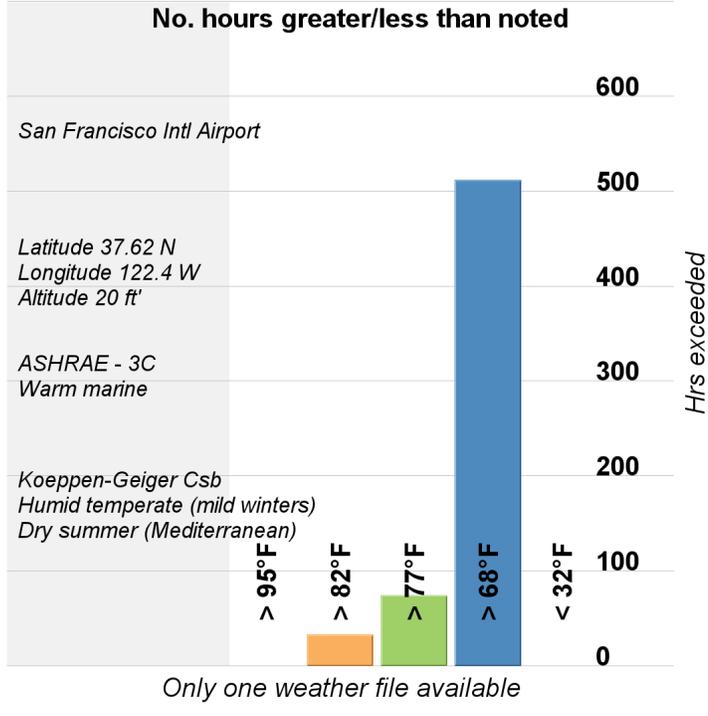


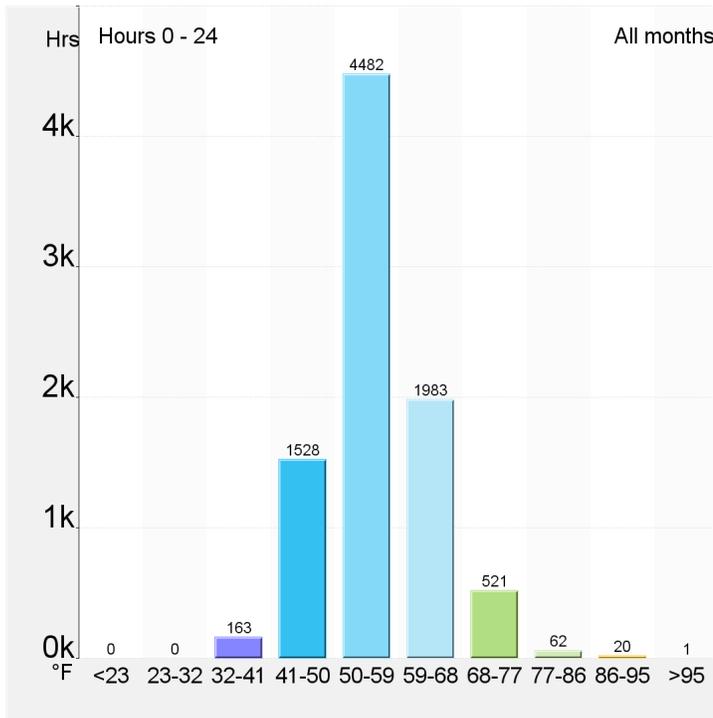
# SUPPORTING DOCUMENTS

## APPENDIX A: DESIGN CONDITIONS

### WEATHER DATA:



As can be seen in the graphs to the left, San Francisco's location is ideal for passive conditioning methods. The majority of the time, the temperature is between 50°F and 59°F. It is because of this reasonable climate that natural ventilation was a crucial design aspect in the mechanical system. By incorporating natural ventilation into the design we were able to see dramatic energy savings.



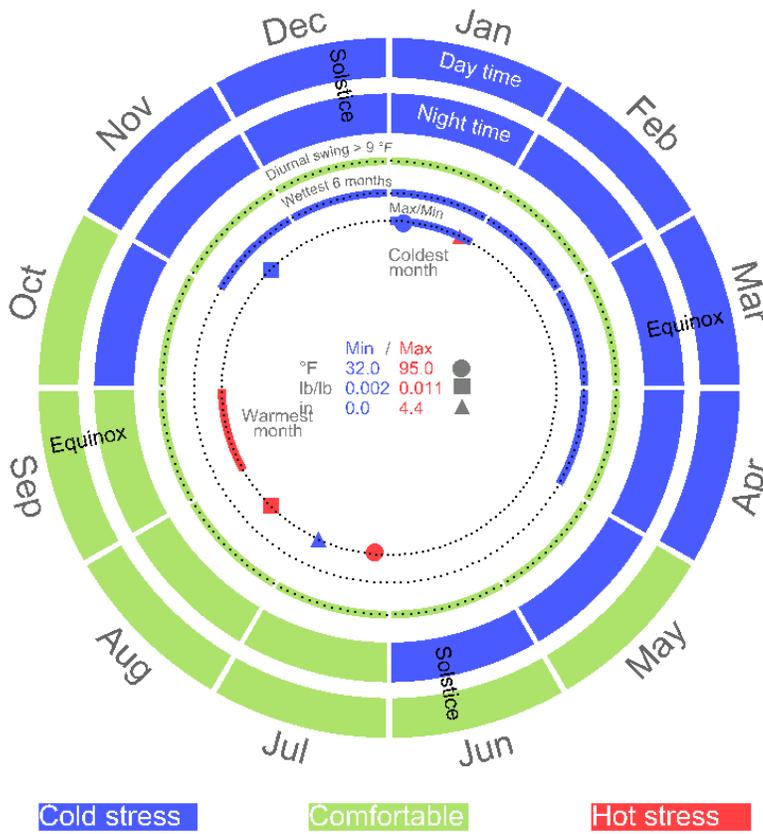
From IES CVE Climatic Report

**DESIGN DATA:**

HDD: 3016  
 CDD: 2883

\*Taken from ASHRAE

ASHRAE Locality: 3C  
 \*Taken from IES CVE Climatic Report



Coldest Month: January  
 Warmest Month: September  
 \*Taken from IES CVE Climatic Report

The above graphic was a crucial instrument in the beginning phases of the design process. This graphic effectively displays numerous design criteria such as hottest/coolest months in the year, maximum and minimum temperatures, and typical day/nighttime comfort conditions.

At first glance it is easy to see that the most saving could potentially be obtained in the summer months where the benefits of natural ventilation could be exploited. The circle graph shows that the outside ambient conditions are considered comfortable in the months from May to October. In addition, it indicates that there are not any months with hot stress, indicating that the heating load of the building will be more influential than the cooling load.

## APPENDIX B: COMBINED HEAT AND POWER

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### CO<sub>2</sub> AND FUEL CONSERVATION CALCULATIONS:

Below can be found the formulas/equations that were used to calculate the Carbon and Fuel reductions associated with incorporating a CHP System. The calculation method was taken from “Fuel and carbon dioxide emissions savings calculations methodology for CHP system” prescribed by the EPA.

#### Formula 1: Fuel Savings from CHP

$$F_S = (F_T + F_G) - F_{CHP}$$

- $F_S$  - Total Fuel Savings (Btu)
- $F_T$  - Fuel Use from Displaced On-site Thermal Production (Btu)
- $F_G$  - Fuel Use from Displaced Grid Electricity (Btu)
- $F_{CHP}$  - Fuel Used by CHP System (Btu)

#### Formula 2: CO<sub>2</sub> Savings from CHP

$$C_S = (C_T + C_G) - C_{CHP}$$

- $C_S$  - Total CO<sub>2</sub> Emissions Savings (lbs.CO<sub>2</sub>)
- $C_T$  - Fuel Use from Displaced On-site Thermal Production (lbs.CO<sub>2</sub>)
- $C_G$  - Fuel Use from Displaced Grid Electricity (lbs.CO<sub>2</sub>)
- $C_{CHP}$  - CO<sub>2</sub> Emissions from the CHP System (lbs.CO<sub>2</sub>)

#### Formula 3: Fuel Use from Displaced On-Site Thermal Production

$$F_T = \text{CHP}_T / \eta_T$$

- $F_T$  - Fuel Use from Displaced On-Site Thermal Production (Btu)
- $\text{CHP}_T$  - CHP System Thermal Output (Btu)  
\*  $\text{CHP}_T = F_{CHP} * 45\%$  (Heat Recovery Efficiency)
- $\eta_T$  - Efficiency of the Thermal Equipment

#### Formula 4: CO<sub>2</sub> Emissions from Displaced On-Site Thermal Production

$$C_T = F_T * \text{EF}_F * (1 * 10^{-6})$$

- $C_T$  - CO<sub>2</sub> Emissions from Displaced On-Site Thermal Production (lbs. CO<sub>2</sub>)
- $F_T$  - Thermal Fuel Savings (BTU)
- $\text{EF}_F$  - Fuel Specific CO<sub>2</sub> Emission factor (lbs. CO<sub>2</sub>/MMBtu)
- $1 * 10^{-6}$  - Conversion factor from Btu to MMBtu

## Formula 5: Displaced Grid Electricity from CHP

$$E_G = \text{CHP}_E / (1 - L_{T\&D})$$

- $E_G$  - Displaced Grid Electricity (kWh)  
 $\text{CHP}_E$  - CHP System Electricity Output (kWh)  
 $L_{T\&D}$  - Transmission and Distribution Losses

## Formula 6: Fuel Use from Displaced Grid Electricity

$$F_G = E_G * HR_G$$

- $F_G$  - Fuel Use from Displaced Grid Electricity (Btu)  
 $E_G$  - Displaced Grid Electricity from CHP (kWh)  
 $HR_G$  - Grid Electricity Heat Rate (Btu/kWh) per subregion  
 \*taken from [www.epa.gov/cleanenergy/documents/pdf file](http://www.epa.gov/cleanenergy/documents/pdf_file) Appendix B

Formula 7: CO<sub>2</sub> Emissions from Displaced Grid Electricity

$$C_G = E_G * EF_G$$

- $C_G$  - CO<sub>2</sub> Emissions from Displaced Grid Electricity (lbs. CO<sub>2</sub>)  
 $E_G$  - Displaced Grid Electricity from CHP (kWh)  
 $EF_G$  - Grid Electricity Emission Factor (CO<sub>2</sub>/kWh) per subregion

Formula 8: CO<sub>2</sub> Emissions from CHP System

$$C_{\text{CHP}} = F_{\text{CHP}} * EF_F$$

$$1,395,837(\text{lbs CO}_2) = 11,930,234,483(\text{Btu}) \times 117(\text{CO}_2/\text{MMBtu})$$

- $C_{\text{CHP}}$  - CO<sub>2</sub> Emissions from CHP System (lbs. CO<sub>2</sub>)  
 $F_{\text{CHP}}$  - Fuel used by CHP System (Btu)  
 $EF_F$  - Fuel Specific Emission Factor (lbs. CO<sub>2</sub>/MMBtu)

## PROCEDURE:

**CO<sub>2</sub> and Fuel Conservation Known Quantities**

	Quantity	Units
CHP <sub>E</sub>	1,014,000	kWh
F <sub>CHP</sub>	11,930,234,483	Btu
CHP <sub>T</sub>	5,368,605,517	Btu
η <sub>T</sub>	80%	
EF <sub>F</sub>	117	lbs. CO <sub>2</sub> /MMBtu
L <sub>T&amp;D</sub>	0	
HR <sub>G</sub>	5,774	Btu/kWh
EF <sub>G</sub>	953	lbs. CO <sub>2</sub> /MWh

$$\text{Formula 1: } F_S = (F_T + F_G) - F_{\text{CHP}}$$

$$635 \text{ (MMBtu)} = (6,710 + 5,854) - 11,930 \text{ (MBtu)}$$

$$\text{Formula 2: } C_S = (C_T + C_G) - C_{\text{CHP}}$$

$$355,663 \text{ (CO}_2\text{)} = (785,159 + 966,342) - 1,395,837 \text{ (CO}_2\text{)}$$

$$\text{Formula 3: } F_T = \text{CHP}_T / \eta_T$$

$$6,710,756,897 \text{ (Btu)} = 5,368,605,517 \text{ (Btu)} / .8$$

$$\text{Formula 4: } C_T = F_T * \text{EF}_F * (1 * 10^{-6})$$

$$785,159 \text{ (CO}_2\text{)} = 6,710,756,897 \text{ (Btu)} \times 117 \text{ (CO}_2\text{/MMBtu)} * 1 * 10^6$$

$$\text{Formula 5: } E_G = \text{CHP}_E / (1 - L_{\text{T\&D}})$$

$$1,014,000 \text{ (kWh)} = 1,014,000 \text{ (kWh)} / (1 - 0)$$

$$\text{Formula 6: } F_G = E_G * \text{HR}_G$$

$$5,854,836,000 \text{ (Btu)} = 1,014,000 \text{ (kWh)} \times 5,774 \text{ (Btu/kWh)}$$

$$\text{Formula 7: } C_G = E_G * \text{EF}_G$$

$$966,342 \text{ (CO}_2\text{)} = 1,014,000 \text{ (kWh)} \times .953 \text{ (CO}_2\text{/kWh)}$$

$$\text{Formula 8: } C_{\text{CHP}} = F_{\text{CHP}} * \text{EF}_F$$

$$1,395,837 \text{ (CO}_2\text{)} = 11,930,234,483 \text{ (Btu)} \times 117 \text{ (CO}_2\text{/MMBtu)}$$

## COMBINE HEAT AND POWER SYSTEM DESIGN:

<b>Max Load Capacities</b>		
Max Heating Capacity	2,100	kBtu/hr
Max Cooling Capacity	7,380	kBtu/hr
<b>65 kW Capstone Microturbines</b>		
Electrical Efficiency	29%	
Generation Capacity	627	kW
Quantity	10	
Actual Capacity	650	kW
<b>Energy Production</b>		
Generation Capacity	650	kW
Operating Hours	1,560	hrs/yr
Generated Power	1,014,000	kWh/yr
Power Consumption	3,815,944	kWh/yr
Electrical Capacity Met	33%	
<b>Heat Recovery</b>		
Heat Recovery Efficiency	45%	
Heat Recovery	1,842	Btu/hr
Capacity Met	88%	

The combined heat and power system (CHP) was sized off of the cooling load since it has the largest capacity. All information necessary for the computation was taken from Capstone's C65 Natural Gas Microturbine Performance Specification Data Sheet. The above table summarizes the resulting plant size, electrical generation capacity, yearly electrical demand satisfied, and thermal hot water capacity met.

**CHP PAYBACK:**

The following calculations estimate the time it will take in order to see a full return on the installed CHP system. Taken into account for this calculation are the savings associated with California's CHP/Cogeneration Incentive Program. From this program we were able to receive back \$0.48/W. This translated into a direct rebate/savings of \$312,000. The annual operation and maintenance (O&M) cost of \$.012/kWh was obtained from the EPA Overview document, *Table III: Summary Table of Typical Cost and Performance Characteristics by CHP Technologies*.

**CHP System Payback Period**

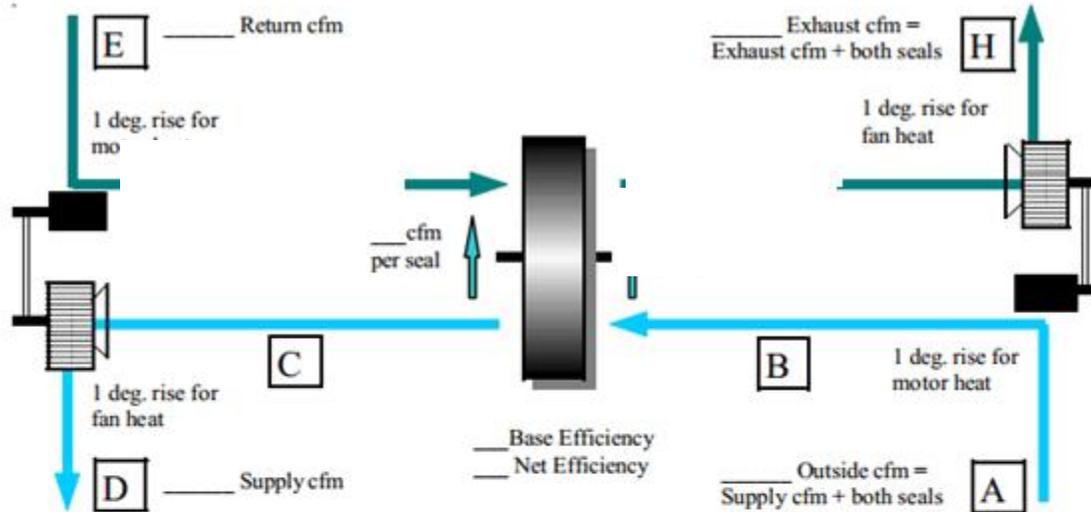
Year	Capital Investment	Yearly Maintenance	Spark Spread	Difference
1	503,000	12,168	101,400	-413,768
2	0	12,168	101,400	-324,536
3	0	12,168	101,400	-235,304
4	0	12,168	101,400	-146,072
5	0	12,168	101,400	-56,840
6	0	12,168	101,400	32,392
7	0	12,168	101,400	121,624
8	0	12,168	101,400	210,856
9	0	12,168	101,400	300,088
10	0	12,168	101,400	389,320
11	0	12,168	101,400	478,552
12	0	12,168	101,400	567,784
13	0	12,168	101,400	657,016
14	0	12,168	101,400	746,248
15	0	12,168	101,400	835,480
16	0	12,168	101,400	924,712
17	0	12,168	101,400	1,013,944
18	0	12,168	101,400	1,103,176
19	0	12,168	101,400	1,192,408
20	0	12,168	101,400	1,281,640
21	0	12,168	101,400	1,370,872
22	0	12,168	101,400	1,460,104
23	0	12,168	101,400	1,549,336
24	0	12,168	101,400	1,638,568
25	0	12,168	101,400	1,727,800

After running the 25 year analysis it was determined that the CHP system would see a full return in just over 5 years.

## APPENDIX C: ENTHALPY WHEEL

### ENTHALPY WHEEL/SENSIBLE AND LATENT LOAD CALCULATIONS:

The following section shows the calculations for the enthalpy wheel that was utilized to satisfy the latent load. Also presented are the sensible and latent load values for a typical office floor. The enthalpy wheel calculations were performed via the methods prescribed by the Berner Energy Recovery document found at [www.bernerenergy.com](http://www.bernerenergy.com). Below is a typical schematic of an enthalpy wheel that will be used to help perform the calculations.



**Design Supply CFM:** 17,000 CFM  
**Design Exhaust CFM:** 17,000 CFM  
**CFM Ratio:** 1.0  
**Base Efficiency:** 75%

#### EFFICIENCY OF THE WHEEL AT WHEEL RATIO

Model No.	CFM	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7
<b>9617</b>	16,000	0.75	0.80	0.83	0.86	0.88	0.91	0.93	0.94
	16,500	0.75	0.80	0.83	0.86	0.88	0.93	0.92	0.94
	17,000	0.75	0.80	0.83	0.86	0.88	0.90	0.92	0.95
	17,500	0.74	0.79	0.82	0.86	0.88	0.90	0.92	0.95
	18,000	0.73	0.78	0.83	0.85	0.87	0.90	0.93	0.95

Quantity	A (OA)	D (SA)	E (RA)	H (EX)
Dry Bulb	81	62	75	75
Wet Bulb	64	63	63	63
% Relative Humidity	39	-	50	50
Gr/lbs	63	62.7	66	66

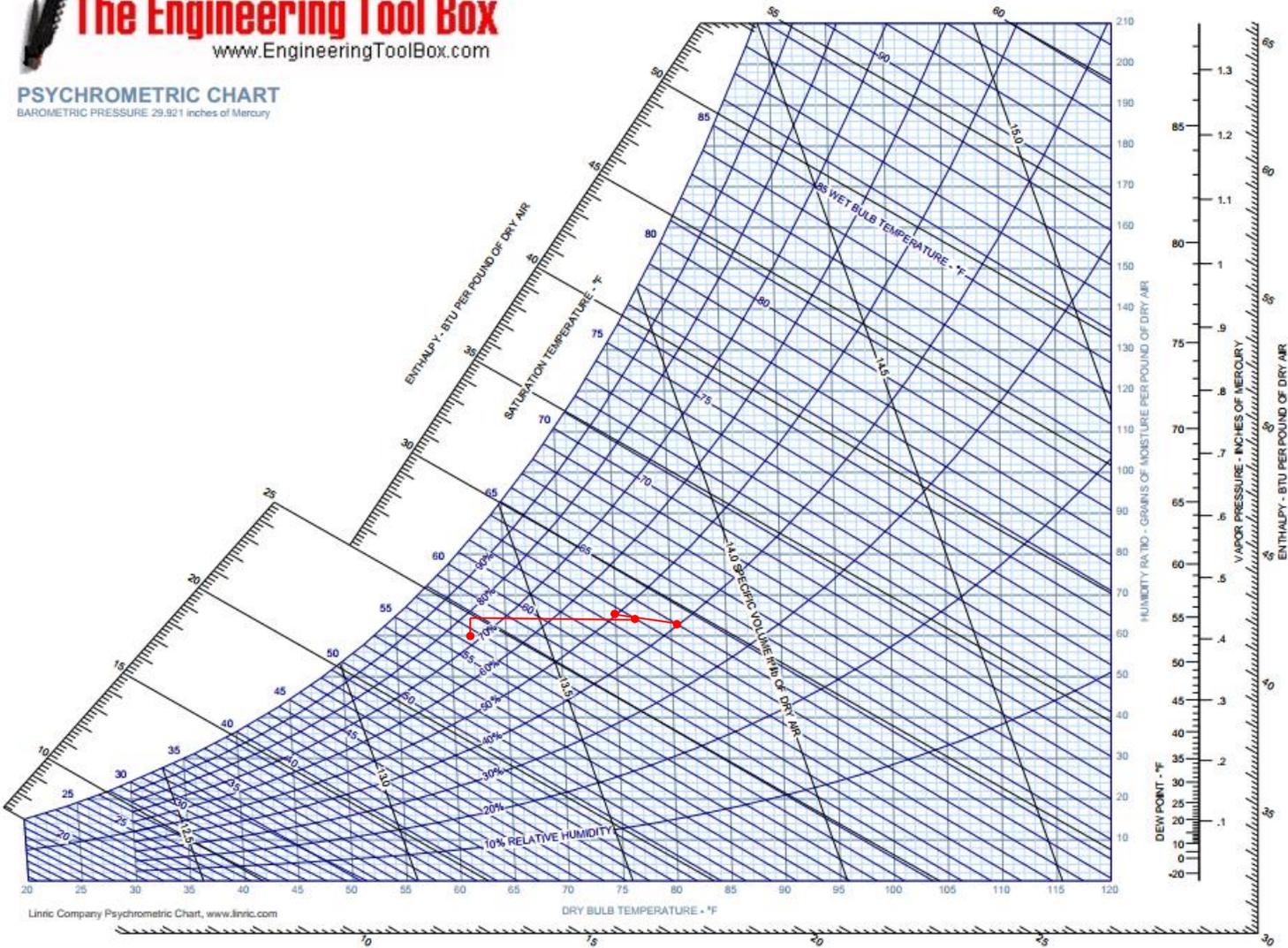
Enthalpy Wheel Capacity Procedure:

Formula 1 (Enthalpy wheel effect on DB):

$$OA_{DB} - RA_{DB} * eff_{Base} = 4.5^{oF} = (81-75)*.75$$

Formula 2 (Enthalpy wheel effect on humidity ratio):

$$OA_{gr/lbs} - RA_{gr/lb} * eff_{Base} = 2.3 \text{ gr/lbs} = (63-66)*.75$$



$$Q_{sensible} = 1.1 * CFM * \Delta T$$

$$Q_{sensible, \text{calculated}} = 242,000 \text{ Btu/hr.}$$

$$Q_{sensible, \text{system}} = 1.1 * 17,175 * (75-62)$$

$$= 245,600 \text{ Btu/hr.}$$

$$Q_{latent} = .68 * CFM * \Delta w$$

$$Q_{latent, \text{calculated}} = 27,000 \text{ Btu/hr.}$$

$$Q_{latent, \text{system}} = .68 * 17,175 * (66-62.7)$$

$$= 38,500 \text{ Btu/h}$$

## APPENDIX D: VENTILATION CALCULATIONS

Room Number	Room Name	Occupancy Category (ASHRAE 62.1)	Area A <sub>z</sub> (sf)	Area Outdoor Air Rate R <sub>3</sub> (Table 6.1)	Occupant Density P <sub>z</sub> (#people)	People Outdoor Air Rate R <sub>p</sub> (CFM/person)	Breathing Zone Outdoor Air Flow V <sub>bz</sub> = R <sub>p</sub> P <sub>z</sub> + R <sub>3</sub> A <sub>z</sub> (CFM)	Zone Air Distribution Effectiveness E <sub>z</sub> (Table 6.2)	Zone Outdoor Air Flow V <sub>oz</sub> = V <sub>bz</sub> /E <sub>z</sub>
B411	Elevator Lobby	Lobby	121	0.06	0.6	5	10	0.8	13
B409	Firemans Service Lobby	Lobby	191	0.06	1.0	5	16	0.8	20
B306	Elevator Lobby	Lobby	221	0.06	1.1	5	19	0.8	23
B300	Firemans Service Lobby	Lobby	191	0.06	1.0	5	16	0.8	20
B303	Service Lobby	Lobby	109	0.06	0.5	5	9	0.8	12
B206	Elevator Lobby	Lobby	221	0.06	1.1	5	19	0.8	23
B200	Firemans Service Lobby	Lobby	191	0.06	1.0	5	16	0.8	20
B203	Service Lobby	Lobby	109	0.06	0.5	5	9	0.8	12
B106	Elevator Lobby	Lobby	104	0.06	0.5	5	9	0.8	11
B100	Firemans Service Lobby	Lobby	187	0.06	0.9	5	16	0.8	20
B103	Service Lobby	Lobby	99	0.06	0.5	5	8	0.8	11
103	Service Lobby	Lobby	105	0.06	0.5	5	9	0.8	11
200	Firemans Service Lobby	Lobby	193	0.06	1.0	5	16	0.8	21
203	Service Lobby	Lobby	101	0.06	0.5	5	9	0.8	11
B112	Engineers Office	Office Space	500	0.06	3.0	5	45	0.8	56
B119	Valet Office	Office Space	90	0.06	1.0	5	10	0.8	13
110	Loading Dock Office	Office Space	100	0.06	1.0	5	11	0.8	14
101	Elevator Lobby	Lobby	350	0.06	1.8	5	30	0.8	37
111	Retail	Sales	400	0.12	6.0	7.5	93	0.8	116
100	Lobby	Main Entry Lobby	3600	0.06	36.0	5	396	0.8	495
113	Retail	Sales	625	0.12	9.4	7.5	145	0.8	182
215	Lobby	Lobby	1584	0.06	7.9	5	135	0.8	168
209	Restaurant	Restaurant dining room	4330	0.18	303.1	7.5	3053	0.8	3816
208	Corridor	Corridor	450	0.06	0.0	0	27	0.8	34
508	Private Office	Office Space	100	0.06	1.0	5	11	1.2	9
509	Private Office	Office Space	100	0.06	1.0	5	11	1.2	9
510	Private Office	Office Space	100	0.06	1.0	5	11	1.2	9
511	Executive Office	Office Space	200	0.06	1.0	5	17	1.2	14
512	Copy Room	Occupiable Storage	100	0.06	1.0	5	11	1.2	9
513	Private Office	Office Space	100	0.06	1.0	5	11	1.2	9
514	Server Room	Media Center	100	0.12	0.0	5	12	1.2	10
515	Copy Room	Occupiable Storage	100	0.06	1.0	5	11	1.2	9
516	Private Office	Office Space	100	0.06	1.0	5	11	1.2	9
517	Private Office	Office Space	100	0.06	1.0	5	11	1.2	9
518	Executive Office	Office Space	200	0.06	1.0	5	17	1.2	14
519	Private Office	Office Space	100	0.06	1.0	5	11	1.2	9
520	Private Office	Office Space	100	0.06	1.0	5	11	1.2	9
521	Private Office	Office Space	100	0.06	1.0	5	11	1.2	9
522	Conference	Conference/Meeting	190	0.06	9.5	5	59	1.2	49
523	Conference	Conference/Meeting	190	0.06	9.5	5	59	1.2	49
501	Elevator Lobby	Lobby	350	0.06	1.8	5	30	1.2	25
500	Open Office	Office Space	10250	0.06	51.3	5	871	1.2	726

APPENDIX E: LOAD CALCULATIONS

AHU-1 - LOBBY Cooling Loads

Air Side Cooling

Room Number	Room Name	Occupancy Category (ASHRAE 62.1)	Area A <sub>z</sub> (sf)	Internal Cooling Load (BTU/hr)	Internal Cooling Load (TONS)	Room Air Set Point (F)	Supply Air Flow (CFM)	Supply Air Temperature (F)	Air Side Cooling Capacity (BTU/hr)	Capacity Satisfied
111	Retail	Retail - Sales	441	2,643	0.22	75	185	62	2643	Confirmed
113	Retail	Retail - Sales	743	17,000	1.42	75	1189	62	17000	Confirmed
100	Lobby	Lobby	9362	651,012	54.25	75	45525	62	651012	Confirmed
<b>TOTAL</b>			9,362	670,655	56	75	46,899	62	670,655	

AHU-2 -PODIUM Cooling Loads

Air Side Cooling

Room Number	Room Name	Occupancy Category (ASHRAE 62.1)	Area A <sub>z</sub> (sf)	Internal Cooling Load (BTU/hr)	Internal Cooling Load (TONS)	Room Air Set Point (F)	Supply Air Flow (CFM)	Supply Air Temperature (F)	Air Side Cooling Capacity (BTU/hr)	Capacity Satisfied
B411	Womens Locker Room	Restroom	608	477	0.04	75	22	55	477	Confirmed
B415	Mens Locker Room	Restroom	612	323	0.03	75	15	55	323	Confirmed
B421A	Service Corridor	Corridor/ Transition	776	227	0.02	75	10	55	227	Confirmed
B411	Elevator Lobby	Lobby	121	3,825	0.32	75	174	55	3825	Confirmed
B409	Firemans Service Lobby	Lobby	191	6,349	0.53	75	289	55	6349	Confirmed
B306	Elevator Lobby	Lobby	221	6,586	0.55	75	299	55	6586	Confirmed
B300	Firemans Service Lobby	Lobby	191	6,123	0.51	75	278	55	6123	Confirmed
B303	Service Lobby	Lobby	109	2,894	0.24	75	132	55	2894	Confirmed
B206	Elevator Lobby	Lobby	221	6,612	0.55	75	301	55	6612	Confirmed
B200	Firemans Service Lobby	Lobby	191	6,125	0.51	75	278	55	6125	Confirmed
B203	Service Lobby	Lobby	109	3,016	0.25	75	137	55	3016	Confirmed
B119	Valet Office	Enclosed Office	87	174	0.01	75	8	55	174	Confirmed
B106	Elevator Lobby	Lobby	104	2,602	0.22	75	118	55	2602	Confirmed
B100	Firemans Service Lobby	Lobby	187	6,108	0.51	75	278	55	6108	Confirmed
B103	Service Lobby	Lobby	99	2,616	0.22	75	119	55	2616	Confirmed
B112	Engineers Office	Enclosed Office	639	1,151	0.10	75	52	55	1151	Confirmed
110	Loading Dock Office	Enclosed Office	97	185	0.02	75	8	55	185	Confirmed
103	Service Lobby	Lobby	105	2,952	0.25	75	134	55	2952	Confirmed
105	Electrical	Electrical/Mechanical	135	579	0.05	90	15	55	579	Confirmed
107	Exit Passageway	Corridor/ Transition	285	397	0.03	75	18	55	397	Confirmed
108	Exit Vestibule	Corridor/ Transition	62	85	0.01	75	4	55	85	Confirmed
M206	Mechanical Platform	Electrical/Mechanical	1,972	32,488	2.71	90	844	55	32488	Confirmed
208	Corridor	Corridor/ Transition	471	745	0.06	75	34	55	745	Confirmed
205	Electrical	Electrical/Mechanical	135	1,108	0.09	90	29	55	1108	Confirmed
200	Firemans Service Lobby	Lobby	193	7,394	0.62	75	336	55	7394	Confirmed
206	Mechanical Room	Electrical/Mechanical	272	1,592	0.13	90	41	55	1592	Confirmed
203	Service Lobby	Lobby	101	3,782	0.32	75	172	55	3782	Confirmed
<b>TOTAL</b>			5,243	73,099	6		4,145		73,099	

**AHU-3 - RESTAURANT Cooling Loads**

**Air Side Cooling**

Room Number	Room Name	Occupancy Category (ASHRAE 62.1)	Area A <sub>z</sub> (sf)	Internal Cooling Load (BTU/hr)	Internal Cooling Load (TONS)	Room Air Set Point (F)	Supply Air Flow (CFM)	Supply Air Temperature (F)	Air Side Cooling Capacity (BTU/hr)	Capacity Satisfied
209A	Kitchen	Food Preparation	1300	23,844	1.99	80	867	55	23844	Confirmed
209	Restaurant	Dining Area - Family	3400	58,903	4.91	75	2677	55	58903	Confirmed
<b>TOTAL</b>			4,700	82,747	7		3,544		82,747	

**AHU-4 - OFFICE Peripheral Cooling Loads**

**Air Side Cooling**

Room Number	Room Name	Occupancy Category (ASHRAE 62.1)	Area A <sub>z</sub> (sf)	Internal Cooling Load (BTU/hr)	Internal Cooling Load (TONS)	Room Air Set Point (F)	Supply Air Flow (CFM)	Supply Air Temperature (F)	Air Side Cooling Capacity (BTU/hr)	Capacity Satisfied
508	Private Office	Office Space	100	2,388	0.20	75	167	62	2,388	Confirmed
509	Private Office	Office Space	100	2,353	0.20	75	165	62	2,353	Confirmed
510	Private Office	Office Space	100	2,373	0.20	75	166	62	2,373	Confirmed
511	Executive Office	Office Space	200	4,784	0.40	75	335	62	4,784	Confirmed
512	Copy Room	Occupiable Storage	100	2,645	0.22	75	185	62	2,645	Confirmed
513	Private Office	Office Space	100	2,676	0.22	75	187	62	2,676	Confirmed
514	Server Room	Media Center	100	5,356	0.45	75	375	62	5,356	Confirmed
515	Copy Room	Occupiable Storage	100	2,646	0.22	75	185	62	2,646	Confirmed
516	Private Office	Office Space	100	2,639	0.22	75	185	62	2,639	Confirmed
517	Private Office	Office Space	100	2,679	0.22	75	187	62	2,679	Confirmed
518	Executive Office	Office Space	200	7,225	0.60	75	505	62	7,225	Confirmed
519	Private Office	Office Space	100	3,679	0.31	75	257	62	3,679	Confirmed
520	Private Office	Office Space	100	3,949	0.33	75	276	62	3,949	Confirmed
521	Private Office	Office Space	100	3,591	0.30	75	251	62	3,591	Confirmed
501B	Electrical	Electrical	100	800	0.07	90	26	62	800	Confirmed
501A	Telecomm	Electrical	100	800	0.07	90	26	62	800	Confirmed
500	Open Office	Office Space	2,563	40,046	3.34	75	2,800	62	40,046	Confirmed
<b>TOTAL</b>			4,363	90,629	8		6,278		90,629	

**AHU-5 - OFFICE Core Cooling Loads**

**Air Side Cooling**

Room Number	Room Name	Occupancy Category (ASHRAE 62.1)	Area A <sub>z</sub> (sf)	Internal Cooling Load (BTU/hr)	Internal Cooling Load (TONS)	Room Air Set Point (F)	Supply Air Flow (CFM)	Supply Air Temperature (F)	Air Side Cooling Capacity (BTU/hr)	Capacity Satisfied
522	Conference	Conference/Meeting	200	4,200	0.35	75	294	62	4,200	Confirmed
523	Conference	Conference/Meeting	200	4,213	0.35	75	295	62	4,213	Confirmed
501	Elevator Lobby	Lobby	350	18,412	1.53	75	1,288	62	18,412	Confirmed
506A	Men's Restroom	Restroom	270	4,408	0.37	75	308	62	4,408	Confirmed
506B	Women's Restroom	Restroom	270	4,452	0.37	75	311	62	4,452	Confirmed
500	Open Office	Office Space	7,689	120,139	10.01	75	8,401	62	120,139	Confirmed
<b>TOTAL</b>			8,979	155,824	13		10,897		155,824	

## APPENDIX F: DUCT SIZING

		Room Airflow (CFM)	Duct Airflow (CFM)	Duct Length (ft)	Friction Loss	Duct Velocity	Duct Size
<b>Duct A</b>							
500	Perimeter Open Office	1,407.9	<b>1407.9</b>	<b>140.0</b>	<b>0.28</b>	<b>1300</b>	<b>13x12</b>
<b>Duct B</b>							
508	Private Office	167.9					
509	Private Office	165.5					
510	Private Office	166.8					
511	Executive Office	336.6	<b>1,398.2</b>	<b>70.0</b>	<b>0.15</b>	<b>1300</b>	<b>13x12</b>
512	Copy Room	188.5					
513	Private Office	186.4					
514	Server Room	186.5					
<b>Duct C</b>							
500	Perimeter Open Office	1,407.9	<b>1,407.9</b>	<b>140.0</b>	<b>0.3</b>	<b>1300</b>	<b>13x12</b>
<b>Duct D</b>							
519	Private Office	262.8					
520	Private Office	257.4					
521	Private Office	246.7					
515	Copy Room	186.5	<b>1,728.5</b>	<b>70.0</b>	<b>0.15</b>	<b>1300</b>	<b>13x12</b>
516	Private Office	186.0					
517	Private Office	189.1					
518	Executive Office	400.0					
<b>Duct E</b>							
500	Open Office	500.0					
501	Elevator Lobby	1,294.6					
501A	Telecom	52.6	<b>2,005.7</b>	<b>65.0</b>	<b>0.11</b>	<b>1300</b>	<b>17x12</b>
501B	Electrical	50.4					
504	Stair 2	108.1					
<b>Duct F</b>							
500	Open Office	500.0					
502	Stair 1	94.5					
502A	Stair 1 Vestibule	82.7	<b>1,302.5</b>	<b>110</b>	<b>0.25</b>	<b>1300</b>	<b>11x12</b>
503	Service Lobby	31.7					
522	Conference	296.7					
523	Conference	296.9					
<b>Direct Supply</b>							
500	Open Office	7,447.3					
507	Fan Room	172.7					

The duct sizing was vital to clash detection and integration. The supply ducts could not be any taller than 13 inches because the raised access flooring is only 14 inches off of the slab. Therefore, the ducts needed to be wider in many cases, but still had to fit within the 24 inches between panels.

**APPENDIX G: WATER USAGE**

Level	Men's Toilets	Women's Toilets	Urinals	Faucets
<b>B4</b>	1	3	2	6
<b>B3</b>	0	0	0	0
<b>B2</b>	0	0	0	0
<b>B1</b>	0	0	0	0
<b>L01</b>	1	1	0	2
<b>L02</b>	1	1	0	0
<b>L05-L30</b>	50	100	50	100
<b>TOTAL</b>	<b>53</b>	<b>105</b>	<b>52</b>	<b>108</b>

Rain Water Collection													Annual
	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	
<b>Rainfall (in)</b>	4.50	4.61	3.26	1.46	0.70	0.16	0.00	0.06	0.21	1.12	3.16	4.56	<b>23.80</b>
<b>Collection Capacity</b>	<b>35,882</b>	<b>36,759</b>	<b>25,994</b>	<b>11,642</b>	<b>5,582</b>	<b>1,276</b>	<b>0</b>	<b>478</b>	<b>1,674</b>	<b>8,931</b>	<b>25,197</b>	<b>36,360</b>	<b>189,774</b>

**Water Use (Baseline)**

	# of Units	Gallons Per Flush	Building Occupants	Occupant Uses/Day	FTE	Yearly Use (Gal/Unit)	Total Use (Gal/Month)	Total Use (Gal/ Year)
Toilet - Men	53	1.6	712.5	1	712.5	1,140	5,035	60,420
Toilet - Women	105	1.6	712.5	3	2,137.5	3,420	29,925	359,100
Urinal	52	1.0	712.5	2	1425	1,425	6,175	74,100
<b>Total Non-Potable</b>							<b>41,135</b>	<b>493,620</b>
		<b>Gallons Per Minute</b>				<b>Total Uses (min)</b>		
Faucet	108	0.5	1425	3	4275	2137.5	1,069	9,619
<b>TOTAL</b>							<b>50,754</b>	<b>609,045</b>

**Water Use (Proposed)**

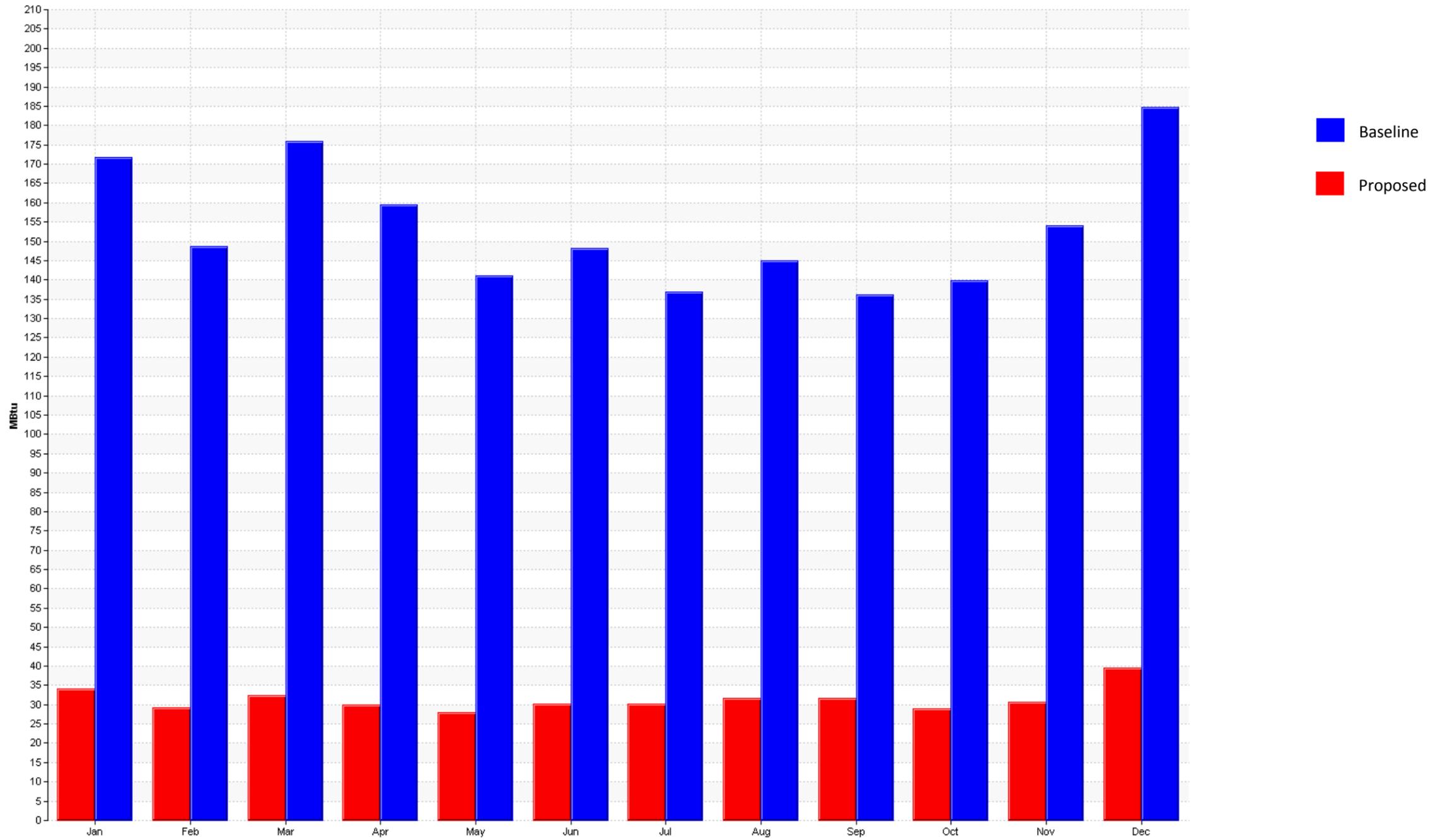
	# of Units	Gallons Per Flush	Building Occupants	Occupant Uses/Day	FTE	Yearly Use (Gal/Unit)	Total Use (Gal/Month)	Total Use (Gal/ Year)
Toilet - Men	53	1.0	712.5	1	712.5	713	3,147	37,763
Toilet - Women	105	1.0	712.5	3	2,137.5	2,138	18,703	224,438
Urinal	52	1.0	712.5	2	1425	1,425	6,175	74,100
<b>Total Non-Potable</b>							<b>28,025</b>	<b>336,300</b>
		<b>Gallons Per Minute</b>				<b>Total Uses (min)</b>		
Faucet	108	0.5	1425	3	4275	2137.5	1,069	9,619
<b>TOTAL</b>							<b>37,644</b>	<b>451,725</b>

The water reduction calculations were based off of LEED 2009 water reduction guidelines. The baseline values were those set forth by the LEED guidelines, and the proposed values were taken from possible manufacturers' websites. A building full-time equivalent occupancy of 1,425 was assumed based on ASHRAE occupant density values.

The rainwater collection values were calculated based on a 15,990 sq ft. roof area. Monthly precipitation levels were found from the National Weather Service.

APPENDIX H: ENERGY USE

Range: Fri 01/Jan to Fri 31/Dec



We modeled our building in IES and were able to calculate our energy use. As can be seen in the graph above, energy use decreased significantly from the baseline every month.

## APPENDIX I: LEED

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### WATER EFFICIENCY 6/10

#### Prerequisite 1: Water Use Reduction

Water demand reduced by 26% (see Appendix G)

#### WE Credit 2: Innovative Wastewater Technologies

**2 Points**

Option 1: Water use reduced by 56% (Appendix G and Table 9 in report) through rainwater collection and demand reduction

#### WE Credit 3: Water Use Reduction

**4 Points**

Water use reduced by 56% (Appendix G and Table 9 in report)

### ENERGY & ATMOSPHERE 26/35

#### Prerequisite 1: Fundamental Commissioning of Building Energy Systems

Budgeted for a commissioning authority

#### Prerequisite 2: Minimum Energy Performance

Option 1: Whole Building Energy Simulation – Used IES to simulate and achieved a savings of 53% (see Table 7 in report)

#### Prerequisite 3: Fundamental Refrigerant Management

Designed chilled water system

#### EA Credit 1: Optimize Energy Performance

**19 Points**

Achieved an overall energy use savings of 53% (see Table 7 in report)

#### EA Credit 4: Enhanced Refrigerant Management

**2 Points**

Option 1: Did not use refrigerants

#### EA Credit 5: Measurement and Verification

**3 Points**

Option 1: Budgeted for a measurement and verification plan

#### EA Credit 6: Green Power – 35% from renewable sources

**2 Points**

Option 1: Determine Baseline Electricity Use – We used IES to determine the annual electricity demand of the site

## INDOOR ENVIRONMENTAL QUALITY 4/15

### IEQ Prerequisite 1: Minimum Indoor Air Quality Performance

Met both Case 1 and Case 2 because our building utilizes both natural and mechanical ventilation

### IEQ Prerequisite 2: Environmental Tobacco Smoke (ETS) Control

Option 1: We are prohibiting smoking on the entire property, inside and outside

### IEQ Credit 1: Outdoor Air Delivery Monitoring 1 Point

Case 1 and Case 2: We have provided for CO<sub>2</sub> for all spaces

### IEQ Credit 6.2: Controllability of Systems - Thermal Comfort 1 Point

Because of our underfloor system, the occupants have control over the vent closest to their desks

### IEQ Credit 7.1: Thermal Comfort – Design 1 Point

Our HVAC system was designed using ASHRAE Standard 55-2004

### IEQ Credit 7.2: Thermal Comfort – Verification 1 Point

We budgeted for a monitoring system

## INNOVATION IN DESIGN 5/6

### ID Credit 1: Innovation in Design 5 Points

Path 1: Innovations in Design – Cogeneration, algae bioreactors

Path 2: Exemplary Performance – two incremental increases in EA Credit 1 (2 pts.), three incremental increases in WE Credit 3 (1 pt.)

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**TOTAL**
**41 POINTS**

## APPENDIX J: DESIGN TOOLS

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The design teams utilized a myriad of tool in order to analyze and develop the mechanical systems. The following tools are outlined below.



### AUTODESK REVIT

- Duct Layout
- Visual System Modeling
- BIM



### INTEGRATED ENVIRONMENTAL SOLUTIONS (IES)

- Load Calculation
- Energy Calculations
- System Analysis



### AUTODESK CAD

- System layouts



### MICROSOFT EXCEL

- Design Calculations



### AUTODESK INVENTOR

- Visual System Modeling



### AUTODESK NAVISWORKS

- BIM
- Clash Detection



### GOOGLE SKETCH UP

- Preliminary Design
- Model Creation Tool

















