HUB Renovations

& Addition

The Pennsylvania State University University Park, PA

Final Report



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April 9th, 2014

HUB RENOVATIONS & ADDITION

THE PENNSYLVANIA STATE UNIVERSITY, UNIVERSITY PARK, PA

PROJECT OVERVIEW

Building Function: Student Union Center Overall Project Cost: \$44.6 Million Size: 40,000 GSF Renovation 64,000 GSF New Construction Project Delivery Method: CM at Risk Contract Type: GMP Contract

PROJECT TEAM

Owner: The Pennsylvania State University Construction Manager: Gilbane Building Company Architect: GUND Partnership Structural Engineer: LeMessurier Consultants M/E/P Engineer: Vanderweil Engineers Civil Engineer: Sweetland Engineering & Assoc.

ARCHITECTURE

Renovated Book Store / New THON Merchandise Store New Seating/Lounge Space Habitable Green Roof Brick Veneer & Glazed Aluminum Curtain Wall System



STRUCTURAL

Foundation: Spread Footings & Micropiles Canopy Truss Roofing System Laterally Braced Structural Steel Framing 18 GA Composite Steel Decking

ELECTRICAL

New 480/277V Transformer Low Voltage MDS - 1600A, 3¢, 4W, 480Y/277V 4 Switchboards: 3 New, 1 Existing Lighting: Mixture of fluorescents and LED's

MECHANICAL

VAV and Single Zone Systems Automatic Wet Pipe Sprinkler System Finned Tube Radiators Fan Coil Units

 ROBERT JUSTIN BARLOW
 CONSTRUCTION OPTION

 http://www.engr.psu.edu/ae/thesis/portfolios/2014/rjb5258/index.html



Executive Summary

Over the fall 2013 and spring 2014 academic year, the HUB Renovations and Addition Project of The Pennsylvania State University was analyzed in order to identify areas that had potential to enhance the project overall. Through countless hours of research, feedback from academic members, the project team, multiple site visits, and construction professionals, four main areas were focused on for further analysis. The following report presents the four analyses performed as part of The Pennsylvania State University Architectural Engineering Senior Capstone Project. The purpose of this thesis project is strictly educational and is not intended to critique the work performed by the project team in any way.

Analysis # 1: Schedule Resequence

The first analysis addressed the feasibility of resequencing the interior bookstore phase of the original schedule. Analyzing the schedule by decreasing unnecessary float, sequencing improvements, and schedule overlap the schedule was looked to be improved. Areas of the project were looked at in order to accelerate the schedule which later analyses touch on. In addition, the lean principle of Last Planner was investigated for implementation on a project such as the HUB. The project team is encouraged to use the suggested acceleration techniques as well as the idea of Last Planner to make up for schedule delay.

Analysis # 2: Terra Cotta Rain Screen Redesign

Nearly half of the renovations and addition on the HUB façade is comprised of a complex terra cotta rain screen. This analysis addresses the need for schedule acceleration by providing an alternative brick veneer design. By switching the rain screen to brick veneer the project was able to save over a week of work days on the exterior façade of the bookstore alone, while saving \$64,143.18. With similar thermal properties analysis and acceptable structural loading, the project team is encouraged to use the alternative design to provide schedule and cost savings.

Analysis # 3: GPS Material Tracking System – Structural Steel

Topics discussed during The 22nd Annual PACE Roundtable by construction professionals led to the research portion provided in the third analysis. With a Just-In-Time delivery system for the structural steel a GPS tag tracking system will help ensure quality control by preventing schedule delays. The cost of the tracking system is roughly \$88,150 and the schedule would not see any savings. Although the technology to track the steel pieces will promote quality control, implementation would not benefit the project team due to the cost impact on a project of this size.

Analysis # 4: Removal of Habitable Green Roof Design

The final analysis looks at the current design of the habitable green roof to be constructed on the existing bookstore roof. Providing an alternative cool roof design will further address the need for schedule acceleration due to unforeseen issues. The alternative design provides a cost savings of \$154,896.00 and a schedule savings of 40 work days. The project team is encouraged to use the alternative design due to the cost and schedule savings of switching the design of an already existing roof structure.

Acknowledgments

Academic Acknowledgments

Penn State AE Faculty & Staff

Dr. Robert Leicht

Prof. Kevin Parfitt

Dr. Charles Cox

Ray Sowers

Corey Wilkinson

Industrial Acknowledgments



Special Thanks

Gilbane Project Team

Derek Stoecklein

Devon Saunders

Family & Friends

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Project Information

Background

The proposal for the HUB Renovations and Addition was made public over three years ago when the need for expansion of one of the most popular buildings on The Penn State University's campus arose. The HUB-Robeson Center was first constructed in 1955 as the student union center for the university and with the increase in student enrollment and the university itself the building has been renovated and expanded multiple times. With the amount of student and public traffic through the HUB daily the need for further expansion was required with the new proposal.

Drawing funds from Student Facilities, Barnes & Nobles, HUB Reserves, and Food Services the HUB Renovations and Addition will involve the following key improvements to the student union building: new seating, new lounge space, a new THON merchandise store, renovated bookstore, renovated food court, and relocation of various retail venues. Once the bids were made public the project team of the architect, GUND Partnership and the Construction Management Firm, Gilbane Construction Company emerged. The project was presented in front of Penn State's Board of Trustees and once approved; construction began in May of 2013.

The focus of this report is the HUB Renovation and Addition Project. The project has a LEED Silver Certification and is slated for 64,000 GSF of new construction and 40,000 GSF of renovation. Figure 1 displays the architect's rendering of the project.



Figure 1: Rendering of HUB-Robeson Building East Entrance | Image courtesy of Penn State

Existing Conditions

The HUB-Robeson Building is located on East Pollock Road in the heart of The Penn State University's campus in University Park, PA. With annual enrollment of more than 45,000 graduate and undergraduate students The Penn State University is one of the largest universities in the United States. The amount of student and pedestrian traffic around and through the HUB itself raises safety and logistical issues. In order to ensure the safety of those around the site multiple access maps were developed and posted. The maps provide access points for the public due to the east entrance being closed during construction. Construction fence surrounds the entire site and access to the site is carefully monitored due to the large amount of traffic around the site. Major access to the site for materials, equipment and are limited to main gate at East Pollock Road to eliminate congestion on campus.

The construction trailers for project team offices will be located offsite across East Pollock Road in the parking lot behind The Ritenour Building. These trailers are located off the construction site due to the limited amount of space around the HUB. Throughout the lifetime of the project multiple areas around the HUB will have temporary partitions in order to direct pedestrian traffic flow through and around the building. A main aspect of the project is the transfer of the bookstore into a temporary location on the HUB lawn. The temporary bookstore is comprised of 22 trailers and provides the same amenities as the current bookstore in order to supply books and retail items to students and the community. Figure 2 depicts the location of the HUB Project on campus.



Figure 2: HUB Location on Campus | Image courtesy of Penn State

Delivery Method

Gilbane is the single prime contractor working on the HUB Renovation and Addition. A Guaranteed Max Price contract is held between Penn State and Gilbane. Penn State has a separate contract with GUND Partnership who is serving as the lead Architect for the project. Subcontractors needed to be prequalified with Gilbane and then bids were formally submitted through Penn State.

Project Schedule

The project schedule incorporates a summary of major construction activities occurring at the HUB. This includes the design phase, procurement, preconstruction and construction activities. Due to parts of the project being turned over to Penn State before the entire project is complete, the construction has been split into phases. As previously stated construction began in May of 2013 and the project has a planned turnover date of March 2015. Figure 3 breaks down the start dates of the major construction activities.

Concerns of the existing structural foundation of the building and contractual issues have delayed the project. The analyses for the report focus on promoting schedule acceleration in order to make up for these potential delays. For the following report all duration and dates are based of the original baseline schedule used during bidding.





Project Cost

The total building construction cost of the HUB Renovations and Addition is \$30 Million. The overall project cost is set at \$44.6 Million; Table 1 provides a cost breakdown.

Project Cost Breakdown		
Description	Cost	
Building Cost	\$30,000,000	
Project Cost	\$44,600,000	
HVAC Cost	\$4,000,000	
Plumbing Cost	\$550,000	
Electrical Cost	\$2,800,000	
Structural Cost	\$3,500,000	

Building System Overview

Structural Steel

The structural system for the HUB project consists of concrete fill on steel deck and composite that bears on structural steel framing. The structure is framed with both, non-composite and composite beams connected with a blend of shear and moment connections. All the bracing for the frame utilizes HSS shapes, where all other structural steel is mostly W shaped steel. During the project duration one tower crane will be used located towards the HUB parking deck.

Mechanical System

The new work set on the project consists of seven AHU units supplying air to the bookstore, the atrium, multipurpose areas and to other existing areas. All the units will be Trane, M Series model ranging in supply 6,600 CFM to 22,000 CFM. These units will consist of both variable-air-volume (VAV) and single-zone air-handling units.

The fire suppression for the entire renovation/addition will comprise of a hydraulically-calculated automatic wet-pipe sprinkler system. All valves shall be equipped with supervisory switches and be provided with lockout covers to prevent tampering.

Electrical System

A new transformer rated at 480/277V will run primary feeder from PSU distribution to a new low-voltage main distribution switchgear that has a rating of 1600A, 3ϕ , 4W, 480Y/277V. This MDS runs to four switchboards, two rated at 208Y/120V, 3ϕ , 4W, 800A, one rated at 480Y/277Y, 3ϕ , 4W, 800A and an existing one rated at 480Y/277Y, 3ϕ , 4W, 2000A. These four switchboards feed panel boards which supply certain areas of the building.

Terra Cotta Rain Screen System

Similar to other newer buildings on campus the HUB Renovations and Addition incorporates newer architectural features with the more traditional aesthetics of the university. Nearly half of the HUB Project's façade is comprised of terra cotta rain screen with another quarter made up of aluminum curtain wall. The terra cotta is a unitized panel system with panels anchored to an aluminum track support in order to allow for thermal movements.

Aluminum Curtain Wall System

The enclosure for the atrium/courtyard area of the addition is aluminum glazed curtain wall. A pressure equalization design has been chosen with all components silicon compatible to provide durability. The curtain wall is aesthetically pleasing with concealed fasteners to create an unbroken line and an unchanging look. The curtain wall is also incorporated along with the terra cotta rain screen system throughout the exterior of the building.

Habitable Green Roof

The HUB Project introduces the first habitable green roof to a university which strives to learn, live, and lead in sustainability practices. The green roof will help advance sustainable architecture and design on campus and will provide several environmental benefits. The extensive green roof design will cover nearly 8,000 SF of the bookstore existing roof structure. The rendering of the east entrance in Figure 4 shows the habitable green roof, aluminum curtain wall system, and the terra cotta rain scree system.



Figure 4: Rendering of HUB-Robeson Building East Façade | Image courtesy of Penn State

Analysis #1: Schedule Resequence

Problem

The structural conditions of the existing portion of the HUB created a potential delay in the project schedule. This creates multiple scenarios for potential schedule acceleration in order to make up a large portion of the time that could be lost due to the structural issue. With the original schedule focusing on specific turn over dates for each phase of the project, the potential acceleration will focus around each one of these crucial phases.

Research Goal

The goal of this analysis is to establish the best schedule sequence for the overall project in order to keep the original turn over dates in tack. The original schedule constraints will be analyzed in order to figure out which phases have areas of flexibility and which phases have the largest areas for issues. Once the main areas are uncovered one phase will be analyzed in order to focus on areas of concern. Possible schedule techniques for these areas include the following; crashing, shifting work, and working on concurrent activities at once. After analyzing multiple options, the most efficient process will be suggested in order for the project team to create a more efficient schedule sequence.

Methodology

- Analyze the original schedule
 - Discover the schedule constraints
- Evaluate the areas with potential flexibility (Issue Areas)
 - Review areas with Gilbane Project Team & AE Faculty (Advisor: Robert Leicht)
 - Develop potential option(s) for the project sequence (Focused around Issue areas)
- Evaluate the potential option(s)
 - Review the option(s) with Gilbane Project Team & AE Faculty (Advisor)
- Suggest the most efficient option to implement
- Research Lean Construction Practices (The Lean Construction Institute)

Resources

- Gilbane Project Team (Project Manager: Randy Holman, Project Engineer(s): Derek & Devin)
- AE Faculty (Advisor: Robert Leicht)
- Other Industry Professional(s) (OPP Staff Members)
- Schedule Software (P6)
- The Lean Construction Institute

Expected Outcome

The potential for delay of the initial schedule allows for the option of resequencing multiple phases of the project. The delay occurred during the demolish phase of the project creating many opportunities to improve upon the schedule. Through a sequencing analysis the schedule is to provide the project team with the best techniques to help maintain the original deadlines. Through the investigation of Lean Construction principles a more efficient way of reducing the schedule will be presented.

Original Schedule

In order to complete a project resequencing analysis the first step is to study the existing schedule to identify areas that can be resequenced or adjusted. The overall schedule was broken down into 9 different construction sections shown in Table 2. Each phase was evaluated separately for sequencing improvements and the potential for actives to overlap. After studying the multiple phases focus for major schedule resequencing shifted towards the Bookstore Interior.

Detailed Schedule Summary			
Description	Start Date	End Date	Total Duration
Sitework	26 February 2014	24 December 2014	43 Weeks
Lobby	16 May 2013	05 September 2014	68 Weeks
Atrium/Courtyard	16 July 2013	09 April 2014	38 Weeks
Courtyard Interiors	09 April 2014	24 December 2014	37 Weeks
Bookstore Interior	16 May 2013	18 July 2014	61 Weeks
Bookstore Exterior	02 December 2013	14 February 2014	10 Weeks
MPR Volume	25 October 2013	29 May 2014	30 Weeks
Overbuild	25 September 2013	26 February 2014	22 Weeks
Food Service Renovation	05 May 2014	15 August 2014	14 Weeks

 Table 2: Detailed Schedule Summary | RJB

The HUB Roberson Center is home to The Pennsylvania State University, University Park's Official Bookstore. The bookstore supplies textbooks, supplies, electronics, Penn State apparel and much more to nearly 45,000 students and the residents of the surrounding community. The turnover of the bookstore back to the University was originally set for mid-July of 2014 however due to unforeseen structural issues the new date for the basement area of the bookstore is September 2014. During the renovation and addition of the HUB a temporary bookstore was set up outside the building in 22 trailers. Although Penn State owns the land and trailers not having the permanent bookstore in the student union center of one of the largest universities in the nation causes some concerns. Focusing on the turnover of the bookstore will help deal with unforeseen issues while ensuring a pleased owner.

Bookstore Interior

The activities in the Bookstore Interior Phase are the focus of the study for this analysis. Focusing on one phase of the project will help to find areas of improvement that may be able to be used in other phases of the project. Figure 5 below shows the original bid schedule for the Bookstore Interiors.

Phase 2: Bookstore Interior/Exterior	292 31-May-13 18-Ju-14	v 18-Jul∮14, Plyase 2 Bookjatore Interiorij Exteriori
- Interior	292 31-May-13 18-Jul-14	V 18-Jul 14, Inferior
Fit Out Computer Store / 110 / 235	10 31-May-13 13-Jun-13	Fit Out Compiler Stor / 110 / 235
Computer Store Vacated	D 31-May-13	Computer Store Vacated 31 May-13
Relocate AT&T to HUB Retail	19 14-Jun-13 11-Jul-13	Relocate AT&1 te HUB Retail
Relocate FS Manager to 235	5 14-Jun-13 20-Jun-13	Relocate FSI Manage to 235
Relocate Copy Center/ Student Employment	5 17-Jun-13 21-Jun-13	Relocate Copy Center / Student Employment
Demoition Bookstore Interior	34 05-Jul-13 21-Aug-13	Demolitiva Bookstøre Interior
Relocate FS Director to Trailer	4 05-Jul-13 10-Jul-13	🛛 Reiocate FS Dire tot to Trailer
Reinforce Columns & Slabs	15 11-Sep-13 01-Od-13	eletorce Countins & \$labs
🚃 Erect Strucutral Steel Mezzanine	20 14-Oct-13 08-Nov-13	Erect Strucutral Steel Mezzanine
💼 Detail Structural Steel & Deck Mezzanine	10 11-Nov-13" 22-Nov-13	🗖 Detail Structural Steel & Deck Mezzahine
Prepare & Place Concrete on Deck Mezzanine	4 25-Nov-13" 29-Nov-13	D Prepare & Plaos Conclete of Deck Mezzanine
Overhead Rough Ins Bookstore Interiors	19 02-Deo-13" 27-Deo-13	Overhead Rought ins Bookstore Interiors
🚃 Frame Walis/ Drywall Bookstore Interiors	19 23-Dec-13" 17-Jan-14	Frame Walls Drywall Bookstore Interfors
Perimeter Walls Bookstore Interiors	25 20-Jan-14" 21-Feb-14	Perimeter Valis Bookstore Intériors
Wall Finishes Bookstore Interiors	25 20-Jan-14" 21-Feb-14	Wall finishes Bookstore Interlors
Celling Finishes Bookstore Interiors	35 24-Feb-14" 11-Apr-14	Celling #Inishes Bookstore Interiors
Floor Finishes Bookstore Interiors	25 14-Apr-14" 16-May-14	Picor Pinishes Bookstore Interiods
Tenant Imporvement Bookstore	5 05-May-14" 09-May-14	D Tenant Imporvement Bookstore
🚃 Move - In Bookstore	10 07-Jul-14" 18-Jul-14	🗖 Move - In Bobistore
Exterior	54 02-Deo-13 14-Feb-14	4-Feb-14, Exterior

Figure 5: Bookstore Interior Schedule | RJB

The first step in the evaluation process was to assess the activities for any unnecessary float or days where no work was scheduled. An example of unnecessary float is evident between relocation of copy center and the start of interior demolition. There is a 10 day work gap between the first activity ending and the other beginning. After discovering gaps similar to this one, each needed to be analyzed individually in order to identify the purpose of the gap and if there was room for improvement. Once each gap was analyzed if the gap was not required, i.e. the start of interior demolition, it has potential to be removed or reduced from the schedule.

After analyzing the gaps between line items, the schedule was studied for potential sequencing improvements. Once the foundation work is complete in the lower levels of the bookstore, the remaining work is on the main floor of the bookstore and new mezzanine level. The basement level of the bookstore holds the entire inventory for the bookstore retail items. Allowing the bookstore occupants to move the large amount of inventory into the basement will help save time instead of turning the bookstore over as a whole. Partial occupation does involve certain regulations that would have to be looked into. New egress plans would have to be created as well as occupant permitting to allow spaces to be occupied while others are under construction. The bookstore itself has always been scheduled to be turned over before the entire project completion date. Along with the bookstore area, the lobby outside the bookstore contains the only accessible entrance during construction so finishing the lobby would be another crucial area of acceleration in order for turnover to occur.

The final way the bookstore interior phase was analyzed in order to be altered was through the study of potential scheduling overlaps. After studying the bookstore phase itself, there were no areas for overlapping activities. When looking to save time by schedule overlapping multiple phases of the project needed to be looked at. For example moving the start of the overbuild up to start the foundation work while demolition in the bookstore is in progress could have potential to accelerate the overall project schedule.

Areas of Schedule Acceleration: Building System

While studying the project schedule for areas of schedule resequencing scenarios the possibility of changing the current Terra Cotta façade system came up. This has potential for major schedule savings and potential cost savings. Analysis 2 provides an in-depth investigation into switching the Terra Cotta façade. It details the potential schedule acceleration of switching to an alternative façade of the exterior of the bookstore. Another area of schedule acceleration is the design of the roof for the bookstore.

Analysis 4 details the removal of the Green Roof proposed for the roof over top of the existing bookstore. The analysis breaks down the potential schedule savings of changing the Green Roof to an alternative design. For the results of changing the façade system and developing an alternative bookstore roofing design refer to the schedule impact section in each relevant analysis. Table 3 displays the current schedule for the bookstore exterior.

Schedule Breakdown – Bookstore Exterior			
Description	Start Date	End Date	Total Duration
Roof Membrane	02 December 2013	13 December 2013	10 Days
Exterior Façade Terra Cotta	02 December 2013	17 January 2014	35 Days
Green Roof / Accessories	16 December 2013	24 January 2014	30 Days
Install Green Roof - Planting	27 January 2014	14 February 2014	15 Days

Table 3: Schedule Bookstore Exterior | RJB

Last Planner System

The Last Planner System (LPS) developed in association with the Lean Construction Institute is a "production planning system designed to produce predictable work flow and rapid learning in programming, design, construction and commissioning of projects" (The Last Planner, 2014). Examples of the lean process have been presented through case studies and industrial experiences throughout the Architectural Engineering curriculum. Las Planner is a short-term project planning system used in engineering construction for over 20 years in order to make improvements in project and program safety, predictability, productivity, speed of delivery, profit and feeling of wellbeing among project staff. Similar to issues that arise on the HUB Project, much of construction management is dealing with issues that have gone wrong in an effort to get back on track.

LPS uses five key conversations that each brings its own benefits, and are listed below

- 1. **Collaborative Programming** creating and agreeing the production sequence
- 2. MakeReady Making tasks in the look ahead period ready so that they can be done when needed
- 3. **Production Planning** collaboratively agreeing production tasks for the next day or week
- 4. **Production Management** collaboratively monitoring production to keep activities on track
- 5. Measurement, learning and continual improvements learning together

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LPS is a production control system designed to ensure the achievement of agreed goals. A collaborative programming process is used to set these goals as a way to engage the entire team from the start. Involving all major players early in the process helps to ensure the critical interdependencies and risks are discussed. There are multiple benefits of collaborative programming which include the following: preparing team members for action together, discuss details much sooner, sort out sequencing and other issues that would be difficult to change later, enable teams to test options while improving workflow, identifies unclear design details, and builds commitment to program and reduces overall schedule period. LPS promotes the use of the important words, "I don't know" which are important in all conversations and some people will do anything to avoid saying them. Promoting the use of these words will help other members of the team help one another to be successful. The second conversation helps to look ahead in the project schedule.

The MakeReady process systematically checks that everything is in place for each of the tasks in the look ahead. The MakeReady process has benefits such as tasks are ready for production when required, safer working/planning, and a greater certainty of time, materials and equipment with less waste. The third conversation deals with production tasks for the upcoming days or week. Production evaluation and planning (PEP) meetings are incorporating in all last planners. Depending on the length of a project, shorter daily work planning may be required but generally PEP meeting occur weekly. The purposes of these meetings are to review and learn from the work done in the previous periods. This allows planning the work that will be done in the next period. The benefits of PEP meeting as it pertains to Last Planner are as follows: maintains commitment to the intention of the project and current client concerns, suppliers prepare better because they know what's expected of them, builds relationships between supplier team leaders, focuses attention on what can really be done, and facilitates learning from experiences. The fifth conversation in LPS helps improve promise reliability and the predictability of production plans.

The Collaborative Programming and Production Planning conversations help to develop the social process in construction promoting a shared sense of responsibility for project delivery. Implementing daily stand-up meetings on site or by phone detailing the work completed the day before. This allows detecting early warning of any late deliveries and enables the team to renew deadlines based on last minute adjustments. Depending on the project, production planning and production management are combined in a daily meeting. The sixth and final conversation promotes learning together about and improving project, planning and production processes. Measurement, learning and continual improvement is the basis for evaluation process in a PEP meeting. Continual improvement elements contribute to more predictable and reliable workflow. When all these conversations are working together they reinforce each other and the overall benefits are greater.

The effect of implementing Last Planner on the HUB Project could result in major schedule savings. This could help benefit the perimeter enclosure as well as the project as a whole. According to the Lean Construction Institute not only does schedule duration and costs decrease but accident frequency decrease as well when LPS is used. Last Planner is a registered trademark by The Lean Construction Institute requires their consent before implementing Last Planner in order to ensure the system is being properly used.

Conclusion

This analysis has evaluated the possibility of removing gaps in construction activities, looking at the schedule for sequencing improvements and overlaps, alternative design for schedule acceleration, and a look into project management methods for more lean construction practices. The project team is encouraged to analyze the schedule for gaps in activities and the ability to overlap phases in order to meet the turn over deadlines set by the university. It is strongly recommended that the project team implement Last Planner System as a lean building tactic due to its capability of reducing schedules. The schedule effect of the alternative design for the exterior façade and Green Roof are provided in Analysis 2 and Analysis 4.

Analysis #2: Terra Cotta Rain Screen Redesign

Problem

The current façade of the existing building consists of mainly brick veneer and the new design implements multiple new facades types. Roughly half of the surface area of the building façade is comprised of a complex terra cotta rain screen. The step-by-step installation process for each fragile piece of terra cotta is labor intensive and time consuming. With the structural concerns leading to potential delays in schedule this analysis will provide a further area for schedule acceleration.

Research Goal

The purpose of this analysis is to look into an alternate system for the terra cotta rain screen that will allow for schedule acceleration. The total square footage of each type of exterior façade will be analyzed based on the cost and time required for each system. With the new design an updated schedule will be produced and a comparison between the original schedule will be developed. An estimate and cost comparison between the original and re-design will provide further analysis of the two systems.

Methodology

- Establish the Square Footage of each façade type
- Establish the scope & production rates for each façade type
- Develop a schedule comparison between original & new design
- Develop an estimate and cost comparison between the original & new design
- Develop Energy Study based off Thermal properties of façade components
- Develop Structural Study Check to ensure new loading is acceptable

Resources

- Gilbane Project Team (Project Manager: Randy Holman, Project Engineer(s): Derek & Devin)
- Design Team (GUND Partnership)
- AE Faculty (Advisor: Robert Leicht, Moses Ling)
- Other Industry Professional(s) (OPP Staff Members)
- Material Specifications
- Construction Drawings
- Mechanical Software
- Structural Software

Expected Outcome

The expected outcome of this analysis is to provide a new system that will accelerate the schedule without taking away from the overall architectural vision of the design team and owner. Ultimately this will save time and money with a reduced labor and equipment requirement to install the new system. Along with the resequencing of the phases this will allow the project to make up for potential delays.

Building Façade Study

In order to develop an alternative façade choice to implement into the project the current design for the addition and renovation was analyzed to determine the overall square footage of each. Terra cotta rain screen covers nearly 50 percent of the exterior of the building with the remainder consisting of the following: Aluminum Glazed Curtain Wall (25%), Brick Veneer (14%), and Metal Paneling (10%). The aluminum glazed curtain wall encloses the atrium/courtyard area of the addition and includes a complex canopy roofing system. Although the brick veneer is the third most commonly used façade type on the new design, due to the amount of brick on the current building and surrounding campus, using brick veneer as a substitute for the terra cotta rain screen was chosen. Table 4 breaks down the façade types further.



Façade Description				
Description	Area (SF)	Percentage	Cost / SF	Weight (PSF)
Terra Cotta Rain Screen	13812.03	51%	\$38.00	25
Aluminum Glazed Curtain Wall	6811.56	25%		
Brick Veneer	3776.4	14%	\$5.00	65
Metal Paneling	2658.22	10%		
Total:	27058.21	100%		

Table 4: Facade Breakdown | RJB

Switch to Brick Veneer

The current terra cotta rain screen system is by Shildan Inc. and features Alphaton terra cotta panels that rest onto aluminum frames by means of a support grid with hooks that the panels rest onto. Figure 7 below shows the process of installing such a system with exterior sheathing attached first. Horizontal substructure aluminum extrusion or metal braces, are then attached to the exterior structure before two and half inches of insulation can be installed. The horizontal extrusions are what provide structural support. Once the vertical spacers are installed, the Alphaton terra cotta panels can be hung from them to complete the rain screen system. All of these steps must be completed in a subsequent order with the use of lifts which is very time-consuming.



Figure 7: Terra Cotta System Installation Steps - Pictures Courtesy of Cladding Corp. (www.claddingcorp.com)

Although the terra cotta system is time-consuming there are advantages to the system which factored into the decision to use it in the design. The following are long term benefits which will help the owner in the long run. Since the insulation is outside of the air/vapor barrier the contestation is continually evaporating due to air movement, providing a higher insulation value which reduces the energy consumption of the building. This will help with provide better comfort and productivity from the occupants. The terra cotta panels do not have calcium leakage or efflorescence effect and can simply be cleaned with water unlike that of a brick façade. The natural ventilation prevents the growth of mold or mildew from occurring in the walls of the building. This allows the terra cotta system to provide a 100-year façade to the building.

A large portion of Penn State's buildings consist of brick façade including the existing structure of the HUB-Robeson building. Introducing such a large square footage of new façade to a building may add character to the campus but does not benefit the University as much as it would another owner. Maintenance on campus is used to dealing with brick veneer and understands how to deal with such issues as calcium leakage or efflorescence effect. Although issues do come up in buildings as they age overtime however the knowledge at Penn State keep the issue of mold and mildew from becoming an issue. Switching the original design from terra cotta rain screen to brick veneer will allow Penn State to continue the continuity of red brick across the campus as well as keep the maintenance work constant from building to building.

Terra Cotta Rain Screen System vs. Brick Veneer: Physical Components

The physical components of the terra cotta rain screen system and brick veneer are similar however the location of the vapor barrier differs in the make-up of the wall. Each façade type utilizes a continuous AVB membrane and 2.5" Mineral Wool Insulation. The terra cotta rain screen system from exterior inwards consists of the following: Terra Cotta Panel (Alphaton Panel), 2.5" Mineral Wool, Continuous AVB Membrane, ¹/₂" Sheathing, and a 6" Metal Stud. Similarly the brick veneer from exterior inwards consists of the following: Brick Façade (8" Brick), Brick Ties (as required), Airspace, 2.5" Mineral Wool Insulation, and a Continuous AVB Membrane. The components within each system were looked at in order to define the scope of work for each system.

The overall dimensions difference of each wall system is 1.125" with the terra cotta rain screen and brick veneer totaling 1' - 4 3/8" and 1' - 5 1/2" respectively. Figure 8.1 shows a dimensioned detail of both the terra cotta rain screen system and Figure 8.2 shows the brick veneer detail. The overall difference in the components of the each system is due to the amount of time spent installing each component.



The terra cotta rain screen system requires a great deal of time spent installing the horizontal and vertical metal grid system that the Alphaton Panel will attach to. Once the exterior sheathing is installed the anchors and vertical metal grids are installed. Next the insulation is installed before the horizontal grid is put in place and this takes some time due to the requirements for it to be level in order to have the Alphaton Panel connect to one another correctly. Once the panels are ready to be installed the remaining process goes by quickly. Each panel requires fasteners which will help connect it to the horizontal grid and one by one each panel will connect to one another completing the terra cotta rain screen system. Unlike the rain screen system most of the time spent installing the brick veneer occurs in laying the brick itself.

Similar to the terra cotta rain screen system the brick veneer requires the installation of and AVB membrane, insulation and the outside layer of masonry. However, more time is spent in the exterior of the system than the interior; it takes much longer to lay bricks than it does to connect the terra cotta panels to the building. Brick veneer is a common façade type and trades are used to laying brick compared to installation of terra cotta panels. This will allow for the brick veneer to be completed without a learning curve which may occur when installing an unfamiliar system like the terra cotta rain screen system.

Mechanical Breadth

The change in façade type from the terra cotta to the brick veneer will not only affect the buildings aesthetics but will also affect the overall energy performance of the building. Through this Mechanical Breadth the thermal properties of both the existing and new façade systems will be looked at and used to perform a simple energy model of the bookstore.

R-Values

With the change in façade systems the overall thermal properties of the systems are different and will therefore affect the building. Each system is constructed of materials which have a unique R-Value. Depending on the location and combination of the materials, the systems will have different thermal properties. Using the HAM Toolbox both the terra cotta system and the brick veneer system were analyzed to determine the overall R-Value of each one. The overall R-Values are shown below, the terra cotta values are in Table 5 and the brick veneer values are in Table 6. The calculations from the HAM Toolbox are provided in Appendix C.1-C.2.

Table 5: Terra Cotta R-Values

Terra Cotta Façade Assembly – R Values		
Construction Material	R-Value (per thickness hr.*ft2*F/BTU)	
Terra Cotta Block	0.54	
Mineral Wool	8.90	
AVB Membrane	0.12	
Exterior Sheathing	0.64	
Metal Stud	0.12	
Total:	10.32	

Table 6: Brick Veneer R-Values

Brick Veneer Façade Assembly – R Values			
Construction Material	R Value (per thickness hr.*ft2*F/BTU)		
Brick	0.64		
Air Cavity	0.98		
Mineral Wool	8.90		
AVB Membrane	0.12		
Exterior Sheathing	0.64		
Metal Stud	0.12		
Total:	11.40		

The brick veneer assembly contains an air cavity which accounts for one more layer than the terra cotta assembly. Also, the brick provides a higher R-Value than the terra cotta helping the brick veneer assembly to obtain a slightly higher overall R-Value. When comparing the two façade assemblies, the new façade assembly has a higher R-Value than the original façade assembly. The brick veneer provides an R-Value of 11.40 hr*ft²*F/BTU compared to 10.32 hr*ft²*F/BTU provided by the terra cotta. The R-Values of the original and new assembly can only provide so much information, so in order to obtain a more in-depth understanding of the thermal properties a simple energy model was developed.



Analytic Software: DesignBuilder

DesignBuilder is a design modeling and simulation program providing information on building energy consumption, CO_2 emissions, occupant comfort, LEED compliance, and much more. Once the building features and location is inputted in the program, the simulator will provide information such as heating/cooling loads and allows users to check effects of alternative designs broken down in a range of comprehensive simulation data. Inputting the different façade systems into the simulator will allow for a comparison between the monthly heat gain values of each system.

Building Energy Model: Terra Cotta vs. Brick Veneer

A simple model of the bookstore of the HUB Project was created within the DesignBuilder in order to compare the two façade systems. The model was developed by creating assemblies for the walls and roofs. The results from each model can be compared to one another since other than the façade assemblies themselves, no other features of the building are changing. Two types of reports were generated, an annual ventilation report and a monthly ventilation report.

The effectiveness of the thermal properties of each façade systems were analyzed in each report. Targeting the effective heat gain for the building would help provide which of the two systems would provide better insulation for the building. The monthly heat loss comparison showed that the difference in overall heat loss was less than a percent difference. A month by month break down of the annual heat loss for each system is shown below in Table 7.

	Monthly Heat Loss Comparison (kBTU)											
Description	Jan	Feb	Mar	Apr	May	June	July	Aug	Sept	Oct	Nov	Dec
Terra Cotta	40812	37224	32648	20913	15063	9355	6902	9500	13583	19298	26098	38967
Brick Veneer	40806	37206	32597	20884	15011	9259	6808	9415	13549	19304	26096	38953

Table 7: DesignBuilder Data | RJB

The annual heat gain values that the original façade design experienced is a net loss of nearly 42948 kBTU. The new brick façade design experiences a net loss of 42708 kBTU. When comparing the two values of the original and new façade designs, the brick façade was less than 1 percent more effective in terms of thermal properties. The slight increase in both R-Value and effectiveness of the thermal properties of materials will come along with the change from terra cotta to brick. Graphs produced by DesignBuilder are provided in Appendix D.2 for the internal heat gains of the bookstore.

Mechanical Breadth: Conclusion

Based on the information provided by the HAM Toolbox and the DesignBuilder Software it is clear that new façade design will perform similarly to the current façade design. The R-Values of the systems overall were both similar and will perform well in the environment in University Park. The data output for the monthly heat loss for the brick veneer was slightly more efficient; however it was an insignificant increase. Overall through this mechanical breadth it was determined that the change from the terra cotta rain screen system to the brick veneer will not have a significant factor on the overall thermal performance of the bookstore.

Terra Cotta Rain Screen System vs. Brick Veneer: Component Weight

One of the advantages of implementing a rain screen system into a design is the reduction in the overall building dead load because of the light weight of the cladding options versus traditional building materials. The terra cotta rain screen system consists of similar components of the brick veneer however the light weight of the framing system and panels themselves make the rain screen system considerably lighter.

The terra cotta rain screen system is nearly 62 percent less in overall unit weight per square foot. The terra cotta rain screen system is 25 PSF where the more traditional brick veneer is 65 PSF. The difference is due to the weight of the brick and terra cotta materials themselves since the remaining components of the systems are practically identical. The Structural Breadth deals with the increase in component weight of the brick veneer system.

Structural Breadth

Changing the terra cotta façade to brick veneer brought up an investigation into the existing structural system. The weight of the brick veneer needed to be supported by the structural system. Through this structural breadth, the two systems were compared and the results will help determine whether any changes need to be made to the existing structural system.

One specific beam will be analyzed located on the second floor of the overbuild located between column lines HH and JJ and column line 37. This beam will carry the load of one of the larger spans of exterior façade due to the change in façade type. This beam is a W21x83 at 34' - 10'' in length and is on the exterior of the building. The allowable limits for a typical W21x83 beam are shown below in Table 8. Figure XX shows the location of the specific beam chosen to be analyzed.

Allowable Limits – Steel Beam							
Beam Type	Length	φ Mn	φ Vn	Deflection			
W21x83	34' - 10"	529.20 kip-ft.	238.05 kip	0.663" – 1.097"			



Table 8: Beam Allowance | RJB

Analytic Software: WebStructural

WebStructural is a newer structural engineering software that has the ability to design beams, columns, connections and more. It was designed by a practicing structural engineer and a software developer who created the program to provide an elegant and powerful structural engineering software. In order to calculate a design a steel beam the program follows 6 essential steps to design a steel beam:

- 1. Material Choose the appropriate grade of steel for the beam you will be designing
- 2. Shape Select the shape of steel beam you would like to design.
- 3. Span Enter the distance you are trying to span.
- 4. Bracing Not to be overlooked! Bracing is critical in determining the capacity of a beam.
- 5. Load Enter loads base on their type and load case
- 6. Design- (ASD and LFRD)

After inputting the essential information required by the program, the results are provided to determine if the beam design is acceptable. The program uses the allowable capacity for bending (ϕM_n), shear (ϕV_n), and deflection (Max D_y) and compares the demand for each due to the loading inputted. Both the terra cotta façade and the brick veneer façade were inputted into the system to check each design.

Loading: Terra Cotta Façade

The original terra cotta façade system was used to calculate loading allowances to compare the new design to. Using the WebStructural Beam Design software the terra cotta system loading was plugged into the system to check for bending, shear, and deflection. The information obtained from the terra cotta results are shown below in Table 9.

Table 9	: Terra	Cotta	Loading	RJB
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Terra Cotta Facade – Design Loads								
Total Load	Mu	Vu	Deflection					
1.15 kip / ft.	219.52 kip-ft.	21.83 kip	0.57"					

Typical loading values were used for live and dead loads on the beam, including the dead load from the weight of the terra cotta façade system. The results showed that the loading for the system was acceptable as designed. After determining the structural member performance with the original façade design, the new brick veneer façade was analyzed. As mentioned in the previous section, the brick veneer system has an increased weight than the terra cotta and with this an increase in loading, moments, shear, and deflection is expected. Screenshots of the results from WebStructural Beam Design program for the terra cotta façade are located in Appendix E.2-E.3.

Loading: Brick Veneer Façade

The same loading calculations were performed to determine how the structural member would react when loaded with the brick veneer façade system. The WebStructural Beam Design software calculated the loading for bending, shear, and deflection. The information obtained from the brick veneer results are shown below in Table 10.

Brick Veneer Facade – Design Loads								
Total Load	Mu	Vu	Deflection					
1.84 kip / ft.	346.41 kip-ft.	34.45 kip	0.94"					

Table 10: Brick Veneer Loading | RJB

The results showed that the loading for the new system were acceptable. As expected with the increase in weight of the system brought and increase in demand for the bending, shear, and deflection. The existing W21x83 beam at 34'-10" in length provides sufficient support to carry the increased load. With the change in façade type, both the moment and shear increased by 57.8%. The loading difference between the systems was increased by 0.69 kip/ft. which is a 60% increase from the original design. Table 11 shows the demand of the two different systems and the capacity of the beam.

Table 11: Facade Loading Comparison | RJB

Façade Loading Comparison							
Description	Total Load	Mu	Vu	Deflection			
Terra Cotta System	1.15 kip / ft.	219.52 kip-ft.	21.83 kip	0.57"			
Brick Veneer System	1.84 kip /ft.	346.41 kip-ft.	34.45 kip	0.94"			
Percent Increase	60%	57.8%	57.8%	64.9%			

The WebStructural calculation results for both façade systems are provided in Appendix E.2-E.3.

Structural Breadth: Conclusion

As previously mentioned, regardless of the increases the existing structural member will support the additional load of the new façade design. Due to the large increase in loading, moment, shear and deflection it is assumed that there will be some structural members that will require upsizing as result of the increased load.

Constructability Issues

With the overall dimensions difference of each wall system being 1.125" the transition from each façade type must be looked at to make up for the greater dimension of the brick veneer. The current design calls for an area which facilitates the transition between different exterior façade components; such as the terra cotta rain screen and the glazed aluminum curtain wall. Figure 12 below shows a detail of the transition from between the rain screen and curtain wall. Another area of issue that needs to be addressed is the vertical transition between components.

At the MPR the aluminum glazed curtain wall is topped off by the terra cotta base. In this situation the change from terra cotta to brick would cause the brick to stick out by the 1.125" compared to the curtain wall. However due to the location of the design being at the parapet the extra depth can be absorbed into the parapet itself.



Schedule Impact

In order to figure out the schedule impact of switching from the terra cotta rain screen system to the brick veneer focus shifts towards the exterior of the bookstore. The bookstore exterior is comprised of the following building façade types: Terra Cotta Rain Screen, Aluminum Curtain Wall, and Brick Veneer. Focusing on the south façade of the bookstore, the terra cotta rain screen system's original duration is 35 days which equates to approximately 6.3 square feet installed per hour. The brick veneer can be installed at a rate of 7.8 square feet per hour and replacing the same square footage on the south façade of the bookstore totaling approximately 29 days. The switch in façade equates to a 20 percent saving in overall duration and eliminates over a week worth of installation time. Table 12 shows the breakdown of the durations for the south façade of the bookstore.

Table 12: Bookstore Facade Schedule Comparison | RJB

Schedule Comparison – Bookstore South Façade								
Description	Start Date	End Date	Total Duration					
Terra Cotta Rain Screen	02 December 2013	17 January 2014	35 Days					
Brick Veneer	02 December 2013	09 January 2014	29 Days					

Cost Impact

Still focusing on the south façade of the bookstore the overall cost of the material and labor is approximately \$64,144.00 less for the switch to brick veneer. The total material cost was calculated using material cost per square foot and the amount of façade being changed from the terra cotta rain screen system to the brick veneer. The labor costs were calculated by using the durations calculated previously for the schedule comparison between the two systems. Table 13 shows the cost breakdown for the south façade of the bookstore. Due to the 20 percent decrease in overall duration it provides a labor cost of \$5,520.00 less with the implementation of the brick veneer. Most of the savings comes from the cost of the materials itself, with terra cotta costing \$33 per square foot more than brick. For the south façade of the bookstore alone it provides a savings of approximately \$58,624.00 with the use of brick veneer.

Table 13: Bookstore Facade Cost Comparison | RJB

Cost Comparison – Bookstore South Façade							
Description	Area	Duration	Material Cost	Material Total	Labor Total	Total	
Terra Cotta Rain Screen	1777 SF	35 Days	\$38 / SF	\$67,505.48	\$32,200.00	\$99,705.48	
Brick Veneer		29 Days	\$5 / SF	\$8,882.30	\$26,680.00	\$35,562.30	
			Difference:	\$58,623.18	\$5,520.00	\$64,143.18	

Looking at the entire building surface area and amount of square footage changing from the terra cotta rain screen system to the brick veneer is 51 percent of the building. The material cost for the brick veneer to cover the nearly 13,813 square feet of the building exterior currently designed for terra cotta will cost \$69,061.00. The price for the brick material itself is only 13 percent the price of the terra cotta. Table 14 below breaks down the material cost differences between the terra cotta and brick.

Cost Comparison – Material Cost								
Description	Area	Material Cost	Material Total					
Terra Cotta Rain Screen	13,813 SF	\$38 / SF	\$524,858.00					
Brick Veneer		\$5 / SF	\$69,061.00					
		Difference:	\$455,797.00					

Table 14: Material Facade Cost Comparison | RJB

Conclusion

Changing the facade type from the terra cotta rain screen to a brick veneer will save both time and money. The change to brick veneer will allow the project to save 6 Days of work during the installation of exterior facade of the bookstore. Overall the project would see a cost savings of \$455,797.00 in material alone and the installation and material cost per the bookstore exterior facade schedule would save \$64,142.18. The terra cotta and brick veneer perform similarly thermally and the structural results accepted both designs. It is recommended that the brick veneer be substituted for the current terra cotta rain screen design in order to save time for the overall project duration.

Analysis # 3: GPS Material Tracking System – Structural Steel

Problem

Due to the amount of student traffic and limited access around the HUB deliveries to the site can be highly problematic. A Just-in-Time delivery method will be implemented on the project for delivery of the structural steel. Maintaining the proper tracking of the pieces delivered to the site will help prevent any delays. Barcodes can be scanned when the pieces are shipped and in route to the site notifying the team of expected delivery times.

Research Goal

This analysis will require research into the most cost effect type of tagging system for steel pieces. The project team will require software to interface with the RFID barcodes to collect the data. Along with an analysis of the tagging system a look into current software available for displaying the data will need to take place. The goal of this analysis is to research the benefit of using RFID tags for the steel erection for material tracking and site logistics.

Methodology

- Obtain steel erection schedule and details
- Identify erection sequence
- Identify required RFID software programs
- Evaluate information to be included on RFID tags
- Determine best method for implementation
- Analyze cost impacts
- Analyze schedule impacts

Resources

- Related Literature
- Gilbane Project Team
- AE Department Faculty & Other Industry Professional(s)
- RFID Tag Specification & Software

PACE Research Aspect

During the 22nd Annual PACE Roundtable held in November great insight was provided into current industry issues and potential solutions for these issues. Information management for the workforce was a topic of the morning break-out sessions. During the session the use of RFID tags were brought up by one of the industry professionals in attendance. Using RFID tags can help eliminate common industry issues through inventory management, receiving shipping accuracy, reducing cycle time, improving product quality, better planning and forecast, and facilitating statistical process control. For a site with tight site logistic, a RFID tagging system can help enhance the ability to keep the project on schedule providing savings in labor costs. A RFID tagging system allows for more accurate and timely deliveries getting the right materials in the right place at the right time. Through proper research into RFID tagging systems a system can be implemented in the HUB project for the steel erection sequence allowing for a multiplicity of benefits to the schedule and cost of the project.

Expected Outcome

This analysis is expected to provide an efficient way of tracking the steel deliveries from the time it leaves the production factory until it is installed and nay required testing is done with the RFID tags. The tracking will provide the project team to better plan the deliveries of all steel throughout the project. In addition, the tracking system will help the steel erection on schedule providing both schedule and cost savings on the overall project.

Background Information

The structural system for the addition to the HUB is comprised of structural steel supports with preengineered bolted connections. The Steel is being fabricated by Supermetal in Rock Hill, South Carolina and will be shipped to the site in State College, PA. With classes out for a week in Spring Semester for Spring Break, Gilbane has chosen this time to have the brunt of the steel trucked in during that time period. With only a week for steel erection of main parts of the addition, having the correct steel pieces on site is crucial to completing the task in the allotted time. During Spring Break the amount of traffic will be cut down however the site is still constricting with narrow limitations for large truck loads to be brought on site. Implementing a GPS tracking system on the steel pieces would allow Gilbane to efficiently track and manage all steel deliveries and erections.

Erection and Sequence

During the week of spring break every piece of steel will be picked directly from the delivery truck and then lifted into place. This one week aggressive schedule will allow for Gilbane to complete a majority of the steel erection when most of the Penn State community is away. Supermetal separated the erection into sixteen different sequences which correlates to Gilbane's seven sequences which are outlined in Figure 13 below. The erection sequence starts with the lobby and shifts towards the atrium/courtyard area ending with the canopy system above.


Inspection and Testing

The inspection and testing of all structural steel fabrication and erection will be performed by an independent Testing Agency under a contract with Penn State University. The contractor must provide the Testing Agency with the following items: Complete sets of approved Shop Drawings, cutting lists, order lists, material bills, shipping lists, mill reports, information as to time and place of all rollings and shipments of materials to shops and field, representative sample pieces, and free and safe access when testing materials.

Field bolted connections need to be accordance with RCSC specifications and wrenches need to be calibrated periodically. A minimum of two bolts in each connection shall be tested and verification of washer position and method of tightening nut must be provided.

All Field welding is to be inspected and tested during fabrication of structural steel assemblies and in accordance with AWS Codes. 100% ultrasonic testing must be accordance with ASTM E-164, for all field full penetration welds. Visual inspection of welds must be performed as well as certify welders and conduct inspections and tests are required.

GPS Software Programs

There are numerous GPS tracking programs available on the market today similar to ones that are used by transportation companies to track the location of their fleet. Systems such as these have multiple benefits one of which is the fact that they have the ability to be an entirely web based GPS tracking system. Being a web based system the information can be viewed on any computer or mobile device such as a tablet or even a smart phone. With the technology integrated into a construction site now is the time to implement GPS tracking systems into the everyday construction world. Intelliwave Technologies is one of the global leaders in providing RFID and GPS material tracking solutions for construction projects.



Intelliwave provides construction projects with the ability to track the location of equipment, personnel and equipment resulting in improved scheduling helping to keep projects on track and on budget. SiteSense materials tracking system by Intelliwave gives total visibility to construction materials and will allow the HUB Project team the ability to track every steel piece from the production facility to the site on campus. The RFID tracking tags can withstand outdoor environments as well as impact from other materials in order to survive the abuse they may face during production, transportation and installation. The battery life of each RFID tag typically lasts 4 years, and each has the ability to be decommissioned from a tag assignment and used multiple times throughout the projects life cycle. This will allow the HUB project team to use a select number of RFID tags throughout the steel erection process on the project.

Implementing SiteSense materials tracking system into a construction project has multiple benefits which include: finding materials faster, it helps reduce material management costs, reduce re-fabrication costs and provides a more predictable construction schedule. Using active RFID tags to track the location of materials on a site will help reduce the amount of time it takes to locate each piece of steel on site. According to Intelliwave Technologies, third party studies have demonstrated that the time to find materials was reduced from 31 minutes to 4 minutes per piece. This will allow the project team to account for each piece of steel in a timely manner on the construction site. The greatest advantage of using the RFID tagging system is the ability to track in real time.

Due to the complexity of location of the project and the limited space available around the site, the justin-time delivery method for the steel is perfect for RFID tagging. The current method calls for trucking in multiple steel deliveries to an offsite location and one by one radioing a truck onsite to make picks from each. The SiteSense materials tacking system will allow the project team to know the location of each piece of steel as it arrives on campus and passes through the gate on site and flagged "Received on Site". This will allow for less times checking that each truck has the right pieces in order to complete the erection sequence. This will help with quality control and allow for the erection sequence to occur without the possibility of delay. The worry of material not showing up on site on time will provide extra cost savings due to reducing the need to re-fabricate items which were lost. RFID tags provide initial benefits as well as long term benefits.

Using SiteSense materials tracking system not only will help predict the schedule on a current project but will help the accuracy of scheduling on future projects. Due to the nature of the fast paced work environment on construction site it is impossible to track the movement of material on a job site from day to day. With the tracking system recording all information to a secure web-based database, information from each construction project will be readily available to help schedule work for future projects.

Choosing Intelliwave Technologies SiteSense Material Tracking System

While researching RFID tagging systems and software Intelliwave Technologies stood out among the rest on multiple accounts. The battery life of the RFID tags for the SiteSense material tracking system allows for the ability to re-use the tags without having to recharge them which other competitors could not provide. A lot of the RFID tagging systems required the installation of high price software onto computers in order to collect the information from each tag. Intelliwave Technologies provides a secure web-based software the helps keep support cost low by having information available from multiple devices through the internet. Figure 14.1 displays a worker accessing tracking data from a tablet. RFID tracking tags can be expensive and with the rugged RFID tags provided by Intelliwave, there is no worry about damage to the technology.

Information on RFID Tags

The SiteSense material tracking system will record the following information in order to provide the project team with necessary information to complete the steel erection on time: tagging, receiving, storing (if necessary), and locating. The project team will have the ability to check the correct steel pieces are en-route to the site. This will ensure that the correct pieces are on each truck and will be on site in time each day for the pick. Since the university has and independent testing agency inspect and test the fabrication and erection the data will not collect testing information in order to allow for reuse of tracking tags. All of the information collected by the RFID tags will be stored and be available throughout the current project and help improve efficiency on future projects.

Schedule Impact

Using the SiteSense material tracking system will be beneficial to the schedule of the steel erection. With the tracking system in place for the steel erection the project team will be able to meet the proposed deadlines for each phase of work. Keeping the steel erection sequence on schedule will allow the Tower Crane to stay on site for a shorter amount of time saving money as well as aesthetically pleasing the university's skyline.

The addition of the tracking system will give the project team the ability to eliminate delays in the erection sequence. This form of quality control will occur from the time the pieces are loaded until each piece is put into place and tested. If there is any steel missing from a shipment the project team will know before they are trucked to campus, saving time on having to wait for missing pieces leading to more efficient shipments.

When erecting a steel structure unforeseen circumstances are inevitable, delays from high winds stop the use of the crane. The quality control from the tracking system will allow for circumstances as such to occur without the worry of further delays from missing steel, testing issues, and other controlled issues. Although there is no exact number of days using the RFID tagging system will save, the ability to have added quality control will help the steel erection sequence run smooth.

Cost Impact

Implementing the GPS tracking system to the steel erection will cost money upfront but this extra cost will directly ensure the schedule is kept on track. With so many schedule issues affecting the project the extra quality control from the tracking system will help maintain the target date.

The cost of each GPS unit is approximately \$350 and with the amount of steel being delivered and used in the construction it would be inefficient to use a different GPS unit for each piece. After examining the delivery schedule for the steel, the amount of pieces per load was looked at to determine the largest truck load that would be delivered which totals 215 pieces. This number is the lowest amount of GPS units that could be used in order to track every piece on every truck load.

The ability to recycle and reuse the GPS units is crucial to lowering the upfront cost that Gilbane will take on as well as limit the service fee during the project. The charge is approximately \$15 per month per device with the devices required activation length for this project being 4 months. The total service charge for 215 devices over the 4 month period would be \$12,900 this would increase with the more units in use and the length each is needed to be in service. The upfront cost of purchasing 215 GPS units would be approximately \$75,250. The overall cost for the GPS tracking system will cost a total of \$88,150 and the cost is outlined in Table 15 below.

GPS Cost Break	down
Description	Cost
GPS Tracking Units (215 Units)	\$75,250
GPS Tracking Service Fee	\$12,900
Total:	\$88,150

Table 15: GPS Cost Breakdown | RJB

Conclusion

Although implementing a GPS tracking system would help the project team immensely with quality control it would be more beneficial for a project of larger scale than the HUB. The project team is confident in the current system in place and it will allow for the steel erection to be completed on time.

The upfront cost of \$75,250 will help the project finish on time but with such a large cost for an addition to an existing building is hard to justify. However with the decrease of price in newer technology over time a GPS tracking system will benefit many construction projects in the future whether it is tracking people, equipment, material and much more.

Analysis # 4: Removal of Habitable Green Roof Design

Problem

Currently the HUB project is on course for a LEED Silver Rating, with the main feature being the habitable green roof above the existing bookstore. With all new construction on campus centered on sustainability and achievement of a LEED rating is a green roof the most efficient step in obtaining a "green building". Typically a habitable green roof requires a substantial structural design to handle the extra load of the roof system. Do the long run benefits of the green roof system outweigh the carbon footprint from its construction? Should other areas of the project be targeted for the LEED points?

Research Goal

The technical analysis for this option will incorporate an in depth look into the additional material required to support the Green Roof system compared to an alternative system. The carbon footprint of the constructing such a system can be compared directly to the schedule in order to find room for acceleration. I intend to compare the long term benefits of a Green Roof to its environmental construction impacts. After analyzing the Green Roof an alternative roofing system will be chosen to compare with the original Green Roof design.

Methodology

- Gain knowledge of green roof systems
 - Including construction methods & long term benefits
- Quantify pros and cons of green roof system
- Look into structural design of bookstore roof
- Compare and contrast the opposing roof systems (cost, schedule, environmental impacts)
- Make recommendation to which overall roof system is the more beneficial

Resources

- Gilbane Project Team (Project Manager: Randy Holman, Project Engineer(s): Derek & Devin)
- AE Faculty (Advisor: Robert Leicht)
- Other Industry Professional(s) (OPP Staff Members)
- Green Roof & Conventional Roofing System Specifications

Expected Outcome

The expected outcome for this analysis is reduced costs and schedule acceleration if the green roof proves to be economically unnecessary. This will allow for further schedule acceleration that is necessary for installation of the green roof. If the redesigned roof system does not disprove the green roof option, it will be recommended that the design remains the same.

Background Information

A 9,681 square foot habitable green roof manufactured by Hydro-Tech Inc. will sit on top of the existing student bookstore. Currently The Pennsylvania State University has multiple building on campus with green roofs however the design for the HUB will be the first habitable green roof on campus. Even though the design is habitable only 17 percent of the total roof area provides the ability for occupation, the remaining area is similar to other green roof designs. Green roofs provide multiple benefits which include the following environmentally friendly characteristics: Reduction of the "heat island" effect, storm water management, beneficial thermal properties, CO_2 sequestering and the use of organic material. Figure 15 below highlight in red the area of the building which will incorporate the green roof.



Figure 17: Green Roof Location | RJB

Current Green Roof Design

As stated previously only a small percentage of the entire green roof design is going to have the ability to be occupied. Table 16 below breaks down the area of the current design of the green roof. The roof assembly for the vegetated roof assembly is the Extensive Green Roof design manufactured by American Hydro-Tech Inc. Extensive Green Roofs are designed to help reduce the "urban heat island" effect and minimize storm water runoff. One key feature of the Extensive Green Roof is shallow growing media required which adds less weight to the roof structure compared to other green roofs. The Extensive Assembly can even be used over metal decking however since it is being implemented over the existing bookstore roof it is going to over concrete. Figure16 shows the design of the green roof and highlights the breakdown of Extensive Assembly and Habitable Walkway Paver.

Green Roof – D	esign Breakd	own
Description	Area	Percentage
Extensive Assembly - Vegetation	7972.5 SF	83%
Ultimate Assembly - Pavers	1708.5 SF	17%
Total:	9681 SF	100%

Table 16: Green Roof SF | RJB



Figure 18: Green Roof Design | RJB

Green Roof Physical Components

The two different types of roofing assembly called out in the design are Extensive Garden Roof Assembly and Ultimate Assembly with roof pavers. The Extensive Assembly consists of multiple layers topped off with a layer of vegetation. Underneath the vegetation there is a layer of growing media on top of a garden drain. The remaining layers that make up the assembly are: Styrofoam, root stop, Hydroflex 30, MM6125 EV-FR and the existing substrate (concrete). Figure 17.1 shows the detail of the assembly provided by Hydro-Tech Inc. The Ultimate Assembly with roof pavers is constructed of similar components with a few alterations.

The Ultimate Assembly from the existing roof surface up to the Styrofoam is the same as the Extensive Assembly except for the extra layer of root stop in the Extensive Assembly. On top of the Styrofoam a layer of paver supports is spaced out evenly in order to help support the pavers themselves. The assembly is topped off by architectural pavers to allow occupants to move around freely. Figure 17.2 shows the detail of the assembly provided by Hydro-Tech Inc. Even though the two assemblies have similarities in physical components the overall loading of the Extensive Assembly is greater. The Extensive Assembly concentrates a load of 35 PSF compared to the Ultimate Assembly which loading is 22 PSF. The difference in loading is due to the weight of the growing media and vegetation required for the green roof itself.



Alternative Design

Keeping the habitable side of the current green roof design was looked into; however due to the schedule and cost savings of using an entirely different roof type an alternate design was created for the entire bookstore roof. In other locations on the building, thermoplastic membrane roofing is being used manufactured by Duro-Last Roofing Inc. This Duro-Last Cool Zone membrane will be a good substitute for the green roof not only because of the saving in cost and schedule but also because of the benefits of the cool roof design.

Cool roofs provide positive benefits in multiple climates such as: significant difference in temperature during hot summer days (compared to traditional roofing materials), help save money and energy during peak cooling demand periods, help reduce urban heat-island effect, and keep moisture out while reflecting ultraviolet (UV) and infrared radiation (IR). These multiple energy savings will allow ease the removal of the green roof, replacing it with an alternative sustainable system.

The Duro-Last Cool Zone system can obtain 1 credit from the U.S. Green Building Council's LEED program and may lead to more credits if combined with other design criteria. The Duro-Last warranty for the product covers materials for 10-20 years. This alternate design provides multiple benefits such as a much lower assembly load for the building to carry.

Alternative Design: Roof Loading

The Duro-Last Cool Zone roofing assembly consists of a 50 Mil polyvinyl membrane which needs to be adhered to the existing roof of the bookstore. Insulation will still be laid down along with the polyvinyl membrane but overall the entire loading is considerably lower. The 50 Mil polyvinyl weighs 0.29 PSF, which compares to the Extensive Green Roof Assembly at 35 PSF.

Schedule Impact

The current green roof design calls for installation of a roof membrane, the green roof / accessories, and the actual planting membrane. The total duration for the green roof design is 55 Days with the installation of the green roof accessories and components accounting for 45 Days. For a project with scheduling issues 55 Days for installation of a new roof design on an existing roof is an area of concern. Table 17 breaks down the durations of the current green roof design.

S	chedule Breakdown – C	urrent Green Roof Desig	n
Description	Start Date	End Date	Total Duration
Roof Membrane	02 December 2013	13 December 2013	10 Days
Green Roof / Accessories	16 December 2013	24 January 2014	30 Days
Install Green Roof - Planting	27 January 2014	14 February 2014	15 Days
		Total Green Roof Duration:	55 Days

Table 17: Green Roof Schedule | RJB

Implementing the Duro-Last Cool Zone design will provide roofing for the same surface area as the green roof in 40 Days shorter. The membrane layer is the only duration required with the Duro-Last design and provides sufficient enclosure for the building. The overall time saving of 8 weeks provides the ability to shift focus towards other physics of the buildings. Table 18 shows the scheduling implications of the Duro-Last and Green Roof and the time savings that come along with it.

	Schedule Breakdowi	n – Duro-Last Design	
Description	Start Date	End Date	Total Duration
Green Roof Assembly	02 December 2013	14 February 2014	55 Days
Duro-Last Assembly	02 December 2013	20 December 2013	15 Days
		Total Difference:	40 Days

Table 18: New Design Schedule Breakdown | RJB

Carbon Footprint Investigation

A research study published in Energy and Buildings Journal shows the overall CO_2 offset of using white roofs and green roofs. Both white roof and green roofs provide sufficient benefits to the environment however green roofs are less reflective and have lower global cooling potential. Compared to typical black roof s, white roofs will offset 10 tons of CO_2 for every 1076 SF of roof area, while green roofs offset 3-4 tons of CO_2 over the lifetime of the roof (Sproul, 2014). This means for the existing roof of the bookstore a white roof would offset nearly 90 tons of CO_2 compared to a green roof which would offset 35 tons of CO_2 over the roofs lifetime. One benefit of the green roof is the ability to help with storm water management. Extensive Green Roofs intercept and retain the first 0.5-0.8 in of rain preventing it from running off. However does the upfront cost of implementing a green roof over a white roof benefit the owner and environment?

Cost Impact

The existing roof of the bookstore does not have to change for the current design green roof design or the alternate Cool Roof design. Changing the green roof design to the Duro-Last Cool Zone Assembly will save the project a total of \$154,896.00 for the 9,681 SF of roof. The Cool Roof design will allow for a 72% reduction in price compared to the green roof design. The cost breakdown below in Table 19 shows the installation and material cost of the Hydro-Tech Roof and the Duro-Last Roof. The total does not include the structure itself since the existing concrete is an approved substrate for both designs.

Cost Comparis	son – Existing	Bookstore Ro	of
Description	Area	Cost / SF	Total Cost
Hydro-Tech Green Roof Assembly	0.601.05	\$22.00	\$212,982.00
Duro-Last Cool Zone Assembly	9681 SF	\$6.00	\$58,086.00
		Difference:	\$154,896.00

Table	19:	Cost	Comparison -	- 1	Roof	Design	RJB
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Conclusion

The removal of the green roof will save both time and money. Implementing a Duro-Last Cool Roof will allow the project to save 40 Days of installation while saving \$154,896.00. It is recommended to substitute the current green roof system with the Duro-Last Cool Zone System.

Report Conclusion

Final Recommendations

Over the fall 2013 and spring 2014 academic year, the HUB Renovations and Addition Project of The Pennsylvania State University was analyzed in order to identify areas that had potential to enhance the project overall. Through countless hours of research, feedback from academic members, the project team, multiple site visits, and construction professionals, four main areas were focused on for further analysis. Sequencing recommendations as well as Last Planner a lean building tactic was analyzed for the bookstore interior schedule. Two of the remaining analysis dealt with schedule saving redesigns, with the other one focused on research into quality control tactics. The purpose of this thesis project is strictly educational and is not intended to critique the work performed by the project team in any way.

Analysis #1: Schedule Resequence

The first analysis addressed the feasibility of resequencing the interior bookstore phase of the original schedule. Analyzing the schedule by decreasing unnecessary float, sequencing improvements, and schedule overlap the schedule was looked to be improved. Areas of the project were looked at in order to accelerate the schedule which later analyses touch on. In addition, the lean principle of Last Planner was investigated for implementation on a project such as the HUB. The project team is encouraged to use the suggested acceleration techniques as well as the idea of Last Planner to make up for schedule delay.

Analysis #2: Terra Cotta Rain Screen Redesign

Nearly half of the renovations and addition on the HUB façade is comprised of a complex terra cotta rain screen. This analysis addresses the need for schedule acceleration by providing an alternative brick veneer design. By switching the rain screen to brick veneer the project was able to save over a week of work days on the exterior façade of the bookstore alone, while saving \$64,143.18. With similar thermal properties analysis and acceptable structural loading, the project team is encouraged to use the alternative design to provide schedule and cost savings.

Analysis #3: GPS Material tracking System – Structural Steel

Topics discussed during The 22nd Annual PACE Roundtable by construction professionals led to the research portion provided in the third analysis. With a Just-In-Time delivery system for the structural steel a GPS tag tracking system will help ensure quality control by preventing schedule delays. The cost of the tracking system is roughly \$88,150 and the schedule would not see any savings. Although the technology to track the steel pieces will promote quality control, implementation would not benefit the project team due to the cost impact on a project of this size.

Analysis #4: Removal of Habitable Green Roof Design

The final analysis looks at the current design of the habitable green roof to be constructed on the existing bookstore roof. Providing an alternative cool roof design will further address the need for schedule acceleration due to unforeseen issues. The alternative design provides a cost savings of \$154,896.00 and a schedule savings of 40 work days. The project team is encouraged to use the alternative design due to the cost and schedule savings of switching the design of an already existing roof structure.

Conclusion

In conclusion, it is recommended that three of the four proposed alternatives are applied to the Hub Renovations and Addition Project on The Pennsylvania State University's campus. Cost savings for the two main redesigns of the exterior façade and green roof would result in a schedule savings of 46 Days for the exterior of the bookstore alone. Further time savings will come from changing the remaining façade of the exterior of the building. These two analyses will also provide considerable cost savings totally nearly \$220,000.00 for the bookstore exterior alone. Using lean construction principle and total resequencing of the project will help keep the project on track as the project team deals with potential scheduling issues. As a result, the three of the four analyses are recommended as they will benefit the HUB Renovations and Addition Project.

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A.1: Original Bid Schedule

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Construction	503 27-Feb-13 06-Feb-15		5, Construction
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💼 Prepare Site for Trallers	26 04-Apr-13 09-May-13	3y-13	
Set Up Book Store Trailers		n-13 m-19 book store traers	
Interior Contratuction: Book Store	20 03-Jun-13 28-Jun-13		
🚃 Exterior Façade @ Book Store	5 13-Jun-13 19-Jun-13	n-13	
Obtain CO Temporary Book Store	3 01-Jul-13 03-Jul-13		
Relocate Temporary Book Store / Reopen for Busine	10 01-Jul-13 15-Jul-13		
L & I Inspection Book Store Trailer	2 01-Jul-13 02-Jul-13	L & All Inspection Body Store Frailer	
Tower Crane	256 30-May-13 28-May-14		
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F/R/P Tower Crane Foundation	9 27-Jun-13 10-Jul-13	13	
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Tower Crane Installation	i.		
Remove Tower Crane	26 09-Apr-14" 14-May-14		
Close Crane Opening			
Phase 2: Bookstore Interior/Exterior	292 31-May-13 18-Jul-14		
Interior	292 31-May-13 18-Jul-14		
Fit Out Computer Store / 110 / 235	10 31-May-13 13-Jun-13	Fit Out Compilier Store / fito / 285	
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Demolition Bookstore Interlor	34 D5-Jul-13 21-Aug-13		
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Erect Strucutral Steel Mezzanine	20 14-Oct-13 08-Nov-13	Pr-13 Erect Stripturtral Steel Mezzbanne	
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AE Senior Thesis | Appendix 45





AE Senior Thesis | Appendix 47



Robert Justin Barlow | Construction Option | April 9th, 2014 FINAL REPORT

A.2: Gilbane's Preconstruction Bid Schedule

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B: Thermal Properties

Descsription		Density lb/ft(3)	Conductivity (k)	Conducance (C)	Per Inch Thickness	For Thickness Listed	Specific Heat
Descarption		Density ID/11(3)	Btu-in./h ft(2) F	btu h/ft(2) F	(1/k) F ft(2) h BTU-in	(1/C) F ft(2) h Btu	Btu/lb F
Terra Cotta							
Terra Cotta Panel		114	2.5				0.21
2.5" Mineral Wool		4	0.25		4		0.232
AVB Membrane		0	16.7		0.12		0
1/2" Ext Sheathing		34	0.8	3.2	1.25	0.31	0.29
6" Metal Stud		12	0.166				0.168
Brick Veneer (OLD)							
3 5/8" Brick		120	0.42				0.2
Airspace		0	0				0
2.5" Mineral Wool		4	0.25		4		0.232
AVB Membrane		0	16.7		0.12		0
Exist. Concrete		140	1				0.22
Metal Panels							
2.5" Mineral Wool		4	0.25		4		0.232
AVB Membrane			16.7		0.12		
1/2" Ext Sheathing		34	0.8	3.2	1.25	0.31	0.29
6" Metal Stud							
Brick Veneer (NEW)							
3 5/8" Brick		120	0.42				0.2
Airspace		0					0
2.5" Mineral Wool		4	0.25		4		0.232
AVB Membrane		0	16.7		0.12		0
1/2" Ext Sheathing		34	0.8	3.2	1.25	0.31	0.29
6" Metal Stud		12	0.166				0.168
Green Roof							
Earth	4	100	0.45				0.2
Polyiso Foam	2.5	1	0.0133				0.29
Concrete	4	140	1				0.2
Ceiling Air Space	24						0

C.1: HAM Toolbox Terra Cotta

TOOL NO. 1 R VALUE ANALYSIS							CLIMATE CONDITIONS Winter Summer Temp(°F) RH(%) Temp(°F) RH(%) Indoor 70 25 75 50 Outdoor 1 67 104 72				
МАТЕ	ERIALS							City Williamsport, PA			
cavity	, 1 in.	•	ł	<u>t</u> elp	<u>5</u> 1	ART/CLR					
Ad	d De <u>l</u> ete	Move <u>u</u> p	Mo	ove <u>d</u> n		Con <u>v</u> ert	(°F) 160 -	WALL SECTION & (°F) TEMPERATURE GRADIENTS 160			
<u>C</u> a	lc <u>G</u> raph	Print	W	allLyb	I	OOLBOX	140 ·				
Layer	Generi	c Material		Thic	<.	R Val.	120 ·				
1	air film (ext), 3/4 in.			0.7	5	0.17	100 -				
2	Terra Cotta bl	k., 2 in.		2.00		0.54	100				
3	semi-rigid ins.	, 2-1/2 in.		2.50		8.90	80 -	- 80			
4	poly film, (6m	il)		0.01		0.12	60 ·				
5	plywood shtg.,	. 1/2 in.		0.50		0.64	00				
6	steel stud, 5-1	/2 in.		5.51		0.12	40 ·	40			
7	air film (int), 3	/4 in.		0.7	5	0.64	20 -	20			
8							20	20			
9							0 -				
10							-20 -				
11							-20	0 4 0 8 12 16			
12								(inches)			
	Total or (Lay	er 0)		10.5	2	11.12		 Standard Wall Wider Wall 			
•						•					

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C.2: HAM Toolbox Brick Veneer

TOOL NO. 1 R VALUE ANALYSIS									Te loor	W	DITION inter) RH(1 25	%)	Su Temp(* 75 104	E	
MATERIALS								City Williamsport, PA							
cavity	r, 1 in		•	<u>H</u> e	elp	<u>S</u> TART/C			.,						
Add Delete Move		Move <u>u</u> p	Move <u>d</u> n		Convert		(°F) WALL SECTION & (°F) TEMPERATURE GRADIENTS								
<u>C</u> a	lc	<u>G</u> raph	<u>P</u> rint	Wal	ILyb	TOOLBO		140 -	Ext					Int	-140
Layer		Generic	Material		Thick	. RVa	il. 1	120 -			X				-120
1	air film (ext), 3/4 in.				0.75	i 0.1	7 1	100 -			Ď				-100
2	brick	(TTW), 4 ir	۱.		4.00	0.6					(\mathbf{X})				100
3	cavi	ly, 1 in.			1.00	9.0	8	80 -	_		(>)				- 80
4	sem	i-rigid ins., 2	2-1/2 in.		2.50	8.8	0	60 -			$\left \right\rangle$				- 60
5	poly	film, (6mil)			0.01	0.1	2			V////					
6		ood shtg., 1			0.50	0.6	4	40 -		V////					- 40
7		l stud, 5-1/2			5.51	0.1	0.12 20				- 20				
8	air fi	lm (int), 3/4	in.		0.75	5 0.E	4								20
9								0 -	_						- 0
10								-20 -							20
11								20	0	4	8		2 16		-20
12											(inc	hes)			
					13.52	12.1	9		<u>ে</u> ৎ†	andaro	l Wall	0.1	Wider \	Vall	
•									~ <u></u>	andar				Tail	

D.1: DesignBuilder Screenshots

FINAL REPORT Robert Justin Barlow | Construction Option | April 9th, 2014

template	PA - WILKES-BARRE/S
Site Location	
Latitude (")	41.32
Longitude (")	-75.72
Site Details	
Elevation above sea level (ft)	948.2
Exposure to wind	2-Normal
Site orientation (")	0
Ground	
Water Mains Temperature	
Precipitation	
Site Green Roof Irrigation	
Time and Daylight Saving	
2aTime zone	(GMT-05:00) Eastern Time (US & Canada)
Use daylight saving	
Start of Winter	Oct
End of Winter	Mar
Start of Summer	Apr
End of Summer	Sep
Simulation Weather Data	
🖰 Hourly weather data	USA_PA_WILKES-BARRE-SCRANTON INTL AP_T
Winter Design Weather Data	
Heating 99.6% coverage	
Outside design temperature (°F)	2.8
Wind speed (ft/min)	2185.1
Wind direction (")	0.0
O Heating 99% coverage	
Summer Design Weather Data	

🔍 Legislative Region		×
Region	Pennsylvania	
😵 Energy Codes / Insulation Standards		¥
✤Uninsulated	Uninsulated	
Typical	IECC-1998	
Mandatory energy code	IECC-2000	
🐵 Best practice	Cold winter 'best practice'	

-	Edit construction	- Terra Cotta								
uil	Constructions	Data			Help					
tior	Layers Surface	properties Image Calculated Cond	lensation analysis		Info Data					
	General		×	Construction Laye	ers					
	Name	Terra Cotta				ayers first, then sele	ect the material			
	Source				and thickness for each layer.					
	Category		Walls	•	🕂 Insert layer					
	Region		General		X Delete layer					
	Calculation Se	ttings		>>						
	Layers				Bridging	oridging to any layer	to model the			
	Number of la		6	-	effect of a relatively	more conductive m	aterial bridging			
	Outermost la	·			a less conductive material. For example wooden joi briging an insulation layer.					
	Materia	d	Terra Cotta			ects are NOT used in I	EnergyPlus but			
	Thickness		0.120		are used in energy co	de compliance checks	requiring			
	Bridged	?			u-values to be carcul	ated according to BS E	:11/130/0940.			
	Layer 2	1	Metals - aluminium		Energy Code Com					
	⇒Materia		0.220		You can calculate t	he thickness of insu tory energy code U-	lation required			
	Thickness		0.220	•	the Energy Code ta	ib at site level.	value as set on			
	Layer 3					ntifies the 'insulation				
	Materia	1	Mineral fibre/wool - wool		layer having the hig bridging is used in	phest r-value and re- the construction.	quires that no			
	Thickness		2.500		Z Set U-Value					
	Bridged				Set 0-value					
	Layer 4			×						
	Materia	d	Vapor: seal, 2 layers of mopped 0	.73 kg/						
	Thickness	(not used in thermal calcs) (in)	0.200							
	Layer 5			×						
	Materia	d	Wood derivatives - plywood							
	Thickness		0.500							
	Bridged									
	Innermost la		Metala starl							
	Materia		Metals - steel 6.000							
	Thickness	· · ·	0.000							
		1								
	Model data		Insert layer Delete	layer	Help	Cancel	ОК			
					· · · · · · · · · · · · · · · · · · ·					
Edit construction - Project wall										
---	---------------------------------------	--								
Constructions Data		Help								
Layers Surface properties Image Calculated Condensation and	alysis	Info Data								
General	*	Construction Layers								
Name Project wall		Set the number of layers first, then select the material and thickness for each layer.								
Source										
Category	Walls 🔹	Insert laver								
Region	Pennsylvania	× Delete laver								
Calculation Settings	»	Duidaina								
Layers	×	Bridging You can also add bridging to any layer to model the								
Number of layers	4	effect of a relatively more conductive material bridging a less conductive material. For example wooden joists								
Outermost layer		briging an insulation layer.								
⊘Material Thielmana (in)	3.937	Note that bridging effects are NOT used in EnergyPlus, but								
Thickness (in) Bridged?	3.337	are used in energy code compliance checks requiring U-values to be calculated according to BS EN ISO 6946.								
Layer 2	*									
Material	XPS Extruded Polystyrene - CO2 Blowin	Energy Code Compliance You can calculate the thickness of insulation required								
Thickness (in)	3.130	to meet the mandatory energy code U-value as set on								
Bridged?		▶ the Energy Code tab at site level.								
Layer 3	*	This calculation identifies the 'insulation layer' as the layer having the highest r-value and requires that no								
Sy Material	Concrete Block (Medium)	bridging is used in the construction.								
Thickness (in)	3.937	2 Set U-Value								
Bridged?										
Innermost layer	×									
Material	Gypsum Plastering									
Thickness (in)	0.512									
Bridged?										
Model data	Insert layer Delete layer	Help Cancel OK								

Edit construction - Project flat roof		
Constructions Data		Help
Layers Surface properties Image Calculated Condensation a	inalysis	Info Data
General	×	Construction Layers
Name Project flat roof		Set the number of layers first, then select the material and thickness for each layer.
Source		
Category	Roofs •	🖶 Insert layer
Region	Pennsylvania	Delete layer
Calculation Settings	»	Deideire
Layers	×	Bridging You can also add bridging to any layer to model the
Number of layers	4	effect of a relatively more conductive material bridging
Outermost layer	*	a less conductive material. For example wooden joists briging an insulation layer.
⊘Material	Asphalt 0.394	Note that bridging effects are NOT used in EnergyPlus, but
Thickness (in) Bridged?	0.394	are used in energy code compliance checks requiring U-values to be calculated according to BS EN ISO 6946.
Layer 2	*	
Material	MW Glass Wool (rolls)	Energy Code Compliance You can calculate the thickness of insulation required
Thickness (in)	5.689	to meet the mandatory energy code U-value as set on
Bridged?		the Energy Code tab at site level.
Layer 3	¥	This calculation identifies the 'insulation layer' as the layer having the highest r-value and requires that no
SyMaterial (Air gap >=25mm	bridging is used in the construction.
Thickness (not used in thermal calcs) (in)	7.874	Z Set U-Value
Innermostlayer	*	
Material	Plasterboard	
Thickness (in)	0.512	
Bridged?		
Model data	Insert layer Delete layer	Help Cancel OK

D.2: DesignBuilder Graphs

Graph – Terra Cotta



Graph – Brick Veneer



D.3: DesignBuilder Outputs

ZONE	ZONE	ZONE	ZONE
PEOPLE	LIGHTS	ELECTRIC	INFILTRATION
			SENSIBLE
			HEAT LOSS
			[kBtu]
[kBtu]	[kBtu]	[kWh]	[·]
8394.35	18217.35	3654.68	40812.24
7299.44	15841.18	3192.23	37224.06
7664.41	16633.24	3373.68	32648.13
8029.38	17425.29	3500.53	20913.30
8394.35	18217.35	3654.68	15063.05
7299.44	15841.18	3219.53	9355.47
8394.35	18217.35	3654.68	6902.95
8029.38	17425.29	3514.18	9500.46
7664.41	16633.24	3360.03	13583.00
8394.35	18217.35	3654.68	19298.65
7664.41	16633.24	3360.03	26098.04
8029.38	17425.29	3514.18	38967.50
	2005227.20	41652.10	270244.04
95257.64	206/27.36	41653.10	270366.86
7299.44	15841.18	3192.23	6902.95
8394.35	18217.35	3654.68	40812.24
	PEOPLE TOTAL HEAT GAIN [kBtu] 8394.35 7299.44 7664.41 8029.38 8394.35 7299.44 8394.35 8029.38 7664.41 8394.35 7664.41 8029.38 95257.64 7299.44	PEOPLE TOTAL HEAT GAIN [kBtu] LIGHTS TOTAL HEAT GAIN [kBtu] 8394.35 18217.35 7299.44 15841.18 7664.41 16633.24 8029.38 17425.29 8394.35 18217.35 7299.44 15841.18 7664.41 16633.24 8029.38 17425.29 8394.35 18217.35 8029.38 17425.29 7664.41 16633.24 8394.35 18217.35 7664.41 16633.24 8394.35 18217.35 7664.41 16633.24 8029.38 17425.29 7664.41 16633.24 8029.38 17425.29 95257.64 206727.36 7299.44 15841.18	PEOPLE TOTAL HEAT GAIN [kBtu] LIGHTS TOTAL HEAT GAIN [kBtu] ELECTRIC EQUIPMENT TOTAL HEAT GAIN [kBtu] 8394.35 18217.35 3654.68 7299.44 15841.18 3192.23 7664.41 16633.24 3373.68 8029.38 17425.29 3500.53 8394.35 18217.35 3654.68 7299.44 15841.18 3219.53 8394.35 18217.35 3654.68 7299.44 15841.18 3219.53 8394.35 18217.35 3654.68 8029.38 17425.29 3514.18 7664.41 16633.24 3360.03 8394.35 18217.35 3654.68 7664.41 16633.24 3360.03 8394.35 18217.35 3654.68 7664.41 16633.24 3360.03 8029.38 17425.29 3514.18 7664.41 16633.24 3360.03 8029.38 17425.29 3514.18 95257.64 206727.36 41653.10 7299.44 15841.18

Output – Terra Cotta

	ZONE PEOPLE TOTAL HEAT GAIN [kBtu]	ZONE LIGHTS TOTAL HEAT GAIN [kBtu]	ZONE ELECTRIC EQUIPMENT TOTAL HEAT GAIN [kWh]	ZONE INFILTRATION SENSIBLE HEAT LOSS [kBtu]
January	8394.35	18217.35	3654.68	40806.65
ebruary	7299.44	15841.18	3192.23	37206.79
March	7664.41	16633.24	3373.68	32597.73
April	8029.38	17425.29	3500.53	20884.43
May	8394.35	18217.35	3654.68	15011.84
June	7299.44	15841.18	3219.53	9259.81
July	8394.35	18217.35	3654.68	6808.29
August	8029.38	17425.29	3514.18	9415.90
ptember	7664.41	16633.24	3360.03	13549.01
October	8394.35	18217.35	3654.68	19304.45
vember	7664.41	16633.24	3360.03	26096.85
cember	8029.38	17425.29	3514.18	38953.66
Annual Sum or Average	95257.64	206727.36	41653.10	269895.41
linimum Months	7299.44	15841.18	3192.23	6808.29
laximum Months	8394.35	18217.35	3654.68	40806.65

Output - Brick Veneer

D.4: Model Images







D.5: Student Bookstore Drawing Document



E.1: Structural Loads

Terra Cotta – Dead Load

Self-weight: (WebStructural accounts for this already)

Slab Weight: 45 PSF

Superimposed: 15 PSF

TC System Weight: 25 PSF

Brick Veneer - Dead Load

Self-weight: (WebStructural accounts for this already)

Slab Weight: 45 PSF

Superimposed: 15 PSF

BV System Weight: 65 PSF

Live Load – Both Systems

Classroom: 40 PSF

Partitions: 20PSF

Conversions

Slab Self-weight:	$\frac{45lb}{ft^2} \times \frac{1kip}{1000lb} \times 6.25ft = 0.28125\frac{kip}{ft}/ft$
Superimposed:	$\frac{15 lb}{ft^2} \times \frac{1 kip}{1000 lb} \times 6.25 ft = 0.09375 \frac{kip}{ft}$
Terra Cotta:	$\frac{25lb}{ft^2} \times \frac{1kip}{1000lb} \times 15.5ft = 0.3875 \frac{kip}{ft}$
Brick Veneer:	$\frac{65lb}{ft^2} \times \frac{1kip}{1000lb} \times 15.5ft = 1.0075\frac{kip}{ft}$
Live Load (C):	$\frac{40lb}{ft^2} \times \frac{1kip}{1000lb} \times 6.25ft = 0.3875kip/ft$
Live Load (P):	$\frac{20 lb}{ft^2} \times \frac{1 kip}{1000 lb} \times 6.25 ft = 0.3875 \frac{kip}{ft}$

Total Loading (TC): 0.77 k/ft

Total Loading (BV): 1.46 k/ft

Total Loading (LL): 0.38 k/ft

E.2: WebStructural – Terra Cotta Loading





🖋 Design OK	LRFD	W21X83	A992
🖋 Bending	0.41		0.
MU (Demand)	219.52 kip-ft	Vu (Demand)	21.8
Φ Mn (Capacity)	529.20 kip-ft	ΦVn (Capacity)	238.0
Controlling Equation Location	F2.1: Yielding 17' 5"	Controlling Equation	G2.1: Nominal Shear Strength
Load Combo	1.2D + 1.6L + 0.5Lr	Location	(
		Load Combo	1.2D + 1.6L + 0
Deflection	0.57	Design Info	

V Deflection	0.57
Based On	Service Cases
Max Service Case	Wind Limit
Max Dy	-0.666 in = L/630
Live Load Limit	L/360
Dead + Live Limit	L/360
Snow or Wind Limit	L/360
Total Load Limit	L/240

Design Info	
Shape Type	W21X83
Weight	83.00 lbs/ft
Self Weight	Included
Ix	1830.00 in 4
Bracing	Continuous Bracing

E.3: WebStructural – Brick Veneer Loading



🗲 Design This Beam

🖋 Design OK

LRFD

W21X83

```
A992
```

🖋 Bending	0.65
MU (Demand)	346.41 kip-ft
Φ Mn (Capacity)	529.20 kip-ft
Controlling Equation	F2.1: Yielding
Location	17' 5"
Load Combo	1.2D + 1.6L + 0.5Lr

Deflection	0.94
Based On	Service Cases
Max Service Case	Wind Limit
Max Dy	-1.097 in = L/390
Live Load Limit	L/360
Dead + Live Limit	L/360
Snow or Wind Limit	L/360
Total Load Limit	L/240

🖋 Shear	0.14
Vu (Demand)	34.45 kip
ΦVn (Capacity)	238.05 kip
Controlling Equation	G2.1: Nominal Shear Strength
Location	0' 0"
Load Combo	1.2D + 1.6L + 0.5Lr

Design Info	
Shape Type	W21X83
Weight	83.00 lbs/ft
Self Weight	Included
Ix	1830.00 in 4
Bracing	Continuous Bracing

F: Typical Brick Relief Detail at Slab



G: Green Roof Details





H: SF Green Roof Design



I: Presentation Slides

SLIDES WILL BE ADDED ON PRESENTATION DAY