

THE PENNSYLVANIA STATE UNIVERSITY MILLENNIUM SCIENCE COMPLEX



**MECHANICAL TECHNICAL REPORT ONE:
BUILDING/PLANT ENERGY ANALYSIS &
MECHANICAL SYSTEMS EXISTING CONDITIONS**

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EXECUTIVE SUMMARY

The Millennium Science Complex is a four story, 275,600 SF square foot, LEED Gold Certified laboratory and office facility for the Life and Materials Sciences on The Pennsylvania State University, University Park campus. Located on the eastern end of campus at the corner of E. Pollack and Bigler Rd, the Millennium Science Complex will be the focus of the Integrated Project Delivery / Building Information Modeling Thesis (IPD/BIM Thesis). The building will house research facilities for the Material Sciences and Life Sciences departments. This report provides a preliminary investigation of the existing mechanical conditions and building/plant loads. From the basis of this analysis, we will be able to propose and investigate other design options in future reports.

The third floor of the Millennium Complex, roughly 45,000 SF, was selected as the focus of the building for this analysis and will be more strictly studied throughout the progression of our research. This floor provides a unique opportunity to study both life and material science laboratories, while incorporating common offices and conference rooms. The third floor is within the scope of a detailed analysis while providing complex interactions between all disciplines. While the whole building will be considered on a holistic level, actual calculations, coordination, and analyses in this report focus solely on the third floor.

The Millennium Science Complex's mechanical system assists the project with energy savings and result in a LEED Gold certification. An energy analysis of the third floor yielded 22% energy savings when compared to an ASHRAE Standard 90.1 model. Based on this comparison, the design of the entire building is expected to achieve 14% energy savings. The mechanical systems required for the varying uses of the Complex occupy approximately 15% of the building's total area. An estimation of the cost of the system was not attainable at the time of this report.

As part of the IPD/BIM Thesis, the mechanical reports will approach mechanical design with the purpose to create synergies with the architectural, lighting, electrical, environmental, and construction facets of design. By creating a more integrated design process, research should evolve a building design that improves the quality of its occupants' lives while decreasing the impact of the building on the environment.

This report begins the mechanical analyses that will be a part of the integrated design process. This paper develops the existing load, system, and energy conditions, so that future improvements may be tracked and compared. It begins with a general description of standards and design assumptions used to accurately model the functions and conditions of the Millennium Science Complex. This report goes on to create an analysis of the energy expended by the operation of the building along with its cost and environmental impacts. The major systems will be broken down for an understanding of their function. And finally, this report will provide insight into how Integrated Project Delivery and Building Information Modeling have been utilized to improve our analyses.

BUILDING OVERVIEW

The Millennium Science Complex is a four story laboratory facility that will combine the research of the Life Sciences and Material Sciences departments at Penn State under one roof. The building consists of stepping, green roofed, cantilevers that extend over campus streets, and will surely become one of the most recognizable buildings on the University Park campus.

The Millennium Science Complex also contains several outstanding sustainable features that will enable the project to attain LEED Gold certification. Green roofs cover the massive cantilevers and drain into a cistern to help reduce stormwater runoff. During construction over 90% of waste was diverted from disposal and over 10% of building materials were from recycled content. The complex mechanical system of the building employs an energy saving design that will reduce impact on the environment throughout the lifetime of the building.

A reliable and sustainable mechanical system is needed within the Millennium Science Complex In order to serve the varying occupants and uses. Laboratory spaces require consistent thermal and air quality conditions to ensure the accuracy of experiments. Laboratory AHUs contain energy recovery devices to offset energy costs associated with the higher indoor air quality requirements. Office spaces need to be designed for the comfort of their occupants with CO₂ measuring devices in dense areas to ensure indoor air quality standards are maintained.

The 4th floor of the building, which serves as the mechanical penthouse, and space in the basement of the building are used to connect into the existing campus chilled water and steam lines here at Penn State. The incoming high pressure steam is reduced to medium and low pressure steam for use in AHU coils, for process loads, and for the production of hot water through heat exchangers. Chilled water is pumped to the mechanical penthouse with the use of variable speed spilt case pumps.

DESIGN OCCUPANCY

At full capacity The Millennium Science Complex is designed to hold 2,898 occupants, not including the number of occupants under its first floor exterior atrium. Specifically, the third floor is designed for 735 persons. Given the office and laboratory functions of the floor, we will assume it to have 20% diversity for future calculations.

Table 3: Occupancy Per Floor

| Floor | Occupants |
|--------------------|-----------|
| Basement | 462 |
| Basement Mezzanine | 48 |
| First Floor | 573 |
| Second Floor | 987 |
| Third Floor | 735 |
| Penthouse | 93 |
| Total | 2,898 |

The energy model used ASHRAE Standard 62.1 Table 6-1 as a basis for occupancy densities using the, “Space by Space Analysis.” These values were reviewed and corrected to more accurately match the building’s function and load. Each office containing at least three chairs was assumed to have 2 occupants. Each grad student cubicle was assumed to be an occupant. A diversity factor of 80% will also be added to account for periods off- peak occupancy.

Table 4: Excerpt from ASHRAE Standard 62.1 Table 6.1 Minimum Ventilation Rates in Breathing Zone

| Occupancy Category | Occupant Density (#/1000 ft ²) |
|-------------------------|--|
| Lecture Classroom | 65 |
| Science Laboratories | 25 |
| Wood/Metal Shop | 20 |
| Computer Lab | 25 |
| Restaurant Dining Rooms | 70 |
| Break Rooms | 25 |
| Conference/Meeting | 50 |
| Office Space | 5 |
| Corridors | - |
| Storage Rooms | - |

DESIGN LIGHTING & EQUIPMENT LOADS

Lighting power density loads were taken from ASHRAE Standard 90.1 Table 9.6.1 on a Space by Space Analysis. Each space was assigned a Common Space Type that best fit its function.

Internal equipment receptacle loads were assumed to match the default values supplied by Autodesk Revit MEP 2011 load calculation on a Space by Space Analysis. Given each type of space, a corresponding default load was applied.

Table 5: Lighting and Equipment Power Densities, using a Space by Space Method

| Common Space Types | LPD , W/ft ² | EPD , W/ft ² |
|---------------------------------|-------------------------|-------------------------|
| Office –Enclosed | 1.1 | 1.5 |
| Office – Open Plan | 1.1 | 1.5 |
| Conference/Meeting/Multipurpose | 1.3 | 1.0 |
| Classroom/Lecture/Training | 1.4 | 1.0 |
| Lounge/Recreation | 1.2 | 0.5 |
| Dining Area | 0.9 | 0.5 |
| Food Preparation | 1.2 | 1.5 |
| Laboratory | 1.4 | 1.5 |
| Restrooms | 0.9 | 0.3 |
| Corridor/Transition | 0.5 | 0.3 |
| Stairs - Active | 0.6 | 0.3 |
| Active Storage | 0.8 | 0.3 |
| Inactive Storage | 0.3 | 0.3 |
| Electrical/Mechanical | 1.5 | 0.3 |
| Post Office – Sorting Area | 1.2 | 1.0 |

DESIGN SCHEDULES

As a university laboratory facility the Millennium Science Complex has a unique schedule of operations. Three sets of schedules were created to estimate the actual usage of the building. These schedules will help to accurately model the energy expenditure. Each hour was assigned a percentage of assumed peak occupancy. From the hours of 6am-8am and 6pm-8pm, it is assumed to be at 30% peak occupancy. For 8am-11am and 1pm-6pm, the building is assumed to be at peak occupancy during school hours. There is an assumed 85% occupancy for lunch hours, and no occupancy for a nighttime setting. Being a research facility, there is potential for it to be operational during the weekend, so a 50% occupancy rate was assigned to Saturday and Sunday. The schedules created were assumed since no operational schedules were provided and templates within Trane TRACE did not correlate with the anticipated usage of the building.

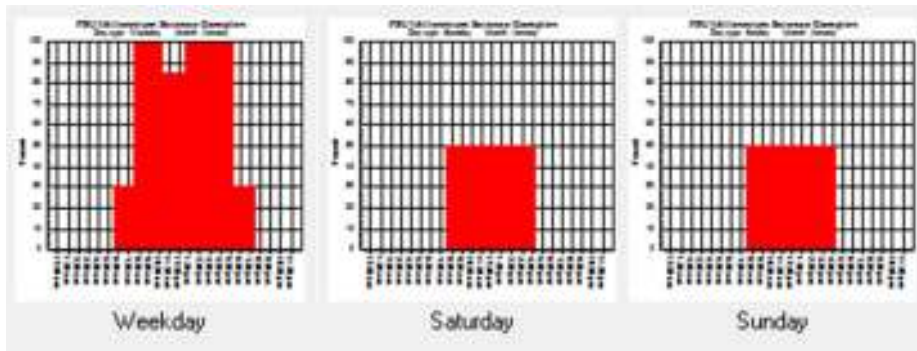


Figure 1: Millennium Science Complex Design Operation Schedules

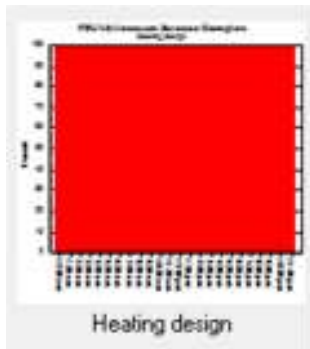


Figure 2: Millennium Science Complex Design Heating Schedule

BUILDING LOAD AND ENERGY MODELING

BASELINE ASHRAE 90.1 BUILDING MODEL

As explained in the executive summary, it was decided that only the 3rd floor would be the focus of detailed analysis. To provide a basis for future design considerations, the third floor was modeled in Trane Trace for a load and energy analysis. A model was created in accordance with ASHRAE 90.1 Baseline Standards, to provide the minimum energy efficiency requirements, using a space by space method. Adjustments to ASHRAE 90.1 were made to better fit the function of the Millennium Complex. Future models will be created to compare existing energy efficiencies and possible future savings.

Baseline Conditions –

- Ventilation Rates –ASHRAE Standard 62.1 Table 6-1 for Space by Space analysis
- Occupant Densities –ASHRAE Standard 62.1 Table 6-1 for Space by Space analysis. Offices adjusted for actual number of occupants.
 - Added an 80% diversity factor to account to fluctuations in occupancy.
 - A customized occupant and load schedule was created to simulate a university laboratory facility
- Lighting Power Densities –ASHRAE Standard 90.1 Table 9.6.1 for Space by Space analysis.
 - Added 10% diversity factor for lighting loads.
- Equipment Loads – Programmed values from Revit MEP 2011 Space Types for Space by Space analysis
- Laboratory Air Changes – Modeled with a design condition of 6 Air Changes Per Hour, based on general exhaust requirements
- Building Envelope – Modeled to minimum requirements according to Table 5.5-5 for Climate Zone 5A
- HVAC System and Type - Based on Table G3.1.1A – A non-residential building of greater than 150,000 sq. ft. using purchased heat will be modeled as System 7 – VAV with Reheat
 - Laboratories and Offices will be zoned separately
 - Laboratories will be served with 100% Dedicated Outdoor Air System with an outdoor air preconditioning energy recovery system
 - Offices will be supplied by a Variable Air Volume with Reheat System with 15% Outdoor Air
- System Type - Based on Table G3.1.1B – A System 7 will be modeled as a Packaged Rooftop VAV with Re-heat, with cooling supplied by chilled water and heating supplied by a hot water fossil fuel boiler
 - Heating will be supplied by campus purchased steam
 - Cooling will be supplied by campus chilled water
- Weather Data - 99.6% design days, 1% dry-bulb, 1% wet-bulb cooling temperatures must be used
- Outdoor Ventilation Rates - Must be the same for proposed and baseline building designs
- Economizers – A System 7 requires the use outdoor air economizers, with a high limit shut off at 70°F
- Energy Recovery – Fan systems above 5000 cfm with 70% or greater minimum outside air requirements shall have an energy recovery system with at least 50% recovery effectiveness
- Boilers – For System 7, boilers shall be natural draft and use same fuel as proposed building
 - Hot Water Temperature – Modeled with 180 degree HWS, and 130 degree HWR
 - Hot Water Reset – Based on Outside Air Dry-Bulb Temperature, 180 degree at 20 degrees and below, and 150 degree at 50 degrees and above, ramped linearly
 - Hot Water Pumps – Only primary is required to be modeled. Will have Variable Frequency Drive

- Chilled Water – For System 7
 - Chilled Water Temperature - Modeled with 44 degree CHWS, and 56 degree CHWR
 - Chilled Water Reset – Based on Outside Air Dry-Bulb Temperature, 44 degree at 80 degrees and above, 54 degree at 60 degrees and below, ramped linearly
 - Chilled Water Pumps – Shall model primary and secondary with Variable Frequency Drive
- Supply Air – Temperature will be reset based on zone demand with a temperature difference of 10 degrees under minimum loading
- VAV System – System 7 re-heat boxes will have a minimum flow of .4 cfm/ sq. ft. of floor area served

Table 6: Baseline ASHRAE 90.1 Building Façade U-Value Conductivities

| | U-Value (BTU/hr-ft ² -F) |
|--------|--|
| Roof | 0.048 |
| Wall | 0.064 |
| Window | 0.045 |
| Slab | 0.038 |

EXISTING DESIGN MODEL

An existing design model was created in Trane TRACE to compare the performance of the building to ASHRAE Standard 90.1. The goal of creating this model was to analyze the effectiveness of the existing design in TRACE and compare the results to the 14% energy savings outlined in the LEED credit report. The existing design model will also serve as a basis for future comparisons. As previously mentioned, the analysis only pertains to the 3rd floor of the Millennium Science Complex, so the comparison to the specified 14% energy savings cannot be considered highly accurate, but rather a preliminary estimation of savings.

A few key factors were improved upon in the existing design model which resulted in energy savings. A total enthalpy wheel was added to the lab AHUs. The ASHRAE Standard 90.1 model only utilized a coil loop to pre-condition outdoor air. The total enthalpy wheel, while increasing the overall system first cost, has been a proven method in reducing energy costs associated with 100% outdoor air systems. The fan types were also changed to model the variable frequency drives (VFDs) as outlined in the design documents. Variable frequency drives are another proven energy saving technology. The VFDs allow the AHUs to match the varying loads in the building instead of operating at full load constantly and in turn save energy. Finally, the enclosure was more accurately modeled and performed better than the baseline characteristics outlined by ASHRAE Standard 90.1.

As a result of the modifications to the ASHRAE Standard 90.1 model, the existing design showcased a total of 23% in annual energy cost savings. Errors in modeling can be attributed to the higher than expected savings percentage and will be investigated during later stages of this project.

More detailed breakdowns of the energy analysis can be found in Appendix C

Table 7: Existing Design Building Façade U-Value Conductivities

| | U-Value (BTU/hr-ft ² -F) |
|--------|--|
| Roof | 0.157 |
| Wall | 0.040 |
| Window | 0.293 |
| Slab | 0.124 |

BUILDING LOAD SUMMARY

The Millennium Science Complex's building loads were simulated in Trane Trace. The following data shows the breakdown of the office and laboratory air handlers. In both cases, there is a significant reduction in peak loads and supply airflows. To check for accuracy, the loads were compared to a common rule of thumb of 1 cfm/ft². The office zone is nearly identical and the more energy intensive laboratory is within acceptable limits.

Table 8: Office Zone Load Summary

| | Cooling (tons) | Heating (MBTUh) | Supply Airflow (cfm) | Outside Air Percentage | cfm/ft ² |
|-----------------|----------------|-----------------|----------------------|------------------------|---------------------|
| Baseline 90.1 | 113.3 | 779.6 | 39,814 | 16.3 | 1.39 |
| Existing Design | 97.2 | 513.9 | 28,974 | 22.5 | 1.01 |

Table 9: Laboratory Zone Load Summary

| | Cooling (tons) | Heating (MBTUh) | Supply Airflow (cfm) | Outside Air Percentage | cfm/ft ² |
|-----------------|----------------|-----------------|----------------------|------------------------|---------------------|
| Baseline 90.1 | 295.8 | 3,151.4 | 34,078 | 100.0 | 2.19 |
| Existing Design | 217.7 | 2,409.2 | 25,588 | 100.0 | 1.64 |

UTILITY DATA

Utility Data was adapted from Penn State Office of Physical Plant (OPP) information available on their website. OPP's avoided costs information was input into our model and the following table summarizes the utilities used within the energy model and their respective rates

Table 10: Utility Information

| Name of Utility | Cost (\$)/Unit |
|------------------------------|----------------------------|
| Purchased Steam | 9.85/1000 lbm (0.82/therm) |
| Purchased Chilled Water | 0.22/ton-hr (1.83/therm) |
| Electric Consumption | 0.07517/kWh |
| Electric On Peak | 1.09/kW |
| Water (N/A in current model) | 3.32/1000 gallons |

EQUIPMENT ENERGY CONSUMPTION BREAKDOWN

The cooling system and its necessary equipment within the Millennium Science Complex account for more energy than any other category, as shown in Figures 3 and 4. In comparison to the ASHRAE 90.1 model, the cooling equipment still is the highest consumer of energy despite experiencing a 44% in chilled water energy reduction for the existing design, see Figure 4.

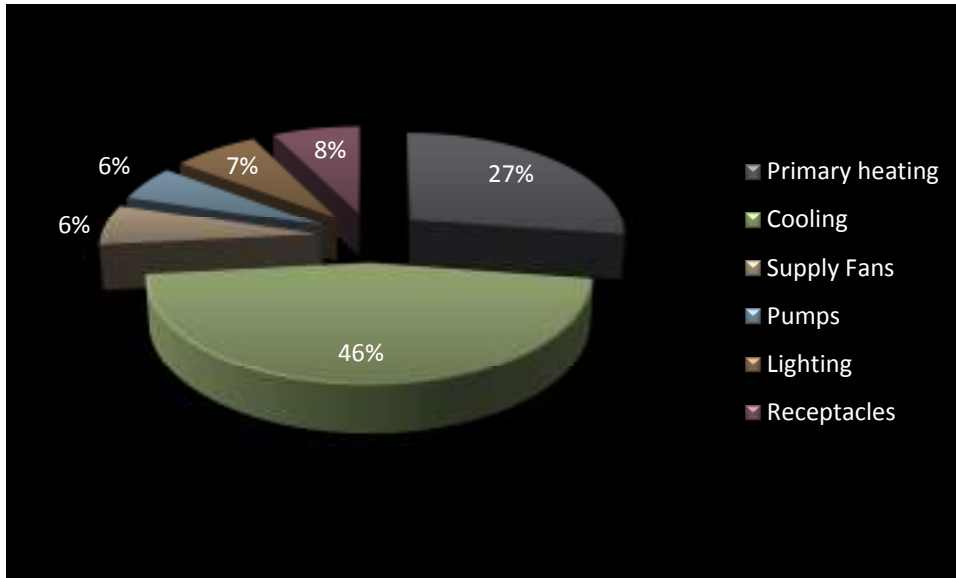


Figure 3: Equipment Energy Consumption: ASHRAE 90.1

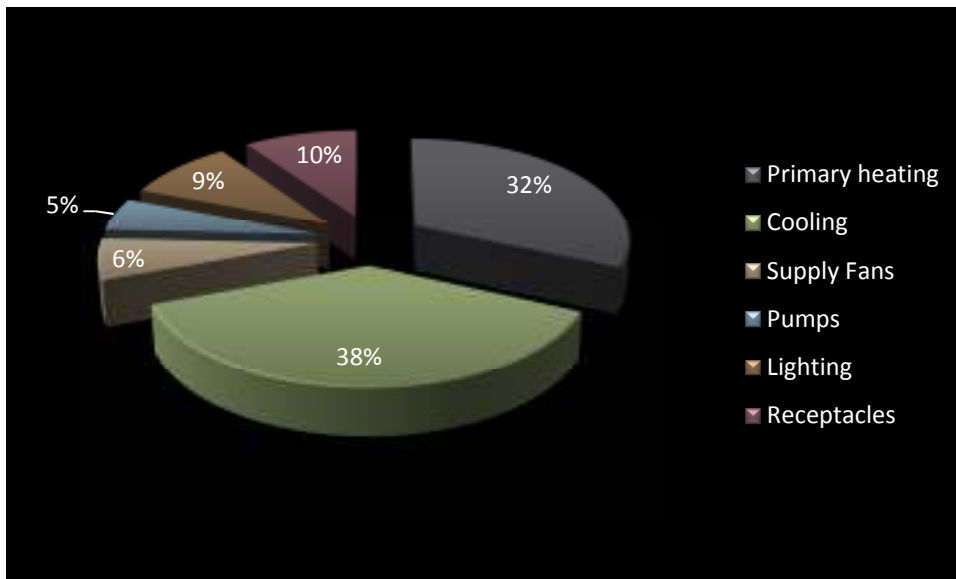


Figure 4: Equipment Energy Consumption: Existing Design

ANNUAL ENERGY CONSUMPTION & OPERATING COST ESTIMATE

The total annual cost estimated to operate the 3rd floor of the Millennium Science Complex came to \$123,745 in the Existing Design model. This represents roughly 23% energy savings in comparison to the ASHRAE Standard 90.1 baseline model. The summer months, particularly July, represent the most costly months of the year due to the increase demand for chilled water for cooling the building. Process steam is still required during the summer months due to the process loads specific to the building.

Table 11: Summarized Annual Results

| | ASHRAE 90.1 | Existing Design | Percent Savings | Cost Savings |
|----------------------------------|------------------|------------------|-----------------|-----------------|
| Electricity (kWh) | 765,979 | 684,280 | 11% | \$6,141 |
| Purchased Chilled Water (therms) | 45,039 | 28,705 | 44% | \$29,891 |
| Purchased Steam (therms) | 26,694 | 24,119 | 9% | \$2,111 |
| Total Costs and Savings | \$161,889 | \$123,745 | 23% | \$38,144 |

Table 12: Comparison of Baseline and Existing Design Energy Intensities

| | Baseline ASHRAE 90.1 | Existing Design |
|---|----------------------|-----------------|
| Energy Intensity (kBTU/ft ² -yr) | 221.2 | 172.2 |
| Cost | \$3.72/SF | \$2.85/SF |

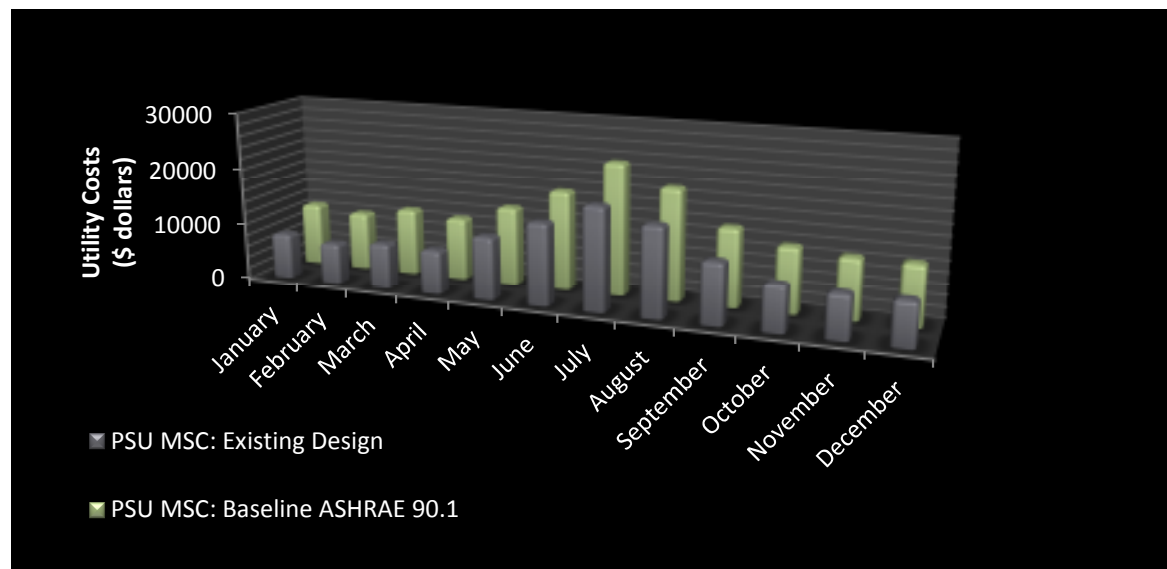


Figure 5: Comparison of Baseline and Existing Design Monthly Utility Costs

Table 13: Baseline ASHRAE 90.1 & Existing Model Monthly Energy Consumption & Costs

| | Electricity (kWh) | | Purchased Steam (therms) | | Purchased Chilled Water (therms) | |
|-------------|-------------------|---------|--------------------------|---------|----------------------------------|----------|
| | 90.1 | Design | 90.1 | Design | 90.1 | Design |
| Jan. Energy | 62,633 | 53,682 | 3,856 | 3,720 | 1,629 | 351 |
| Jan. Cost | \$4,708 | \$4,035 | \$3,162 | \$3,051 | \$2,981 | \$642 |
| Feb. Energy | 56,759 | 48,539 | 3,624 | 3,487 | 1,463 | 288 |
| Feb. Cost | \$4,267 | \$3,649 | \$2,971 | \$2,859 | \$2,678 | \$526 |
| Mar. | 65,874 | 57,236 | 3,034 | 2,715 | 2,184 | 747 |
| Mar. Cost | \$4,952 | \$4,302 | \$2,488 | \$2,226 | \$3,996 | \$1,367 |
| Apr. Energy | 61,607 | 53,705 | 1,994 | 1,724 | 2,507 | 1,193 |
| Apr. Cost | \$4,631 | \$4,037 | \$1,635 | \$1,414 | \$4,588 | \$2,182 |
| May Energy | 66,840 | 60,696 | 959 | 869 | 4,187 | 3,060 |
| May Cost | \$5,024 | \$4,562 | \$786 | \$713 | \$7,663 | \$5,600 |
| Jun. Energy | 66,191 | 62,053 | 1,239 | 989 | 6,091 | 4,745 |
| Jun. Cost | \$4,976 | \$4,665 | \$1,016 | \$811 | \$11,146 | \$8,682 |
| Jul. Energy | 65,824 | 62,375 | 1,602 | 1,280 | 9,260 | 7,271 |
| Jul. Cost | \$4,948 | \$4,689 | \$1,318 | \$1,050 | \$16,946 | \$13,305 |
| Aug. Energy | 68,852 | 64,321 | 1,442 | 1,164 | 6,961 | 5,358 |
| Aug. Cost | \$5,176 | \$4,835 | \$1,182 | \$954 | \$12,739 | \$9,805 |
| Sep. Energy | 63,380 | 56,988 | 973 | 860 | 4,378 | 3,135 |
| Sep. Cost | \$4,764 | \$4,284 | \$798 | \$705 | \$8,012 | \$5,738 |
| Oct. Energy | 64,895 | 57,109 | 1,870 | 1,660 | 2,610 | 1,313 |
| Oct. Cost | \$4,878 | \$4,293 | \$1,534 | \$1,362 | \$4,777 | \$2,403 |
| Nov. Energy | 61,832 | 54,547 | 2,451 | 2,203 | 2,122 | 846 |
| Nov. Cost | \$4,648 | \$4,100 | \$2,010 | \$1,806 | \$3,884 | \$1,549 |
| Dec. Energy | 61,292 | 53,029 | 3,645 | 3,446 | 1,646 | 399 |
| Dec. Cost | \$4,607 | \$3,986 | \$2,989 | \$2,826 | \$3,013 | \$730 |

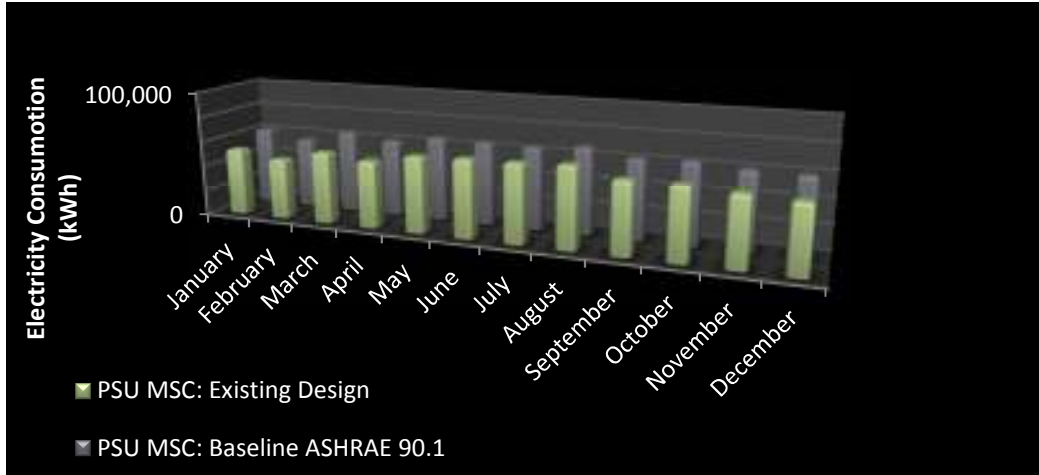


Figure 6: Comparison of Baseline and Existing Design Monthly Electricity Consumption

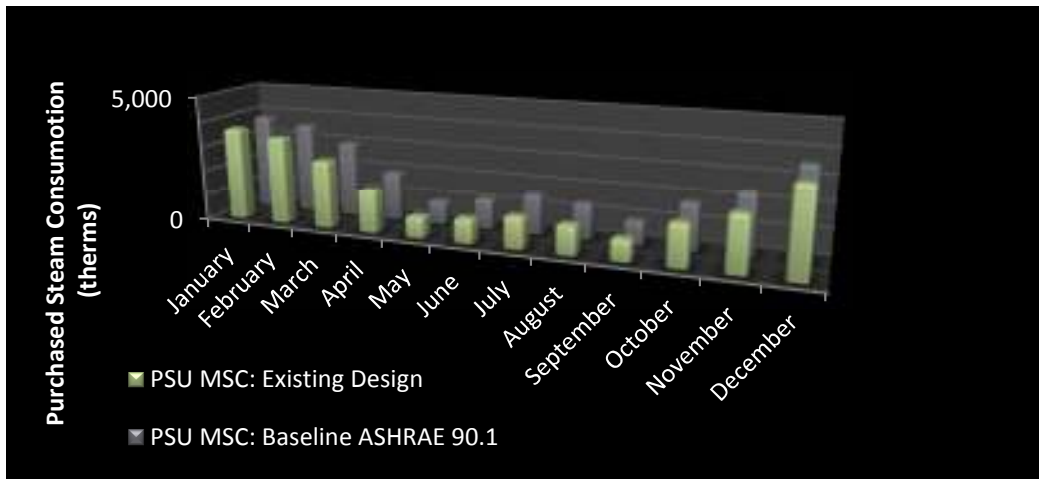


Figure 7: Comparison of Baseline and Existing Design Monthly Purchased Steam Consumption

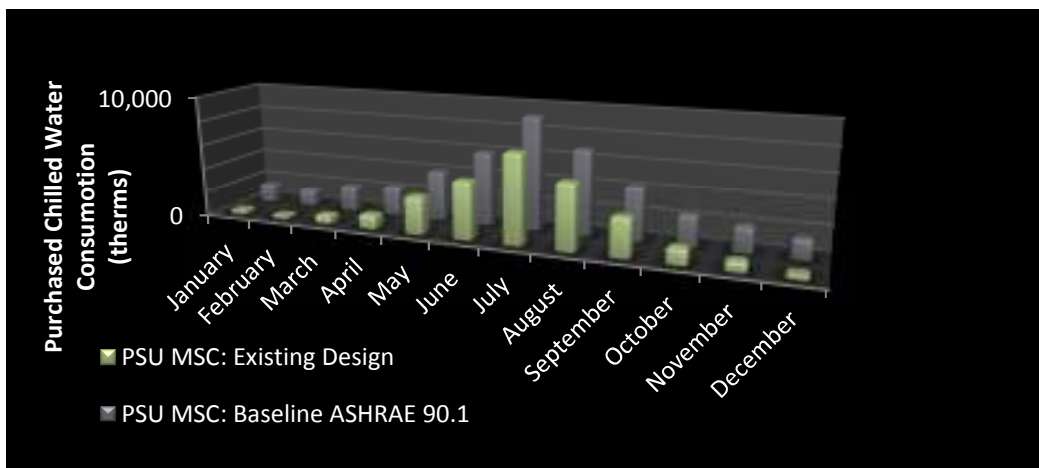


Figure 8: Comparison of Baseline and Existing Design Monthly Purchased Chilled Water Consumption

BUILDING EMISSIONS FOOTPRINT

The building emissions footprint of Penn State’s Millennium Science Complex was analyzed using the total source energy consumption data calculated from Trane TRACE. The third floor was only modeled in TRACE due to time constraints. The third floor comprises roughly 45,000 SF of the 276,000 SF in the building. A comparison was done between the ASHRAE 90.1 Standard and the existing building conditions.

Table 14: Comparison of emission rates from Trane TRACE

| | ASHRAE 90.1 Standard Emissions | Existing Design |
|---|--------------------------------|-----------------|
| Total Building Energy (Btu/ft ² -yr) | 221,194 | 172,158 |
| Total Source Energy (Btu/ft ² -yr) | 335,995 | 280,932 |
| CO ₂ (lbm/yr) | 3,487,813 | 2,714,609 |
| SO ₂ (gm/yr) | 26,966 | 20,988 |
| NO _x (gm/yr) | 5,420 | 4,219 |

In comparison, an emissions analysis was performed using data obtained from National Renewable Energy Laboratory’s technical report titled, “Source Energy and Emission Factors for Energy Use in Buildings.” Factors for the amount of pollutant produced were taken from the Eastern United States data. The multiplier for the source energy factors is 2.528, assuming the use of fossil fuel energy. It is important to remember that Penn State purchases green power to offset emissions however that was not factored into these calculations.

Table 15: Comparison of emission rates from NREL

| Pollutant | Lb produced per kWh delivered | 90.1 Model Emissions (lbs) | Existing Design Model Emissions (lbs) |
|------------------|-------------------------------|----------------------------|---------------------------------------|
| CO _{2e} | 1.74 | 3,369,327 | 3,009,956 |
| CO ₂ | 1.64 | 3,175,688 | 2,836,970 |
| Solid Waste | 0.0205 | 39,696 | 35,462 |
| SO _x | 0.000857 | 1,659.5 | 1,482.5 |
| NO _x | 0.000300 | 580.9 | 519.0 |
| CH ₄ | 0.000359 | 695.2 | 621.0 |
| CO | 0.0000854 | 165.4 | 147.7 |
| TNMOC | 0.00000726 | 14.1 | 12.6 |
| N ₂ O | 0.00000387 | 7.5 | 6.7 |
| PM10 | 0.00000926 | 17.9 | 16.0 |
| Lead | 0.0000000139 | 0.0269 | 0.0240 |
| Mercury | 0.00000000336 | 0.0065 | 0.0058 |

MECHANICAL SYSTEM EXISTING CONDITIONS OVERVIEW

SYSTEM OPERATION OVERVIEW

AIR SIDE

As shown in Figure 9, the airside system for The Millennium Science Complex utilizes a VAV system where each terminal unit is supplied with air from AHUs located in the mechanical penthouse. The air is supplied to the spaces through ceiling mounted low velocity radial diffusers to maintain room temperature setpoint. The air return is also through the ceiling plenum to the return air duct riser. CO₂ sensors are located in both the return air and outside air ducts on each floor to maintain the concentration level of 470 ppm of CO₂.

For the non-lab spaces the supply air is provide by three VAV AHUs, with 33,000 cfm capacity each. The VAV boxes are controlled by wall mounted temperature sensors to maintain a fixed temperature of 75°F. The north perimeter offices are serviced with hot water coils, which are the main heating source, for the VAV boxes. In decreasing loads, the static pressure sensor in the longest duct run controls the variable frequency drive for the supply fans. The non-laboratory AHUs utilize outdoor air economizer to save energy since they are not a dedicated outdoor air system. During the economizer mode, the return fan is capable of returning total air capacity and releases to the louvered penthouse. This is due to the supply fans interlocked to the return fans.

The animal care facility (vivarium) is serviced by two 25,000 cfm AHUs with 95% efficient air filters. The AHUs are 100% dedicated outdoor air systems that provide variable air volume to the spaces. To ensure operating capacity for the animal holding rooms and animal care facility, the AHUs were sized for 100% of maximum block airflow demand and are connected to standby power. The supply and exhaust air volumes are controlled by airflow control valves via the Laboratory Airflow Control System. General exhaust is removed through the ceiling inlet located over the bio-safety cabinet. The facility is exhausted with a dedicated exhaust system to two fans located on the roof. The exhaust system consists of manifold fume hood exhausts and the general room exhaust. Figure 9 shows a simplified exhaust riser diagram for the Millennium Science Complex.

The clean room is serviced by one dedicated AHU that is a 100% outdoor air system. It is designed to lower the humidity levels to 45% RH, which is required for pressurization and makeup air. The building's main supply air duct is routed to the clean room and capped for future fitout. In order to maintain proper indoor air quality, the clean room has a separate toxic exhaust fan and the main toxic exhaust system is routed to the clean room area and capped for future fitout. General exhaust from the room is routed to the main building general lab exhaust system.

Five 50,000 cfm 100% outdoor air AHUs provide supply air to the laboratories located in the Millennium Science Complex. The AHUs provide 100% of system capacity and are connected to standby power. In case of power loss, only one AHU will operate. To utilize energy, each unit includes an enthalpy heat recovery wheel and integral exhaust fan to operate concurrently with the supply. Energy is transferred from the lab general exhaust system and not the fume hood exhaust to ensure proper indoor air quality so that the incoming outdoor air does not get contaminated. Exhaust air is removed from the spaces with fume hoods, process point exhausts, and general exhaust registers. The fume hood and vivarium exhaust fans are equipped with run around energy recovery coils that circulate glycol with two pumps to the preheat coils in the AHF AHUs, clean room AHU, and quiet lab AHU. The supply and exhaust airflow are controlled by the Laboratory Airflow Control System. Phoenix venture valves are used to ensure proper ventilation and pressurization since the supply air valve is interlocked to the room general exhaust and fume hood exhaust.

WATER SIDE

CHILLED WATER:

The Millennium Science Complex chilled water is serviced from the PSU campus central plant. Chilled water is pumped into the northeast corner of the building into the ground level mechanical room. Four variable speed horizontal split case chilled water pumps in a manifold configuration, where one is used as a standby, pump the chilled water to the AHUs located in the mechanical penthouse on the fourth floor. Figure 10 shows a simplified diagram illustrating the chilled water layout. The chilled water is pumped to the penthouse and is circulated throughout the floors to the VAV boxes to service the cooling coils. A chilled water control valve modulates under varying load in the VAV to maintain a fixed coil discharge temperature for each zone. To maintain minimum flow throughout the system during very low flow conditions, each cooling coil has two way valves and a main differential pressure bypass. For partial load conditions, one low flow pump is provided in order to save energy. In case the pump fails a pump bypass line is provided with an automatic control valve to ensure system reliability.

The chilled water is pumped to two plate and frame heat exchangers before it reaches the mechanical penthouse, as shown in Figure 10, to service the secondary condenser water cooling. This is dedicated for process cooling of equipment and supplemental loads in the building to serve cold rooms and environmental rooms. The process cooling system flows past an expansion tank and through two variable speed drive circulation pumps in the basement mechanical room. Both the heat exchangers and circulation pumps were designed for redundancy to provide 100% backup. The pumps are connected to standby power to ensure flow upon power failure. The chilled water is also connected to standby power to provide cooling for the animal care facility (vivarium) AHU and one main lab penthouse AHU. Chilled water is to be redirected to these two AHUs from the cooling coil loop control valves upon power failure.

HOT WATER:

High pressure steam at 140 psig is the building's heating source and is supplied from the PSU campus boiler plant. The steam enters the northeast corner of the building into the ground mechanical room and flows to the pressure reducing station. At the PRV station, the high pressure steam is reduced to medium pressure at 60 psig with one pressure reducing valve, as shown in Figure 11. The medium pressure steam is used for equipment throughout the building, such as laboratory sterilization and domestic hot water heat exchangers. From the PRV station the MPS flows through three hot water heaters and then to three clean steam generators in the mechanical penthouse. The medium pressure condensate is collect then returns to a pump in the basement. Clean steam from the steam generators is fed to each laboratory AHU to provide the required lab humidity with clean filtered water. Medium pressure process steam at 85 psig is supplied to the vivarium and laboratories to serve glass washers, cage washers, sterilizers, and autoclaves.

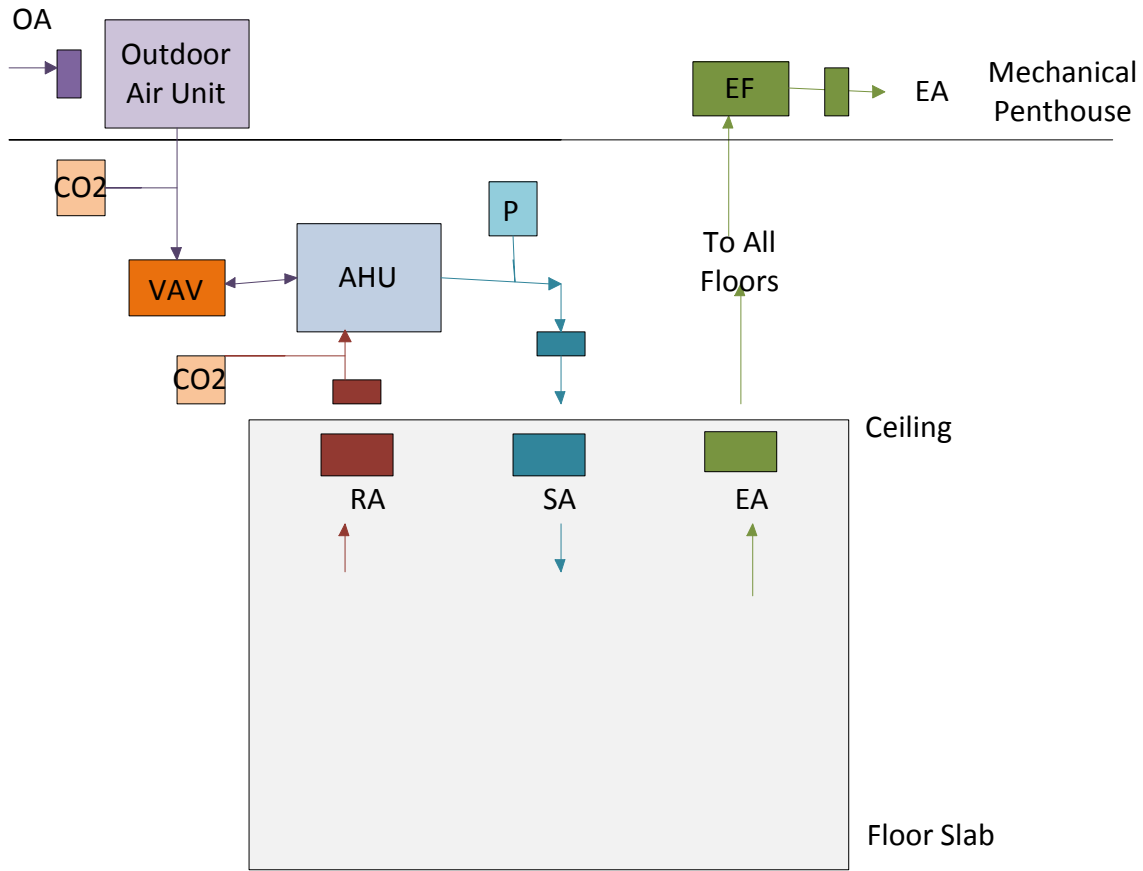
At the PRV station, the high pressure steam is also reduced from 140 psig to 15 psig using two pressure reducing valves for low pressure steam. Low pressure steam is used for most of the mechanical equipment in the building such as: reheat and preheat coils at the AHUs, humidification and plate and frame hot water heat exchangers for perimeter heating elements, and terminal device reheat coils. From the PRV station, as shown in Figure 11, LPS flows to two redundant plate and frame steam to hot water heat exchangers to serve the lab and office reheat coils at air terminal devices. Two pumps placed in parallel circulate the hot water to the reheat coils. Two plate and frame steam to hot water heat exchangers with two inline pumps also serve the variable flow

perimeter finned tube elements in areas where the glass height is greater than 11 feet high, such as office spaces, conference rooms, and laboratories.

Localized compressed air powered condensate pumps pump the steam condensate from the mechanical penthouse back to the ground level mechanical room. The condensate is then pumped back to the main campus boiler plant.

EXISTING SYSTEMS SCHEMATIC DRAWINGS

Figure 9: Typical Airside Diagram for Spaces



| Legend | |
|-------------------|-------------------------|
| RA: | Return Air |
| SA: | Supply Air |
| EA: | Exhaust Air |
| OA: | Outside Air |
| CO ₂ : | Carbon Dioxide Sensor |
| VAV: | Variable Air Volume Box |
| EF: | Exhaust Fan |
| P: | Static Pressure Sensor |

Figure 10: Chilled Water Flow Diagram

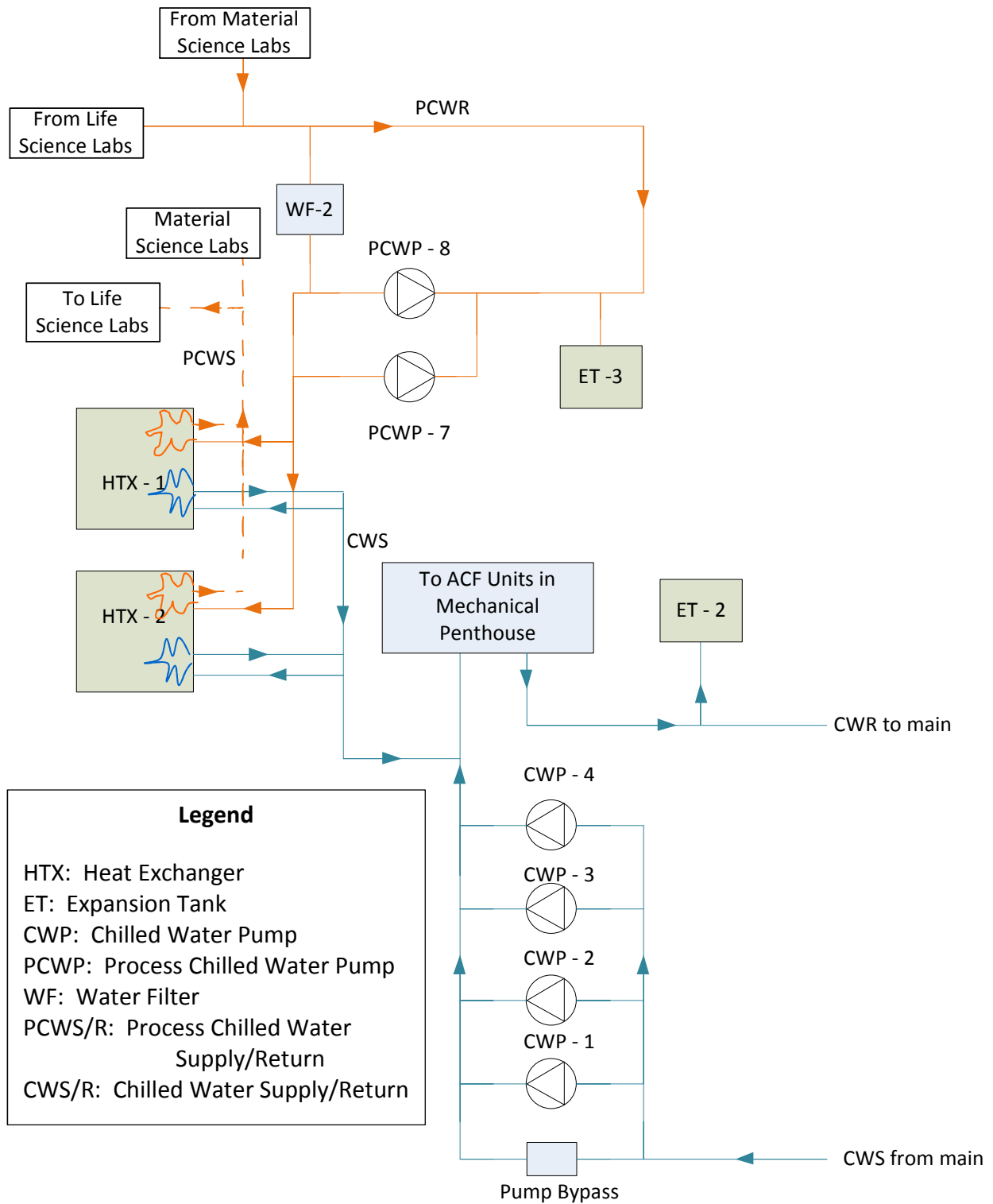
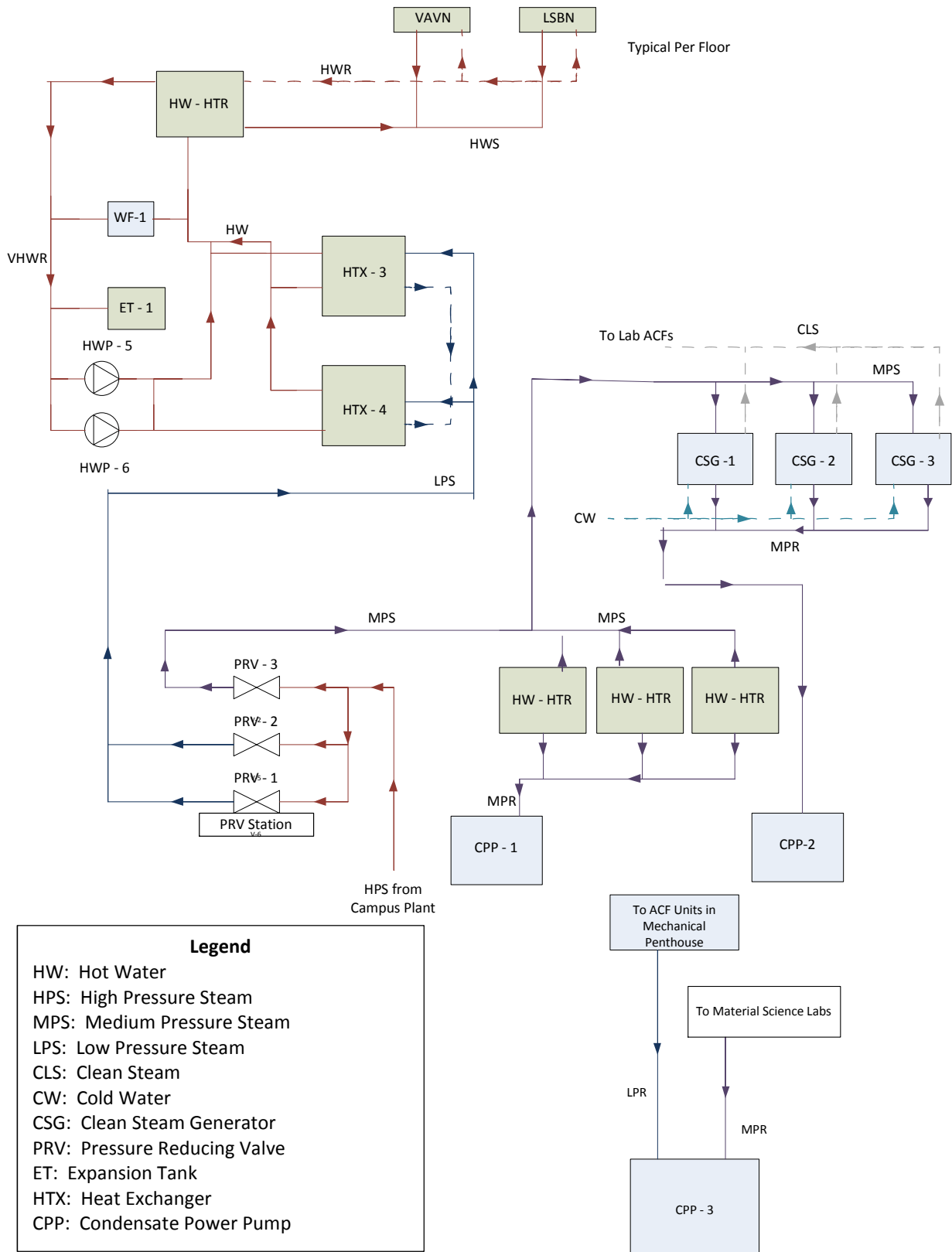


Figure 11: Hot Water Flow Diagram



SUMMARIZATION OF MAJOR MECHANICAL EQUIPMENT

Table 16: Major Mechanical Equipment-Pumps

| Designation | Service | Location | Flow Rate (gpm) | Total Pump Head (ft) | RPM | Pump Type |
|------------------|--|----------------------|-----------------|----------------------|------|------------------|
| CWP-1 | Chilled Water | Basement Mezzanine | 2780 | 150 | 1800 | Horizontal Split |
| CWP-2 | Chilled Water | Basement Mezzanine | 2780 | 150 | 1800 | Horizontal Split |
| CWP-3 (standby) | Chilled Water | Basement Mezzanine | 2780 | 150 | 1800 | Horizontal Split |
| CWP-4 (low flow) | Chilled Water | Basement Mezzanine | 800 | 60 | 1800 | Horizontal Split |
| HWP-5 | Hot Water Heating | First Floor | 930 | 100 | 1800 | Vertical In-line |
| HWP-6 | Process Cooling Water | First Floor | 930 | 100 | 1800 | Vertical In-line |
| PCWP-7 | Process Cooling Water | First Floor | 600 | 100 | 1800 | Vertical In-line |
| PCWP-8 (standby) | Radiant Cooling Water-Quiet Labs | First Floor | 600 | 100 | 1800 | Vertical In-line |
| CWP-9 | Radiant Cooling Water-Quiet Labs | Basement | 75 | 25 | 1800 | Vertical In-line |
| CWP-10 (standby) | Radiant Cooling Water-Quiet Labs | Basement | 75 | 25 | 1800 | Vertical In-line |
| GWP-11 | Glycol Heating/Cooling Run-Around Coil | Mechanical Penthouse | 775 | 75 | 1800 | Vertical In-line |
| GWP-12 | Glycol Heating/Cooling Run-Around Coil | Mechanical Penthouse | 775 | 75 | 1800 | Vertical In-line |
| GWP-13 | Snow Melt System | First Floor | 25 | 85 | 3500 | End Suction |

Table 17: Major Mechanical Equipment- AHUs

| Designation | Service | Location | Capacity (cfm) | OA Capacity (cfm) | Heat Recovery Wheel | Notes |
|-------------|----------------|----------------------|----------------|-------------------|---------------------|---------------------|
| ACF-1 | Lab | Mechanical Penthouse | 50,000 | 50,000 | Y | - |
| ACF-2 | Lab | Mechanical Penthouse | 50,000 | 50,000 | Y | - |
| ACF-3 | Lab | Mechanical Penthouse | 50,000 | 50,000 | Y | - |
| ACF-4 | Lab | Mechanical Penthouse | 50,000 | 50,000 | Y | - |
| ACF-5 | Lab | Mechanical Penthouse | 50,000 | 50,000 | Y | - |
| ACF-6 | Offices | Mechanical Penthouse | 33,000 | 4,950 | N | - |
| ACF-7 | Offices | Mechanical Penthouse | 33,000 | 4,950 | N | - |
| ACF-8 | Offices | Mechanical Penthouse | 33,000 | 4,950 | N | - |
| ACF-9 | Animal Holding | Mechanical Penthouse | 25,000 | 25,000 | Y | - |
| ACF-10 | Animal Holding | Mechanical Penthouse | 25,000 | 25,000 | Y | - |
| ACF-11 | Quiet Labs | Mechanical Penthouse | 13,000 | 13,000 | Y | - |
| ACF-12 | Clean Room | Mechanical Penthouse | 51,000 | 51,000 | Y | - |
| CRAC-1 | LS/MS Server | Mechanical Room | 14,600 | - | N | 40% Ethylene Glycol |
| ACU-1 | MDF/IDF | Basement | 1,250 | - | N | Supplemental |
| ACU-2,3 | LS DATA | Basement | 3,750 | - | N | Supplemental |
| ACU-4 | TELECOM | First Floor | 1,250 | - | N | Supplemental |
| ACU-5 | TELECOM | First Floor | 1,250 | - | N | Supplemental |
| ACU-8 | TELECOM | Second Floor | 1,250 | - | N | Supplemental |
| ACU-9,10 | IDF | Second Floor | 3,750 | - | N | Supplemental |
| ACU-11 | LS DATE | Second Floor | 1,250 | - | N | Supplemental |
| ACU-12 | TELECOM | Second Floor | 1,250 | - | N | Supplemental |
| ACU-13 | TELECOM | Second Floor | 1,250 | - | N | Supplemental |
| ACU-14 | IDF ROOM | Third Floor | 1,250 | - | N | Supplemental |
| ACU-15 | TELECOM | Third Floor | 1,250 | - | N | Supplemental |
| ACU-16 | ELEV MACHINE | Mechanical Penthouse | 2,500 | - | N | Supplemental |
| ACU-17 | ELEV MACHINE | Mechanical Penthouse | 2,500 | - | N | Supplemental |
| ACU-18 | BIOPHOTONICS | Second Floor | 2,500 | - | N | Supplemental |
| ACU-19 | BOIPHOTONICS | Second Floor | 2,500 | - | N | Supplemental |
| ACU-20 | BIOPHOTONICS | Second Floor | 2,500 | - | N | Supplemental |

Table 18: Major Mechanical Equipment- Fan Coil Units

| Designation | Service | Location | Air Quantity (cfm) | Total Cooling Capacity (MBH) | Heating Capacity (MBH) |
|----------------|--------------------|--------------------|--------------------|------------------------------|------------------------|
| FCUNQ012_1,2,3 | Tunnel Corridor | Basement | 600 | 12.9 | 21.8 |
| FCUN160_1,2 | Equipment Corridor | First Floor | 600 | 12.9 | - |
| FCUN270_1,2,3 | Equipment Corridor | Second Floor | 600 | 12.9 | - |
| FCUN361_1,2 | Equipment Corridor | Third Floor | 600 | 12.9 | - |
| FCUNP053 | Electrical | Basement Mezzanine | 1400 | 48.9 | - |

Table 19: Major Mechanical Equipment--Air to Air Heat Recovery Units

| Designation | Service | Location | Air Quantity (cfm) | Wheel Size (in) | Motor rpm |
|-------------|---------|----------------------|--------------------|-----------------|-----------|
| HRW-1 | ACF-1 | Mechanical Penthouse | 50,000 | 154 x 154 | 1800 |
| HRW-2 | ACF-2 | Mechanical Penthouse | 50,000 | 154 x 154 | 1800 |
| HRW-3 | ACF-3 | Mechanical Penthouse | 50,000 | 154 x 154 | 1800 |
| HRW-4 | ACF-4 | Mechanical Penthouse | 50,000 | 154 x 154 | 1800 |
| HRW-5 | ACF-5 | Mechanical Penthouse | 50,000 | 154 x 154 | 1800 |

Table 20: Major Mechanical Equipment-Plate and Frame Heat Exchangers

| Designation | Service | Location | Type | Flow Rate (GPM) |
|-------------|----------------------------------|------------------|----------------|-----------------|
| HTX-1 | Process Cooling Water | First Floor Mer. | Water to Water | 897.7 |
| HTX-2 | Process Cooling Water | First Floor Mer. | Water to Water | 897.7 |
| HTX-3 | Hot Water Heating | First Floor Mer. | Steam to Water | 930 |
| HTX-4 | Hot Water Heating | First Floor Mer. | Steam to Water | 930 |
| HTX-5 | Radiant Cooling Water Quiet Labs | Basement | Water to Water | 75 |
| HTX-6 | Radiant Cooling Water Quiet Labs | Basement | Water to Water | 75 |
| HTX-7 | Snow Melt System | First Floor Mer | Water to Water | 25 |

Table 21: Major Mechanical Equipment-Clean Steam Generators

| Designation | Service | Location | Clean Steam Capacity (lb/hr) | Steam Pressure (psig) |
|-------------|------------|-----------|------------------------------|-----------------------|
| CSG-1 | Laboratory | Penthouse | 4,000 | 15 |
| CSG-2 | Laboratory | Penthouse | 4,000 | 15 |
| CSG-3 | Laboratory | Penthouse | 4,000 | 15 |

LOST USABLE SPACE

The mechanical system equipment and components encompass a large amount of the physical space within the building. Not only is floor area lost due to shaft rising through each floor and mechanical equipment rooms, but the building’s floor to floor height needed to be increased in order to snugly fit all of the mechanical equipment underneath the structure and above the finished ceiling. A breakdown of the lost floor area and lost volume of the building is provided below.

Table 22: Lost Usable Area Breakdown

| Floor | Lost Usable Area |
|---|------------------|
| Basement | 9,050 SF |
| 1 st Floor | 4,150 SF |
| 2 nd Floor | 1,175 SF |
| 3 ^d Floor | 1,014 SF |
| 4 th Floor: Mechanical Penthouse | 27,287 SF |
| Total Area Lost | 42,676 SF |

The overall building encompasses a total of 275,600 SF. Therefore, the area covered by mechanical systems for the building corresponds to 15.5% of the total usable area within the building.

The Millennium Science Complex has an average floor to floor height of 19 feet. An average of 9 feet is left for both structure and mechanical systems. An average estimate of 7 feet of plenum space can be used to calculate the volume of the MEP & Telecom distribution in the area not dedicated to the mechanical systems, 232,924 SF. The MEP & Telecom distribution system consumes 31% of the building’s volume.

Table 23: Lost Usable Volume Breakdown

| | |
|---|--------------|
| Average Building Floor to Floor Height | 19 ft. |
| Average Mechanical Plenum Height | 7 ft. |
| Building Area(without shaft and MEP space) | 232,924 SF |
| Volume of Space from distribution systems | 1,630,468 CF |
| Volume of Building | 5,236,400 CF |
| Percentage of Building Volume dedicated to MEP & Telecom distribution | 31% |

EA CREDIT 1: OPTIMIZE ENERGY PERFORMANCE, 2 POINTS

A whole building energy simulation was completed using ASHRAE Standard 90.1-2004, Appendix G. The building design energy cost savings percentage is at least 14%. Two points are awarded for this level of energy optimization.

EA CREDIT 3: ENHANCED COMMISSIONING, 1 POINT

The design specifications call for the building to follow the necessary steps to qualify for this credit.

EA CREDIT 4: ENHANCED REFRIGERANT MANAGEMENT, 1 POINT

No Halon or HCFC based refrigerants were used in HVAC equipment.

EA CREDIT 5: MEASUREMENT AND VERIFICATION (UNDECIDED, 1 POINT)

The project may or may not achieve this credit. To achieve EA Credit 5, the Millennium Science Complex would have to instill a plan to continually monitor the energy consumption of the building to ensure the building continually performs efficiently

EA CREDIT 6: GREEN POWER, 1 POINT

Penn State committed to purchasing an annual supply of 83,600 megawatts of renewable energy in 2006 for the next 5 years. This is equivalent to 20% of what the university's annual supply. This energy is split between nationally based Low Impact Hydropower Institute's hydropower (39%), biomass (20%), wind energy (20%), and Pennsylvania based wind energy (21%).

INDOOR ENVIRONMENTAL QUALITY: 12 of 15 Credits

EQ PREREQUISITE 1: MINIMUM IAQ PERFORMANCE

EQ PREREQUISITE 2: ENVIRONMENTAL TOBACCO SMOKE CONTROL

Both prerequisites are required to be met.

EQ CREDIT 1: OUTDOOR AIR DELIVERY MONITORING, 1 POINT

CO₂ monitoring devices are located within air handling units and densely occupied conference rooms

EQ CREDIT 3.1: CONSTRUCTION IAQ MANAGEMENT PLAN, DURING OCCUPANCY, 1 POINT

EQ CREDIT 3.2: CONSTRUCTION IAQ MANAGEMENT PLAN, BEFORE OCCUPANCY, 1 POINT

During the construction of the building, an IAQ plan was laid out and followed. Before the building is occupied the systems will be ran to purge the spaces of any remaining construction related contaminants.

EQ CREDIT 4.1: LOW EMITTING MATERIALS, ADHESIVES & SEALANTS, 1 POINT

EQ CREDIT 4.2: LOW EMITTING MATERIALS, PAINTS & COATING, 1 POINT

EQ CREDIT 4.3: LOW EMITTING MATERIALS, CARPET SYSTEMS, 1 POINT

EQ CREDIT 4.4: LOW EMITTING MATERIALS, COMPOSITE WOOD & AGRIFIBER, 1 POINT

All materials that apply to the above credits meet tolerances for VOC content limits and other prescriptive requirements.

EQ CREDIT 5: INDOOR CHEMICAL & POLLUTANT SOURCE CONTROL, 1 POINT

Building entrances contain grilles that serve to collect dirt from occupants as they enter the building. Also, since the laboratory rooms have the likelihood of producing chemicals harmful to indoor air quality, each room is tied into an exhaust system that purges exhaust straight out of the building.

EQ CREDIT 6.1: CONTROLLABILITY OF SYSTEMS: LIGHTING, 1 POINT

Lighting controls are provided for at least 90% of the individual spaces in the building as well as controls for all multi-person spaces.

EQ CREDIT 7.2: THERMAL COMFORT, VERIFICATION, 1 POINT

The credit requires a survey of the new building's occupants thermal satisfaction from 6 to 18 months after occupancy to ensure that no more than 20% of occupants are thermally uncomfortable and remediation if 20% of occupants are dissatisfied.

EQ CREDIT 8.1: DAYLIGHT & VIEWS, DAYLIGHT 75% OF SPACES, 1 POINT

EQ CREDIT 8.2: DAYLIGHT & VIEWS, DAYLIGHT 90% OF SPACES, 1 POINT

The building is required to use natural daylight to produce the required illumination levels with 90% of the regularly occupied spaces. The use of natural daylight connects the occupant with the outdoors and has been linked with improvements in mood and productivity.

OVERALL EVALUATION

The mechanical systems in the Millennium Science Complex provide an intricate and reliable design to accommodate the diverse laboratories and general spaces for the Material and Life Sciences. Through the programs' pursuit to achieve LEED Gold Certification, numerous technologies and equipment were utilized to reduce the energy usage. Although the building's operating history does not exist currently, reasonable assumptions were made to estimate the energy performance of the building.

Enthalpy heat recovery wheels and runaround reheat coils that service the laboratories and animal control facilities have proven to be successful in other designs and offset the additional energy use associated with a 100% outdoor air system. Connecting into the campus steam and chilled water lines reduces the amount of space that would need to be devoted to large mechanical equipment such as chillers and boilers. VAV systems are proven to reduce energy usage and have been widely used throughout the building industry.

The Millennium Science Complex has been designed to a high standard in all aspects. It is likely that Penn State investigated many viable systems and selected the approach that best fit the university's current and future plans and overall growing emphasis on sustainable and responsible building. Future reports will investigate opportunities for improvement in energy usage and synergy with other design disciplines within the collaborative environment of the Integrated Project Delivery/ Building Information Modeling thesis teams.

INTEGRATED PROJECT DELIVERY/BUILDING INFORMATION MODELING

COORDINATION MODELING

All disciplines have received a set of basic BIM models from the design team, developed in Autodesk Revit 2011 platforms. While these are a useful start to coordinating design information between disciplines, they are not a complete set of construction documents. The mechanical model contains only the main risers and runs, not including the smaller branch ducting. It also does not include any of the dense gas pipework that are meant to supply the laboratory sectors. While these major items are missing, it may be due to a small cost-benefit relationship of this additional modeling. With such a large above ceiling plenum, it may not have been cost effective to model these extra details for the benefits of coordination.

In the picture below, it is easy to see the complexity of the building systems in the Millennium Science Complex. The tolerances and clearances between electrical (gray conduit), mechanical (blue ductwork), structural (red members), and architectural systems are very tight. Through accurate modeling, our research team hopes to better coordinate areas of congestion. The most congested areas within the third floor will be surrounding the four mechanical shafts. By coordinating these areas, coordination modeling will be able to produce the most significant benefits.

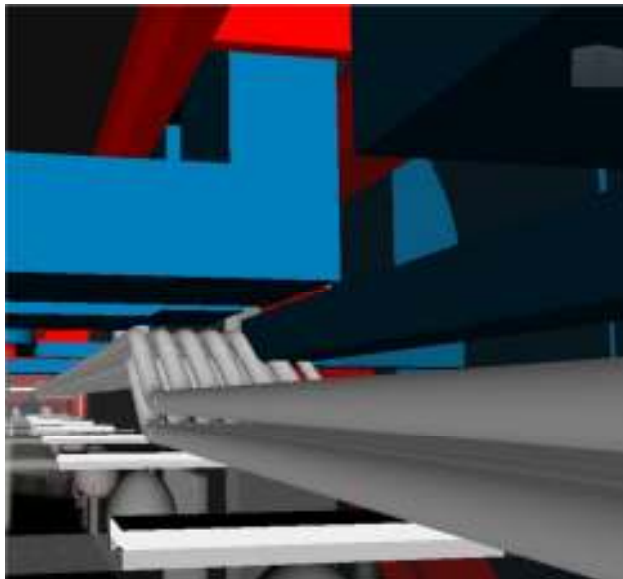


Figure 12: Screenshot from the Coordination Model of All Disciplines

EXISTING CLASH DETECTION

All discipline models have been brought together in Autodesk Navisworks Manage 2011 for a collision coordination model. While there are a few instances of interdisciplinary collisions, as seen below, the models in general have been coordinated very well. They do not, however, accurately represent the actual ceiling conditions, as many things are not modeled. Mechanically, there is very little branch ductwork and no diffusers modeled. Electrically there is no branch conduit modeled. While in most cases these aspects might not cause serious collision issues, there is potential for them to cause problems in the congested areas highlighted in the preceding sections. It may be worthwhile to model in greater detail these other components to fully realize the congested conditions that will be found in the field.

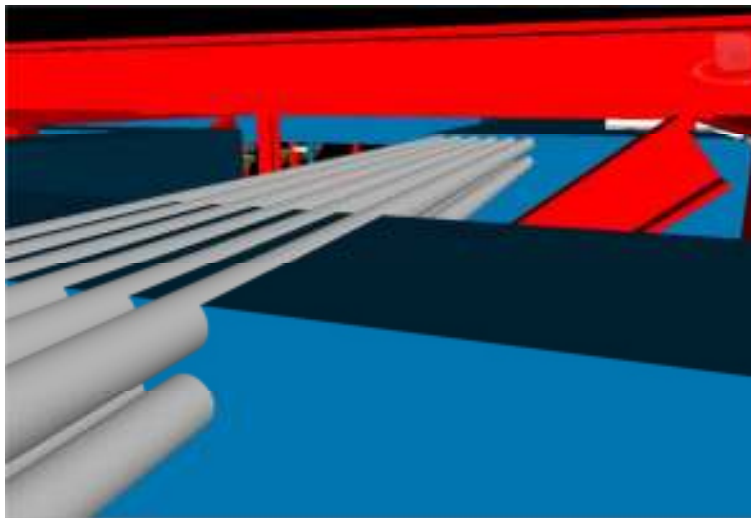


Figure 13: Example of Existing Mechanical Ductwork and Electrical Conduit Collision

ENERGY MODELING

In order to achieve the goals of useful integration and energy modeling, there was a great effort to share project design information through our models. Revit models were created with spaces that had crucial information fields for energy analysis. With the input of our mechanical and electrical engineers' design standards, the model successfully exported embedded building information.

When opened for analysis in a separate program (Trane TRACE), the model retained such important information as room names, floor areas, occupancy, lighting power densities, and equipment load densities. This information would be the basis of our load calculations, energy analysis, and system analysis.

The model was unable however to transfer accurate information about the roof areas and exterior walls, which were later manually updated. These errors stem from the creation methodology and complexity of the architecture model, and would require a significant time investment to ensure their correctness.

The workflow for this space information process would begin with a model of the architecture, most likely completed by the architect. When rooms are developed, the architect could create corresponding spaces. These spaces could then be embedded with information by any party, i.e. occupancy densities from the lab planner, lighting power densities by the electrical engineer. Once building information has been modeled, it could then be exported by the architect for the mechanical engineer to run further analysis. The mechanical engineer must still check to ensure the quality and accuracy of the export, but this model now contains crucial information that previously would have been held by multiple parties in multiple locations. With space information modeling, the model becomes a better tool for sharing project design information.

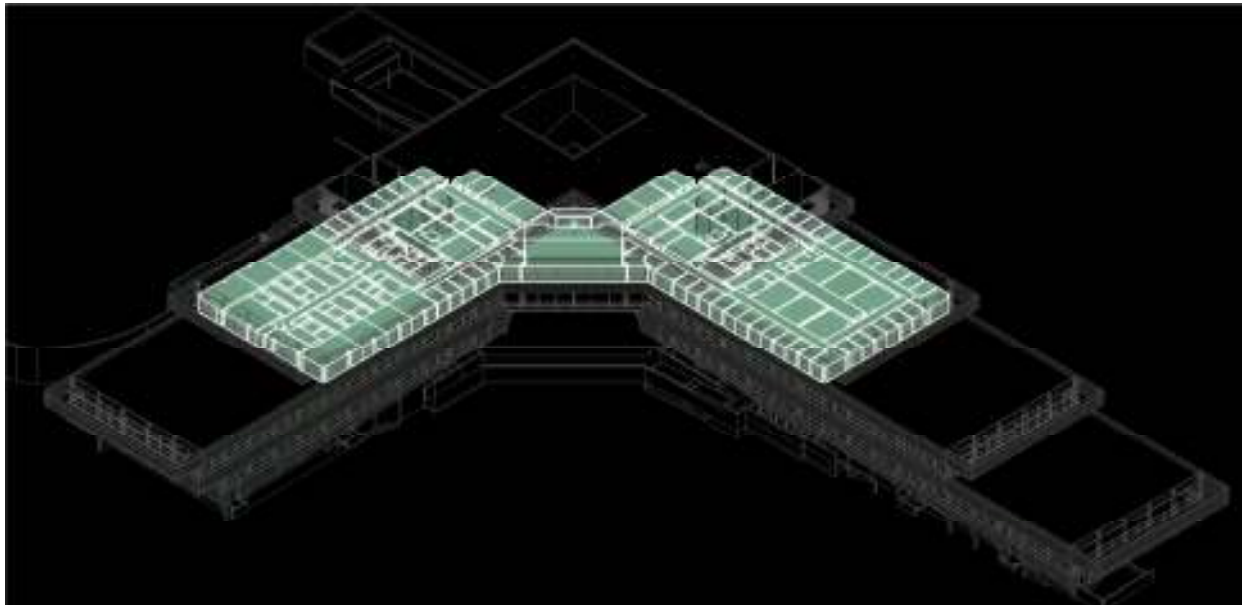


Figure 14: Exported Spaces from Revit Model with Information Embedded

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APPENDIX B: LEED Credit Summary



**LEED for New Construction v 2.2
Registered Project Checklist**

Project Name: PSU- Millennium Science Complex

Project Address: University Park, PA

| Yes | ? | No | | |
|------|---|----|---|---|
| 41 | 6 | 22 | Project Totals (Pre-Certification Estimates) 69 Points | |
| GOLD | | | Certified: 26-32 points | Silver: 33-38 points Gold: 39-51 points Platinum: 52-69 points |

| Yes | ? | No | | |
|-----|---|----|------------------------------------|---|
| 11 | 0 | 3 | Sustainable Sites 14 Points | |
| Yes | | | Prereq 1 | Construction Activity Pollution Prevention Required |
| 1 | 0 | 0 | Credit 1 | Site Selection 1 |
| 1 | 0 | 0 | Credit 2 | Development Density & Community Connectivity 1 |
| 0 | 0 | 1 | Credit 3 | Brownfield Redevelopment 1 |
| 1 | 0 | 0 | Credit 4.1 | Alternative Transportation, Public Transportation 1 |
| 1 | 0 | 0 | Credit 4.2 | Alternative Transportation, Bicycle Storage & Changing Rooms 1 |
| 0 | 0 | 1 | Credit 4.3 | Alternative Transportation, Low-Emitting & Fuel Efficient Vehicles 1 |
| 1 | 0 | 0 | Credit 4.4 | Alternative Transportation, Parking Capacity 1 |
| 1 | 0 | 0 | Credit 5.1 | Site Development, Protect or Restore Habitat 1 |
| 1 | 0 | 0 | Credit 5.2 | Site Development, Maximize Open Space 1 |
| 1 | 0 | 0 | Credit 6.1 | Stormwater Design, Quantity Control 1 |
| 1 | 0 | 0 | Credit 6.2 | Stormwater Design, Quality Control 1 |
| 1 | 0 | 0 | Credit 7.1 | Heat Island Effect, Non-Roof 1 |
| 1 | 0 | 0 | Credit 7.2 | Heat Island Effect, Roof 1 |
| 0 | 0 | 1 | Credit 8 | Light Pollution Reduction 1 |

| Yes | ? | No | | |
|-----|---|----|----------------------------------|---|
| 3 | 1 | 1 | Water Efficiency 5 Points | |
| 1 | 0 | 0 | Credit 1.1 | Water Efficient Landscaping, Reduce by 50% 1 |
| 1 | 0 | 0 | Credit 1.2 | Water Efficient Landscaping, No Potable Use or No Irrigation 1 |
| 0 | 0 | 1 | Credit 2 | Innovative Wastewater Technologies 1 |
| 0 | 0 | 0 | Credit 3.1 | Water Use Reduction, 20% Reduction 1 |
| 1 | 1 | 0 | Credit 3.2 | Water Use Reduction, 30% Reduction 1 |



LEED for New Construction v 2.2 Registered Project Checklist

| Yes | ? | No | | | |
|---|---|----|--------------------------------|---|------------------|
| 5 | 3 | 9 | Energy & Atmosphere | | 17 Points |
| Yes | | | Prereq 1 | Fundamental Commissioning of the Building Energy Systems | Required |
| Yes | | | Prereq 1 | Minimum Energy Performance | Required |
| Yes | | | Prereq 1 | Fundamental Refrigerant Management | Required |
| <p>*Note for EA1: All LEED for New Construction projects registered after June 26, 2007 are required to achieve at least two (2) points.</p> | | | | | |
| 2 | 2 | 6 | Credit 1 | Optimize Energy Performance | 1 to 10 |
| | | | Credit 1.1 | 10.5% New Buildings / 3.5% Existing Building Renovations | 1 |
| | | | → Credit 1.2 | 14% New Buildings / 7% Existing Building Renovations | 2 |
| | | | Credit 1.3 | 17.5% New Buildings / 10.5% Existing Building Renovations | 3 |
| | | | Credit 1.4 | 21% New Buildings / 14% Existing Building Renovations | 4 |
| | | | Credit 1.5 | 24.5% New Buildings / 17.5% Existing Building Renovations | 5 |
| | | | Credit 1.6 | 28% New Buildings / 21% Existing Building Renovations | 6 |
| | | | Credit 1.7 | 31.5% New Buildings / 24.5% Existing Building Renovations | 7 |
| | | | Credit 1.8 | 35% New Buildings / 28% Existing Building Renovations | 8 |
| | | | Credit 1.9 | 38.5% New Buildings / 31.5% Existing Building Renovations | 9 |
| | | | Credit 1.10 | 42% New Buildings / 35% Existing Building Renovations | 10 |
| 0 | 0 | 3 | Credit 2 | On-Site Renewable Energy | 1 to 3 |
| | | | Credit 2.1 | 2.5% Renewable Energy | 1 |
| | | | Credit 2.2 | 7.5% Renewable Energy | 2 |
| | | | Credit 2.3 | 12.5% Renewable Energy | 3 |
| 1 | 0 | 0 | Credit 3 | Enhanced Commissioning | 1 |
| 1 | 0 | 0 | Credit 4 | Enhanced Refrigerant Management | 1 |
| 0 | 1 | 0 | Credit 5 | Measurement & Verification | 1 |
| 1 | 0 | 0 | Credit 6 | Green Power | 1 |



LEED for New Construction v 2.2 Registered Project Checklist

| Yes | ? | No | | | |
|-----|---|----|----------------------------------|--|------------------|
| 5 | 2 | 6 | Materials & Resources | | 13 Points |
| Yes | | | Prereq 1 | Storage & Collection of Recyclables | Required |
| 0 | 0 | 1 | Credit 1.1 | Building Reuse, Maintain 75% of Existing Walls, Floors & Roof | 1 |
| 0 | 0 | 1 | Credit 1.2 | Building Reuse, Maintain 95% of Existing Walls, Floors & Roof | 1 |
| 0 | 0 | 1 | Credit 1.3 | Building Reuse, Maintain 50% of Interior Non-Structural Elements | 1 |
| 1 | 0 | 0 | Credit 2.1 | Construction Waste Management, Divert 50% from Disposal | 1 |
| 1 | 0 | 0 | Credit 2.2 | Construction Waste Management, Divert 75% from Disposal | 1 |
| 0 | 0 | 1 | Credit 3.1 | Materials Reuse, 5% | 1 |
| 0 | 0 | 1 | Credit 3.2 | Materials Reuse, 10% | 1 |
| 1 | 0 | 0 | Credit 4.1 | Recycled Content, 10% (post-consumer + 1/2 pre-consumer) | 1 |
| 0 | 1 | 0 | Credit 4.2 | Recycled Content, 20% (post-consumer + 1/2 pre-consumer) | 1 |
| 1 | 0 | 0 | Credit 5.1 | Regional Materials, 10% Extracted, Processed & Manufactured | 1 |
| 0 | 1 | 0 | Credit 5.2 | Regional Materials, 20% Extracted, Processed & Manufactured | 1 |
| 0 | 0 | 1 | Credit 6 | Rapidly Renewable Materials | 1 |
| 1 | 0 | 0 | Credit 7 | Certified Wood | 1 |

| Yes | ? | No | | | |
|-----|---|----|-------------------------------------|--|------------------|
| 12 | 0 | 3 | Indoor Environmental Quality | | 15 Points |
| Yes | | | Prereq 1 | Minimum IAQ Performance | Required |
| Yes | | | Prereq 2 | Environmental Tobacco Smoke (ETS) Control | Required |
| 1 | 0 | 0 | Credit 1 | Outdoor Air Delivery Monitoring | 1 |
| 0 | 0 | 1 | Credit 2 | Increased Ventilation | 1 |
| 1 | 0 | 0 | Credit 3.1 | Construction IAQ Management Plan, During Construction | 1 |
| 1 | 0 | 0 | Credit 3.2 | Construction IAQ Management Plan, Before Occupancy | 1 |
| 1 | 0 | 0 | Credit 4.1 | Low-Emitting Materials, Adhesives & Sealants | 1 |
| 1 | 0 | 0 | Credit 4.2 | Low-Emitting Materials, Paints & Coatings | 1 |
| 1 | 0 | 0 | Credit 4.3 | Low-Emitting Materials, Carpet Systems | 1 |
| 1 | 0 | 0 | Credit 4.4 | Low-Emitting Materials, Composite Wood & Agrifiber Products | 1 |
| 1 | 0 | 0 | Credit 5 | Indoor Chemical & Pollutant Source Control | 1 |
| 1 | 0 | 0 | Credit 6.1 | Controllability of Systems, Lighting | 1 |
| 0 | 0 | 1 | Credit 6.2 | Controllability of Systems, Thermal Comfort | 1 |
| 0 | 0 | 1 | Credit 7.1 | Thermal Comfort, Design | 1 |
| 1 | 0 | 0 | Credit 7.2 | Thermal Comfort, Verification | 1 |
| 1 | 0 | 0 | Credit 8.1 | Daylight & Views, Daylight 75% of Spaces | 1 |
| 1 | 0 | 0 | Credit 8.2 | Daylight & Views, Views for 90% of Spaces | 1 |



LEED for New Construction v 2.2 Registered Project Checklist

| Yes | ? | No | | |
|----------|----------|----------|--|-----------------|
| 5 | 0 | 0 | Innovation & Design Process | 5 Points |
| 1 | 0 | 0 | Credit 1.1 Innovation in Design: Provide Specific Title | 1 |
| 1 | 0 | 0 | Credit 1.2 Innovation in Design: Provide Specific Title | 1 |
| 1 | 0 | 0 | Credit 1.3 Innovation in Design: Provide Specific Title | 1 |
| 1 | 0 | 0 | Credit 1.4 Innovation in Design: Provide Specific Title | 1 |
| 1 | 0 | 0 | Credit 2 LEED® Accredited Professional | 1 |

APPENDIX C: ASHRAE CLIMATIC DESIGN INFORMATION

2009 ASHRAE Handbook - Fundamentals (IP)

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ALTOONA BLAIR CO ARPT, PA, USA

WMO#: 725126

Lat **40.36N** Long **78.32W** Elev **1470** SdP **13.93** Time Zone: **-5.00 (NAE)** Period **82-06** WBAN **14736**

Annual Heating and Humidification Design Conditions

| Coldest Month | Heating DB | | Humidification DP/MCDB and HR | | | | | | Coldest month WS/MCDB | | | | MCWS/PCWD to 99.6% DB | |
|---------------|------------|------------|-------------------------------|------------|------------|-------------|------------|-------------|-----------------------|-------------|-------------|-------------|-----------------------|------------|
| | 99.6% | 99% | 99.6% | | 99% | | 0.4% | | 1% | | MCWS | PCWD | | |
| | | | DP | HR | MCDB | DP | HR | MCDB | WS | MCDB | | | | |
| 1 | 4.7 | 9.6 | -6.4 | 4.1 | 7.5 | -1.7 | 5.3 | 11.9 | 27.5 | 29.4 | 24.9 | 27.1 | 8.9 | 260 |

Annual Cooling, Dehumidification, and Enthalpy Design Conditions

| Hottest Month | Hottest Month DB Range | Cooling DB/MCWB | | | | | | Evaporation WS/MCDB | | | | | | MCWS/PCWD to 0.4% DB | |
|---------------|------------------------|-----------------|-------------|-------------|-------------|-------------|-------------|---------------------|-------------|-------------|-------------|-------------|-------------|----------------------|------------|
| | | 0.4% | | 1% | | 2% | | 0.4% | | 1% | | 2% | | MCWS | PCWD |
| | | DB | MCWB | DB | MCWB | DB | MCWB | WS | MCDB | WS | MCDB | WS | MCDB | | |
| 7 | 19.3 | 88.5 | 72.0 | 85.7 | 70.7 | 83.0 | 69.6 | 74.7 | 83.9 | 73.2 | 82.0 | 71.6 | 79.8 | 8.0 | 280 |

| Dehumidification DP/MCDB and HR | | | | | | | | | Enthalpy/MCDB | | | | | | Hours 8 to 4 & 55/69 |
|---------------------------------|--------------|-------------|-------------|--------------|-------------|-------------|--------------|-------------|---------------|-------------|-------------|-------------|-------------|-------------|----------------------|
| 0.4% | | | 1% | | | 2% | | | 0.4% | | 1% | | 2% | | |
| DP | HR | MCDB | DP | HR | MCDB | DP | HR | MCDB | Enth | MCDB | Enth | MCDB | Enth | MCDB | |
| 72.0 | 125.0 | 79.6 | 70.3 | 118.0 | 77.7 | 89.1 | 112.9 | 78.2 | 39.1 | 83.9 | 37.6 | 82.0 | 36.3 | 79.9 | 731 |

Extreme Annual Design Conditions

| Extreme Annual WS | | | Extreme Max WB | Extreme Annual DB | | | | n-Year Return Period Values of Extreme DB | | | | | | | |
|-------------------|-------------|-------------|----------------|-------------------|-------------|--------------------|------------|---|-------------|--------------|-------------|--------------|-------------|--------------|--------------|
| 1% | 2.5% | 5% | | Mean | | Standard deviation | | n=5 years | | n=10 years | | n=20 years | | n=50 years | |
| | | | | Min | Max | Min | Max | Min | Max | Min | Max | Min | Max | | |
| 21.9 | 18.8 | 17.2 | 82.4 | -2.6 | 92.5 | 8.1 | 3.5 | -8.4 | 95.0 | -13.2 | 97.1 | -17.7 | 99.1 | -23.6 | 101.6 |

Monthly Climatic Design Conditions

| | Annual | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | |
|---|----------|----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | |
| Temperatures, Degree-Days and Degree-Hours | Tavg | 50.4 | 27.9 | 30.6 | 38.1 | 49.5 | 58.8 | 67.5 | 71.7 | 70.0 | 62.6 | 52.2 | 42.6 | 31.9 |
| | Sd | | 11.40 | 9.59 | 10.63 | 9.41 | 8.00 | 6.47 | 5.14 | 5.51 | 7.30 | 8.33 | 9.28 | 10.28 |
| | HDD50 | 2679 | 690 | 546 | 398 | 121 | 15 | 0 | 0 | 4 | 76 | 259 | 570 | |
| | HDD65 | 5959 | 1150 | 964 | 837 | 472 | 226 | 50 | 7 | 19 | 130 | 404 | 673 | 1027 |
| | CDD50 | 2810 | 4 | 2 | 28 | 105 | 287 | 526 | 672 | 619 | 381 | 143 | 36 | 7 |
| | CDD65 | 617 | 0 | 0 | 2 | 6 | 33 | 126 | 214 | 173 | 56 | 7 | 0 | 0 |
| CDH74 | | 4899 | 0 | 0 | 16 | 76 | 336 | 1003 | 1711 | 1299 | 417 | 40 | 1 | 0 |
| | CDH90 | 1333 | 0 | 0 | 2 | 10 | 57 | 260 | 524 | 375 | 94 | 1 | 0 | 0 |
| Monthly Design Dry Bulb and Mean Coincident Wet Bulb Temperatures | 0.4% | DB | 61.1 | 61.4 | 75.6 | 81.4 | 85.5 | 89.8 | 92.3 | 91.5 | 87.4 | 78.5 | 70.7 | 64.4 |
| | | MCWB | 55.9 | 50.0 | 59.6 | 63.6 | 68.3 | 72.5 | 73.0 | 73.5 | 69.5 | 64.5 | 58.6 | 56.9 |
| | 2% | DB | 55.1 | 53.8 | 67.5 | 75.5 | 81.6 | 86.0 | 88.8 | 87.5 | 82.4 | 74.2 | 65.0 | 57.8 |
| | | MCWB | 49.5 | 45.7 | 54.8 | 59.4 | 65.7 | 70.6 | 72.8 | 71.6 | 67.8 | 62.6 | 55.3 | 52.0 |
| 5% | DB | 48.4 | 48.6 | 60.8 | 70.2 | 78.0 | 83.1 | 85.7 | 84.0 | 78.9 | 70.2 | 61.1 | 51.7 | |
| | MCWB | 43.2 | 41.9 | 51.2 | 57.2 | 64.0 | 69.5 | 71.5 | 70.4 | 66.3 | 60.5 | 54.1 | 46.1 | |
| 10% | DB | 42.5 | 44.4 | 54.4 | 65.1 | 73.3 | 80.2 | 82.4 | 81.2 | 75.2 | 68.2 | 57.0 | 45.7 | |
| | MCWB | 37.8 | 39.3 | 46.6 | 54.0 | 61.5 | 68.0 | 70.4 | 69.2 | 65.5 | 58.5 | 51.2 | 40.8 | |
| Monthly Design Wet Bulb and Mean Coincident Dry Bulb Temperatures | 0.4% | WB | 57.3 | 52.5 | 61.8 | 65.7 | 71.4 | 76.1 | 77.4 | 76.2 | 73.2 | 68.2 | 61.4 | 58.5 |
| | | MCDB | 60.2 | 58.5 | 72.5 | 75.9 | 81.9 | 84.2 | 87.2 | 85.9 | 81.4 | 75.3 | 66.5 | 64.2 |
| | 2% | WB | 51.0 | 46.8 | 56.5 | 62.0 | 68.5 | 73.4 | 74.9 | 74.1 | 70.7 | 65.2 | 58.4 | 53.5 |
| | | MCDB | 54.4 | 52.2 | 64.8 | 71.7 | 77.8 | 81.7 | 84.4 | 83.5 | 78.0 | 70.2 | 63.1 | 57.6 |
| | 5% | WB | 43.5 | 43.1 | 51.6 | 59.1 | 66.1 | 71.4 | 73.3 | 72.5 | 68.9 | 62.4 | 55.4 | 46.9 |
| | | MCDB | 47.4 | 47.8 | 59.5 | 68.0 | 74.7 | 79.6 | 82.3 | 81.0 | 75.2 | 68.2 | 59.3 | 50.5 |
| | 10% | WB | 38.0 | 39.5 | 47.1 | 55.9 | 63.6 | 69.8 | 71.8 | 70.9 | 67.2 | 60.5 | 51.7 | 41.6 |
| | | MCDB | 42.3 | 43.8 | 53.9 | 64.0 | 71.2 | 77.6 | 80.0 | 78.4 | 72.8 | 65.4 | 56.6 | 45.8 |
| Mean Daily Temperature Range | 3% DB | MCDBR | 12.9 | 14.5 | 16.7 | 19.5 | 19.6 | 19.2 | 18.3 | 19.6 | 19.3 | 18.3 | 14.9 | 13.0 |
| | | MCDBR | 18.8 | 21.3 | 25.0 | 28.0 | 25.5 | 22.8 | 22.8 | 23.3 | 24.0 | 23.7 | 20.8 | 19.3 |
| | 5% WB | MCWBR | 15.1 | 15.8 | 15.9 | 15.0 | 12.7 | 10.9 | 10.1 | 10.7 | 12.0 | 13.7 | 14.4 | 15.1 |
| | | MCWBR | 17.2 | 18.8 | 22.5 | 22.9 | 21.6 | 19.6 | 19.0 | 19.8 | 18.1 | 19.6 | 17.6 | 17.9 |
| Clear Sky Solar Irradiance | taud | | 0.301 | 0.324 | 0.361 | 0.361 | 0.415 | 0.473 | 0.482 | 0.486 | 0.392 | 0.349 | 0.318 | 0.300 |
| | | taud | 2.397 | 2.247 | 2.155 | 2.248 | 2.069 | 1.910 | 1.913 | 1.879 | 2.215 | 2.330 | 2.438 | 2.472 |
| | Ebn,noon | | 274 | 281 | 281 | 289 | 274 | 258 | 254 | 248 | 268 | 269 | 265 | 265 |
| | | Edh,noon | 29 | 37 | 44 | 43 | 52 | 61 | 60 | 60 | 41 | 34 | 28 | 26 |

- | | | | | | |
|-------------------|---|-------|---|-----------|---|
| CDDn | Cooling degree-days base n°F, °F-day | Lat | Latitude, ° | Period | Years used to calculate the design conditions |
| CDHn | Cooling degree-hours base n°F, °F-hour | Long | Longitude, ° | Sd | Standard deviation of daily average temperature, °F |
| DB | Dry bulb temperature, °F | MCDB | Mean coincident dry bulb temperature, °F | StdP | Standard pressure at station elevation, psi |
| DP | Dew point temperature, °F | MCDBR | Mean coincident dry bulb temp. range, °F | taub | Clear sky optical depth for beam irradiance |
| Ebn,noon | Clear sky beam normal and diffuse horizontal irradiances at solar noon, Btu/h/ft ² | MCDB | Mean coincident dew point temperature, °F | taud | Clear sky optical depth for diffuse irradiance |
| Edh,noon | zonal irradiances at solar noon, Btu/h/ft ² | MCWB | Mean coincident wet bulb temperature, °F | Tavg | Average temperature, °F |
| Elev | Elevation, ft | MCWBR | Mean coincident wet bulb temp. range, °F | Time Zone | Hours ahead or behind UTC, and time zone code |
| Enth | Enthalpy, Btu/lb | MCWS | Mean coincident wind speed, mph | WB | Wet bulb temperature, °F |
| HDDn | Heating degree-days base n°F, °F-day | MCWBR | Mean coincident wet bulb temp. range, °F | WBAN | Weather Bureau Army Navy number |
| Hours 8/4 & 55/69 | Number of hours between 8 a.m. and 4 p.m. with DB between 55 and 69 °F | MCDBR | Mean dry bulb temp. range, °F | WMO# | World Meteorological Organization number |
| HR | Humidity ratio, grains of moisture per lb of dry air | PCWD | Prevailing coincident wind direction, °, 0 = North, 90 = East | WS | Wind speed, mph |

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