

Shaun Kreidel Structural Option

AE Senior Thesis Spring 2010

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Existing Building Information

Location

- 2130 G Street, NW Washington, D.C.
- Foggy Bottom District

Building Statistics

- Function | Educational
- Occupant | District of Columbia Schools
- Size | 68,000 sq. ft.
- Stories | 4 stories (1 Below Grade)

Project Cost

• \$39.2 million

Existing Gravity System

- Composite steel system
- W10 to W33 sections
- 3 ½" LWC over 2" 20 GA LOK composite steel floor decking

Existing Foundation System

- Shallow foundation
- Reinforced cast-in-place spread footings and grade beams
- Existing footings of the school require underpinning

Existing Lateral System

- The addition is divided by an expansion joint
- Joint creates total of three lateral systems
- Referred to as "Area 1" and "Area 2" in this presentation
- Braced frames and shear walls resist lateral loads
 - Braced frames comprised of HSS square sections
 - Shear Walls are 12" and 8" thick

Project Goals

Problem Statement

- wide flange beams which range from W10 to W33 sections
- 5 ¼" decking system
- total floor depth amounts to 38 ¼"
- welded moment connections required for cantilever

- Structural Depth Study | Redesign gravity system
 - Post tensioned slab and one way slab
 - Limit total floor depth
- Structural Depth Study | Redesign lateral system
 - Remove shear walls and braced frames
 - Concrete moment frames
- Construction Management Breadth Study
 - Cost effect of structural system change
 - Schedule influence of new structural system
- Architectural Breadth Study
 - Aesthetic influence of dropped ceilings

Structural Depth Study

Floor Plan Alterations

- Area 1
 - Column lines G and 7 moved 6.25" towards the interior
 - Column line 5 was moved 14.25" to south
- Area 2
 - Column line A shifted 14" to west and B shifted 16" to east
 - Column lines 1 and 7 shifted 6" to south and north respectively
 - Columns along A.5 and C were deleted
 - Column located in green
 - was added



PT Overview

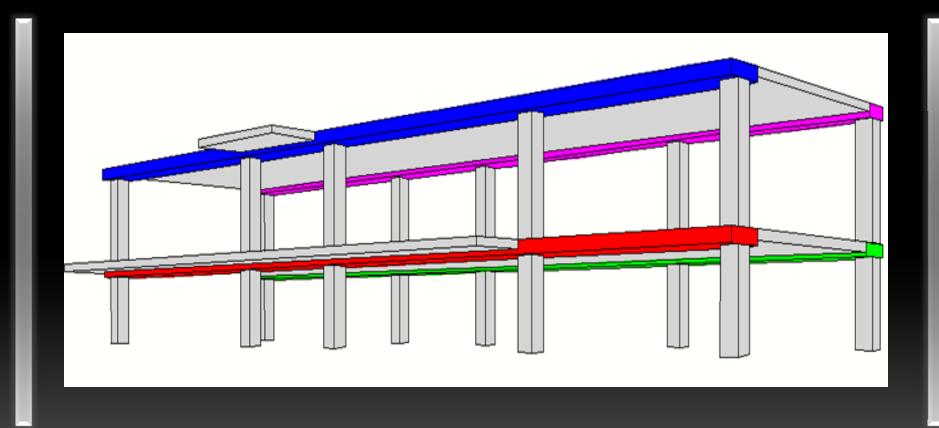
- Method of prestressing
- Tendon tensioned after concrete has hardened
- Chapter 18 of ACI 318-05
- Unbonded tendons
- Tendons fabricated with plastic sheathing and grease
- ½" diameter, 7 wire strands

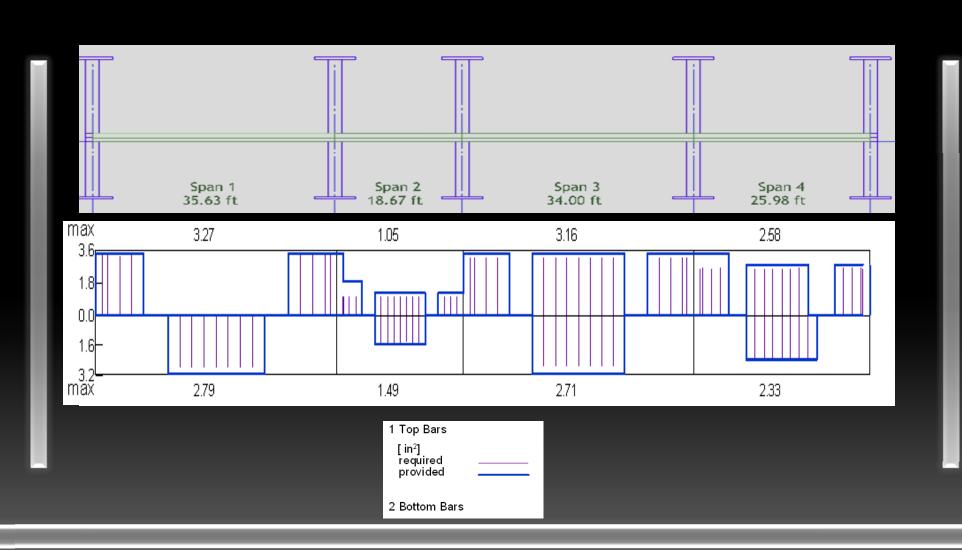
Tendon Properties Area= .153 in² f_{pu} = 270 ksi Estimated Prestress Loss= 15ksi f_{se} = .7*(f_{pu})- 15ksi= 174 P_{eff} =A* f_{se} = 26.6 kip/tendon P/A: Max=300, Min=150

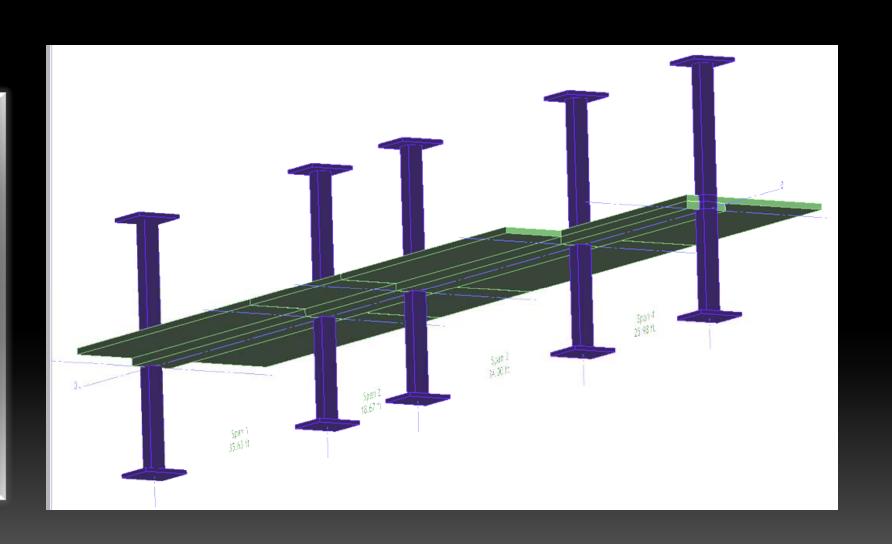
Shortening Restraint

- Important to allow for the shortening of slab
- Reduces the amount of cracking due to shrinkage
- Isolate the slab from the foundation wall
- Isolate the perimeter columns
- Column lines were displaced from the foundation wall

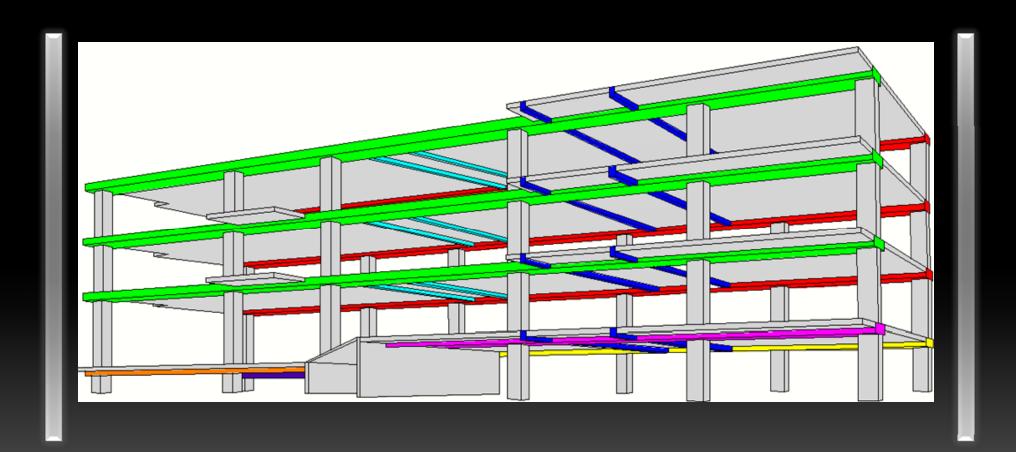


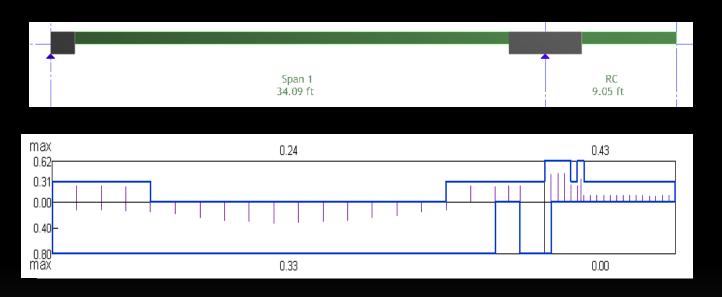










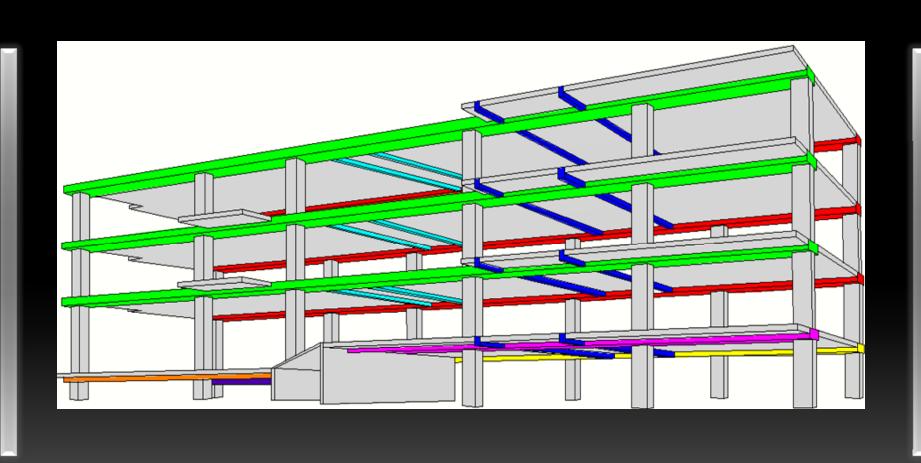


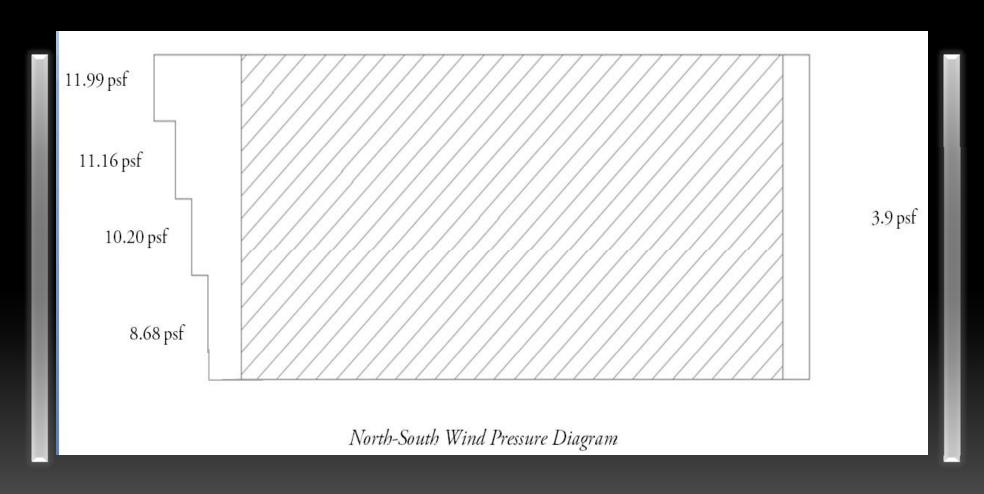
| Span | Class | Туре | W |
|------|-------|------|-------|
| | | | k/ft2 |
| ALL | LL | U | 0.050 |
| ALL | SDL | U | 0.015 |

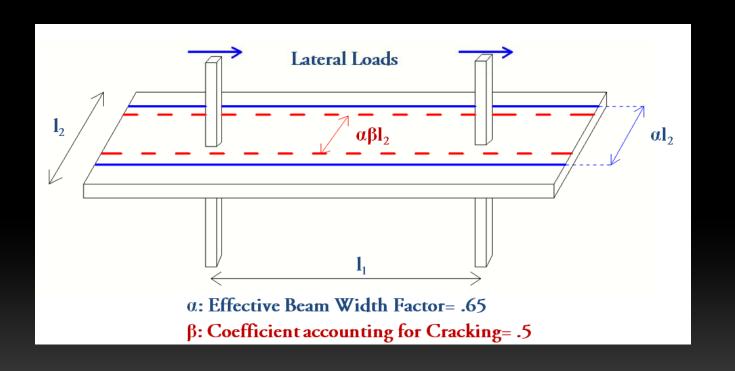
$$L = L_o \left(0.25 + \frac{15}{\sqrt{K_{LL} A_T}} \right)$$

[in²]
required ____
provided ____

Reinforcement perpendicular to tendons: As= .0018*b*h







SCHOOL WITHOUT WALLS

WASHINGTON D.C.

| Story | Diaphragm | Load | UX (in) | UY (in) |
|-----------------|-----------|---------------|---------------------|---------------------|
| STORY4 | D4 | XWIND | 1.1218 | 0.0007 |
| STORY4 | D4 | YWIND | -0.0012 | 0.1851 |
| STORY4 | D4 | XQUAKE | <mark>1.331</mark> | 0.0016 |
| STORY4 | D4 | YQUAKE | 0.0013 | <mark>0.7267</mark> |
| STORY4 | D4 | CASE3 | 0.8405 | 0.1394 |
| STORY4 | D4 | CASE2X | 0.8772 | 0.0033 |
| STORY4 | D4 | CASE2Y | -0.0047 | 0.1386 |
| STORY4 | D4 | CASE4 | 0.8725 | 0.1418 |
| STORY3 | D3 | XWIND | 0.9105 | 0.0003 |
| STORY3 | D3 | YWIND | -0.0008 | 0.1591 |
| STORY3 | D3 | XQUAKE | <mark>1.0466</mark> | 0.0003 |
| STORY3 | D3 | YQUAKE | 0.0007 | <mark>0.6051</mark> |
| STORY3 | D3 | CASE3 | 0.6823 | 0.1196 |
| STORY3 | D3 | CASE2X | 0.705 | -0.0002 |
| STORY3 | D3 | CASE2Y | -0.0029 | 0.1194 |
| STORY3 | D3 | CASE4 | 0.7021 | 0.1192 |
| STORY2 | D2 | XWIND | 0.5796 | 0.0004 |
| STORY2 | D2 | YWIND | -0.0003 | 0.1097 |
| STORY2 | D2 | XQUAKE | <mark>0.6395</mark> | 0.0002 |
| STORY2 | D2 | YQUAKE | 0.0003 | 0.4 |
| STORY2 | D2 | CASE3 | 0.4345 | 0.0826 |
| STORY2 | D2 | CASE2X | 0.4444 | -0.0008 |
| STORY2 | D2 | CASE2Y | -0.0013 | 0.0824 |
| STORY2 | D2 | CASE4 | 0.4431 | 0.0816 |
| ENTRANCE | D1 | XWIND | 0.0622 | 0.0001 |
| ENTRANCE | D1 | YWIND | 0 | 0.0116 |
| ENTRANCE | D1 | XQUAKE | 0.0652 | 0 |
| ENTRANCE | D1 | YQUAKE | 0 | 0.0401 |
| ENTRANCE | D1 | CASE3 | 0.0466 | 0.0088 |
| ENTRANCE | D1 | CASE2X | 0.0467 | -0.0006 |
| ENTRANCE | D1 | CASE2Y | 0 | 0.0088 |
| ENTRANCE | D1 | CASE4 | 0.0467 | 0.0082 |

Construction Management Breadth Study

| Existing | Steel | Struc | ture |
|----------|-------|-------|------|
| | | | |

Concrete Structure

| Description | Total \$ | Total \$ ** |
|---------------------------|-------------|----------------|
| Formwork | 2,743 | 76,057 |
| | | |
| Concrete reinforcing | 4,557 | 38,921 |
| Cast in place concrete | 12,077 | 31,576 |
| Structural framing | 53,590 | |
| Metal deck | 11,135 | |
| Fire and smoke protection | 10,304 | |
| Total Estimate | 94,406 | 146,555 |

Existing Steel Structure

Concrete Structure

| Description | Total \$ ^^ | Total \$ |
|---------------------------|----------------|-------------|
| Formwork | 82,989 | 178,464 |
| Concrete reinforcing | 63,058 | 95,135 |
| Cast in place concrete | 47,731 | 80,011 |
| Structural framing | 161,102 | |
| Metal deck | 25,506 | |
| Fire and smoke protection | 17,734 | |
| Total Estimate | 398,121 | 353,610 |

Conclusions

Acknowledgements

Questions

&

Comments