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# **Technical Report 1** ASHRAE Std. 62.1 & 90.1 Analysis



# Duval County Unified Courthouse Facility

Jacksonville, Florida

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### **Executive Summary**

The purpose of this report is to determine the compliance or noncompliance of The Duval County Unified Courthouse Facility of Jacksonville, Florida with the American Society of Heating, Refrigerating, and Air-Conditioning Engineers, Inc. (ASHRAE) Standards 62.1 and 90.1

The ASHRAE Standard 62.1 Analysis done on the facility showed that the building is largely compliant with Section 5 based on Indoor Air Quality. The facility meets or exceeds all requirements of this section. Section 6 was completed by calculating the air flow rates for three AHU's that serve the west side of the facility. The three AHU's chosen were based on building symmetry, spaces served, and space repetition on other levels. AHU 1W-1 was chosen to represent the majority of the west side of the first level being predominantly office space. AHU 2W-1 was chosen to represent the west side courtrooms on the other levels. AHU 7W-3 was chosen as it serves the auxiliary spaces around the courtrooms that are repeated on other levels. The calculations show that each space receives adequate ventilation.

The ASHRAE Standard 90.1 Analysis for The Duval County Unified Courthouse Facility confirmed that the facility is mostly compliant with the standard. The analysis followed the Mandatory Provisions and Prescriptive Path Methods of determining compliance. Section 5 – Building Envelope, did not fully comply by having a higher than allowed ratio of fenestration to gross wall area for three of the four sides. This was compensated, however, by using very efficient glazing that exceeded the requirements of U-Value and SHGC. All equipment was analyzed in Section 6 – HVAC, and met the requirements, except for some supply air fans when calculating the Fan Power Limitations. Some fans used a slightly larger horsepower than the standard allows most likely due to filters and large, separated areas. The lighting power density just meets the requirement and could be altered to make it more efficient.

#### **Building Summary**

The Duval County Unified Courthouse Facility is a 798,000 square feet, 7 level government building. The facility houses 51 total courtrooms, judicial offices, hearing spaces, and conference areas. It also includes parking areas, a detention zone, and building support areas on the first floor.

Its façade is predominantly precast limestone aggregate concrete panels and vertical spanning aluminum curtain wall vision glazing. Three large aluminum curtain walls with spandrel glazing also exist under the roofs to allow natural lighting into the front lobby and central atrium. The roof system is primarily a flat composite concrete insulated roof. Two sloped roofs exist over the lobby and central core of the building which use an insulated standing seam metal roof deck system.

#### **Systems** *Airside:*

The Duval County Unified Courthouse Facility utilizes 25 Air Handling Units (AHU's) to distribute air throughout the building. The 51 courtrooms are served by 14 AHU's while the other 11 AHU's serve the remainder of the building. All AHU's are served with outdoor air by three Makeup Air Units (MAU's), two of which are heat recovery units from exhaust air. Most units are located on the interior of the building in mechanical rooms or penthouses with the exception of two AHU's and two MAU's which are all located on the second floor roof.

#### Zone Conditioning:

Most areas are served by Variable Air Volume (VAV) AHU's with VAV boxes in the zones. The VAV boxes also utilize terminal reheat coils. The exceptions to VAV systems are the four courtrooms on the third and fourth floors at the northern side of the building. Each of these four courtrooms is served by its own Constant Air Volume (CAV) unit. Fan Coil Units (FCU) are also utilized in some corridors for additional conditioning.

#### Waterside:

Heating hot water used by AHU heating coils, terminal VAV boxes, and FCU's is generated by two natural gas boilers in a first floor mechanical room. Each boiler has an output of 13,390 MBH. Chilled water is supplied by J.E.A. Public Utility Company. The chilled water is pumped from a central pumping room to the AHU cooling coils and FCU's.

## ASHRAE Std. 62.1

#### Section 5 Analysis – Systems & Equipment

#### Section 5.1 Natural Ventilation

No windows in The Duval County Unified Courthouse Facility are operable, hence, Natural Ventilation is not used in the building and this subsection does not apply.

#### Section 5.2 Ventilation Air Distribution

Assuming that all VAV terminal boxes are calibrated correctly to allow proper minimum outdoor air flow, then each space meets the necessary air flow requirements.

#### Section 5.3 Exhaust Duct Location

All exhaust ducts that may convey potentially harmful contaminants such as those from toilet rooms, locker rooms, and holding cells are negatively pressurized with respect to areas that they pass.

#### Section 5.4 Ventilation System Controls

All AHU's run on a set schedule to operate at optimum start based on the building schedule.  $CO_2$  sensors are used on return air ducts to verify that adequate ventilation air is being maintained. The MAU's operate 24 hours per day, seven days per week to constantly bring in outdoor ventilation air to dilute the space air.

#### Section 5.5 Airstream Surfaces

Most airstream surfaces used in ductwork and other equipment are sheet metal surfaces and metal fasteners. Some ducts utilize a 1" interior duct liner, however. These liners comply with ASTM C 1071, are coated with an antimicrobial coating, and covered with a film that complies with UL 181.

#### Section 5.6 Outdoor Air Intakes

All three outdoor air intakes for the three MAU's are at least the minimum distance away from any specific outdoor contaminant source as mentioned in Table 5-1 in section 5.6.1. All intakes are capable of managing rain entrainment and intrusion through the use of rain hoods. All intakes utilize insect and bird screens compliant with section 5.6.5.

#### Section 5.7 Local Capture of Contaminants

All exhaust from parking areas, toilet rooms, and holding cells are ducted to exhaust fans and expelled from the building.

#### Section 5.8 Combustion Air

All combustion air from the two boilers is ducted separately through an exhaust flue up through the seventh floor roof and out of the building.

#### Section 5.9: Particulate Matter Removal

All AHU's utilize air filters that are rated at either MERV 8 or MERV 13, both of which are compliant with section 5.9.

#### Section 5.10 Dehumidification System

The facility uses the AHU's cooling coils as a means of dehumidification and sensors in return air ducts measure relative humidity of the spaces. The controls do not allow the relative humidity to go above 60%. The building's outdoor air intake is greater than the exhaust air flow.

#### Section 5.11 Drain Pans

All drain pans have a 2% slope in at least two planes are two inches deep. The drain is located at the lowest point and is sealed. The drain pan extends at least one foot past the coil.

#### Section 5.12 Finned-Tube Coils and Heat Exchangers

Drain pans are provided beneath all coils and all coils have adequate space provided for cleaning and replacement.

#### Section 5.13 Humidifiers and Water-Spray Systems

The Duval County Unified Courthouse Facility does not use any separate humidifiers or water-spray systems.

#### Section 5.14 Access for Inspection, Cleaning and Maintenance

All access doors are at least 24" wide by unit casing height (with a maximum of 60" tall) to allow unobstructed access for cleaning and replacement of equipment.

#### Section 5.15 Building Envelope and Interior Surfaces

All building envelope walls utilize a weather barrier to prevent water entering the building. A vapor barrier is provided inside the wall construction to limit water vapor transfer. All chilled water pipes are insulated to protect against surface condensation.

#### Section 5.16 Buildings with Attached Parking Garages

All interior parking areas on the first level are negatively pressurized compared to adjacent occupant spaces to restrict vehicular exhaust transfer to those spaces. The garages open into vestibules or separated corridors and directly exhaust air outside of the building.

#### Section 5.17 Air Classification and Recirculation

Most of the building's return air is classified as Class 1 from the majority of office, courtroom, and assembly spaces. Toilet room and holding cell is considered Class 2, and may be recirculated within those zones but is directly exhausted outside of the building.

#### Section 5.18 Requirements for Buildings Containing ETS Areas & ETS-Free Areas

The Duval County Unified Courthouse Facility is a non-smoking facility, therefore it is only classified as an ETS-Free Area. The facility does not apply to this sections requirements.

#### Section 6 Analysis – Procedures

For the purpose of calculating ventilation rates for The Duval County Unified Courthouse Facility, three typical AHU's have been selected. This is due to the symmetry of the building, the repetition of the spaces and how the AHU's serve the spaces. The AHU's being analyzed are 1W-1, 2W-1, and 7W-3.

#### **Zone Calculations Procedure** Breathing Zone Outdoor Airflow (V<sub>bz</sub>):

 $V_{bz}=R_p*P_z*+R_a*A_z$ 

(Equation 6-1)

Where: A<sub>z</sub>=Zone Floor Area (ft<sup>2</sup>)

 $P_z$ =Zone Population, The largest number of people to occupy the space [Estimated from values in Table 6-1 of Std. 62.1]

R<sub>p</sub>=Outdoor Airflow Rate per Person (cfm/person) [Defined in Table 6-1 of Std. 62.1]

R<sub>a</sub>=Outdoor Airflow Rate per Unit Area (cfm/ft<sup>2</sup>) [Defined in Table 6-1 of Std. 62.1]

Zone Air Distribution Effectiveness (E<sub>z</sub>)

E<sub>z</sub>=1 [Defined in Table 6-2 of Std. 62.1]

Zone Air Outdoor Airflow (Voz)

 $V_{oz}=V_{bz}/E_z$ 

(Equation 6-2)

Primary Outdoor Air Fraction  $(Z_p)$ 

 $Z_p = V_{oz} / V_{pz}$ 

(Equation 6-5)

System Ventilation Efficiency  $(E_v)$ 

 $E_{\nu}$  is found using the maximum  $Z_{p}$  value [Defined in Table 6-3 of Std. 62.1]

Uncorrected Outdoor Air Intake (Vou)

 $V_{ou}=D\sum_{all \ zones}(R_p*P_z)+\sum_{all \ zones}(R_a*A_z)$  (Equation 6-6)

Where: D=Occupant Diversity= $P_s/\sum_{all zones} P_z$  (Equation 6-7)

P<sub>s</sub>=System Population, The total population in the area served by the system

Outdoor Air Intake (Vot)

 $V_{ot}=V_{ou}/E_v$  (Equation 6-7)

#### Assumptions

Only AHU's 2W-1, 1W-1, and 7W-3 are being calculated because they serve the west half of an extremely symmetrical building. These AHU's have been selected because they serve the different spaces of this side of the courthouse that are repeated on other floors. AHU 2W-1 serves the west courtrooms on level two, which is similar to all other levels. AHU 1W-1 serves the majority of the office space on the west side of the first level. AHU 7W-3 serves the auxiliary areas around the

courtrooms on every floor with courtrooms. This is acceptable due to the similarity and repetition of spaces and symmetrical layout.

Special file rooms such as secure files, file vaults, etc. were analyzed as storage spaces. Vestibules to courtrooms were analyzed as additional corridors due to no major need for people ventilation.

#### **Section 6 Findings**

The Spreadsheets in Appendix B show the airflow of each space analyzed along with the calculation spreadsheet.

From the spreadsheet for AHU 1W-1, it is noted that the highest value of  $Z_p$  is in an interior lobby and has a value of 27%. This seems quite high and upon further inspection it should be noted that it assumed a large volume of people to be in this space at once. It is a relatively small lobby for a small office area in the facility and will never have that amount of people. It is averaged at 1.26 cfm/sf, which seems a little on the high side. This is perhaps due to incorrect people density assumptions in the program.

From the spreadsheet for AHU 2W-1, the  $Z_p$  value is the same for all spaces at 27%. This is because all of these spaces are courtrooms similar in size. The value may seem high, but it is because it assumes a large amount of people to be in the courtrooms. Based on the size and layout of the courtroom, this value may not be too far off and it may fit that many people. It is averaged at 1.53 cfm/sf, but this should only be due to the large volume of people assumed.

From the spreadsheet for AHU 7W-3, the largest  $Z_p$  value is of 48% and for multiple corridors. It is uncertain why these corridors are requiring such a large volume of outside air, though. It is averaged at 0.98 cfm/sf.

#### 62.1 Conclusion

The Duval County Unified Courthouse Facility's HVAC system is well designed to meet all requirements based on Section 5 of Standard 62.1. This effort to meet and exceed these standards helps achieve the goal of increased indoor air quality. Careful placement and design of outdoor air intakes as well as the filtering and precautions taken on airstream surfaces all help to improve the indoor air quality. By meeting the requirements of this section, The Duval County Unified Courthouse Facility has taken the steps to earn LEED points in the Indoor Environmental Quality Category.

Calculations were also performed to be sure that enough outdoor air is being brought in for ventilation rates. Some areas' outdoor air fractions are possibly over estimated based on their large people density based on ASHRAE's assumptions. Through adjustments of real population amounts, these values could be corrected.

## ASHRAE Std. 90.1

ASHRAE Standard 90.1 is an energy standard for buildings that focuses on the energy usage and the efficiency of the Building Envelope, HVAC systems, Service Water Heating, Power & Lighting, and other auxiliary equipment.

#### Section 5 Analysis – Building Envelope

#### Section 5.1.4 Climate

The Duval County Unified Courthouse Facility in Jacksonville, Florida is located in Climate Zone 2A. See Figure 1 below.





#### Section 5.4 Mandatory Provisions

All joints around fenestration, doors, and between walls are sealed as well as any openings in the roof for equipment or shafts. Loading dock weatherseals are not required in Climate Zone 2A. Vestibules in Climate Zone 2A are exempt from section 5.4.3.4, but the Duval County Unified Courthouse Facility has entrance and emergency exit vestibules that do comply with this section.

#### Section 5.5 Prescriptive Building Envelope Option

Section 5.2 of the standard lists two compliance paths, the Prescriptive Building Envelope Option and the Building Envelope Trade-Off Option. The Prescriptive Building Envelope Option is used provided that the building's vertical fenestration area does not exceed 40% of the gross wall area and skylight fenestration does not exceed 5% of the gross roof area. Only the northern façade wall was compliant with this fenestration area. The other three façade walls were over the limit by 5-6%. The southern façade has two large glazed curtain walls to accentuate it as the main entrance. The east and west facades are dominated by the vertical strips of glazing because of peripheral offices and courtrooms, but could be adjusted to comply with the 40% requirement.. The areas are summarized in Table 1. No skylights exist for the facility.

Fenestration Areas										
Façade	Area of Glazing (SF)	Gross Wall Area (SF)	Percentage Glazing	Compliance						
North	31,059	80,965	38%	YES						
South	38,778	86,370	45%	NO						
East	17,181	37,150	46%	NO						
West	17,131	37,150	46%	NO						

#### Table 1

The building envelope materials were compared to Table 5.5-2 for Climate Zone 2A to examine the individual materials' compliance with Standard 90.1 even though three out of the four façade walls are out of compliance due to their fenestration area. Table 2 summarizes the values of the envelope materials for The Duval County Unified Courthouse Facility and the applicable Standard 90.1 values.

Building Envelope Values										
		90.1 Requirements Specified Values								
Opaque Element	Description	Assembly Maximum U-Value	Insulation Minimum R-Value	Assembly U-Value	Insulation R-Value	Compliance				
Roof	Insulation Entirely Above Deck	0.048	20.0	0.048	20	Yes				
Roof	Metal Roof Deck	0.065	19.0	0.063	20	Yes				
Walls, Above Grade	Mass	0.151	5.7	0.168	11	No				

Floors	Mass	0.107	6.3	0.322	None	No
Slab-On- Grade Floor	Unheated	0.730	NR	0.730	None	Yes
Opaque Doors	Swinging	0.700		0.500		Yes
Fenestration	Description	Assembly Maximum U-Value	Assembly Max SHGC	Assembly U-Value	SHGC	Compliance
Metal Framing	Curtainwall/ Storefront	0.70	0.25	.62	.14	Yes
Metal Framing	Entrance Doors	1.10	0.25	.62	.14	Yes
Metal Framing	All Other	0.75	0.25	.39	.14	Yes

#### Table 2

Through this Prescriptive Approach, most building envelope elements were found to be in compliance with the section. Above grade walls have a slightly higher Assembly U-Value due to the non-continuous insulation because of metal stud framing on the interior side of the wall. Floors slabs are not insulated because the temperature of the above and below levels is assumed to be the same.

#### Section 6 Analysis – Heating, Ventilation, and Air Conditioning

#### Section 6.2 Compliance Path

Two compliance paths are available in this section, the Simplified Approach Option or the Mandatory Provisions and Prescriptive Path. The Mandatory Provisions and Prescriptive Path has been selected in order to accurately compare the energy efficiencies of the HVAC equipment

#### Section 6.4 Mandatory Provisions

Zones are equipped with thermostats that will control supply air temperature by directly regulating the chilled water valve. If additional heating energy is required, terminal reheat activates in the zones VAV boxes.

Controls are based on a day-to-day occupied and unoccupied time schedule. During unoccupied times, the system has the capability to setback down to 55°F for heating or 85°F for cooling. Optimum start is used on the AHU's in order to get space temperature to an adequate level before regular occupancy hours.

The MAU's fans are controlled by the need for ventilation air based upon the control on the regular AHU's operation. MAU supply fans will only operate when a connected AHU is in operation. If an MAU supply fan is not operating, its respected outdoor air dampers will be closed.

All ducts and chilled water piping have been insulated to prevent thermal transfer through the material. Ducts and plenums have been sealed to prevent leakage to meet Class C requirements in Section 6.4.4.2.

#### Section 6.5 Prescriptive Path

No economizer control has been found in the control descriptions. Section 6.5.1 lists that there is no economizer requirement for Climate Zone 2A.

All fan motors were analyzed based on their design air flow rate in CFM and their maximum nameplate HP. The equations from Section 6.5 used to find the prescribed HP ratings are as follows:

HP≤CFM*0.0011	(For Constant Volume Fans)
HP≤CFM*0.0015	(For Variable Volume Fans)

Most of the fans are compliant with the standard with the exception of the four CAV AHUs that serve the four individual north side courtrooms and the large air handlers that serve the seventh level. A detailed summary of each fan and its compliance is included in Appendix B.

All VAV fan systems are controlled with a Variable Frequency Drive (VFD), including those over 10HP. Control static pressure setpoints of VAV boxes are reset based on the zone requiring the most pressure.

All water pumps that have a pump head exceeding 100 feet and also use a motor exceeding 50 HP utilize a VFD to vary the flow.

No heat rejection equipment is specified for The Duval County Unified Courthouse Facility because it does not have a central cooling plant. Therefore, no requirements in Section 6.5.5 are applicable to this facility.

Two of the three MAU's are equipped with air-to-air cross flow enthalpy wheels of effectiveness roughly equal to 74%. Each MAU is capable of bringing in 40,000 CFM of outdoor air, and the two heat recovery units exhaust 25,000 CFM. The third MAU, located in a penthouse above the seventh level, that supplies outdoor air to the six AHU's on the seventh level is not equipped with an exhaust fan or energy recovery unit. All air from the spaces served by this unit is exhausted individually through other exhaust fans.

#### Section 6.8 Minimum Equipment Efficiencies

Two Computer Room Air Conditioning (CRAC) units are used for the computer spaces in the building. No submittals were made available for these units, but the HVAC specifications require

they meet the requirements of Section 6.8 in the standard. The required values for these CRAC units is summarized in Table 3.

CRAC Unit Efficiency Requirements										
Туре	Size Category	Heating Section	Sub- Category	Specified Size	Minimum EER	Compliance				
Air Conditioners	≥135,000 BTU/hr and	Electric	Split	193,800 BTU/hr	11.0	YES				
Water Cooled	<240,000 BTU/hr	Resistance	System	180,000 BTU/hr	11.0	YES				

#### Table 3

The heating system utilizes two natural gas boilers that are each rated above the minimum effiency as stated in Section 6.8. The required and specified values are included in Table 4.

Boiler Efficiency Requirements										
Туре	Fuel Category	Input Size Category	Minimum Efficiency	Specified Input Size	Rated Efficiency	Compliance				
Hot Water Boiler	Gas-Fired	>2,500,000 BTU/hr	80%	16,330,000 BTU/hr	82%	YES				
Hot Water Boiler	Gas-Fired	>2,500,000 BTU/hr	80%	16,330,000 BTU/hr	82%	YES				

#### Table 4

All combined heating and cooling supply ducts utilize insulation of R-8 and all return ducts use insulation of R-4. Both of these insulation R-Values are compliant with Zone 2A. All hydronic piping is insulated with the adequate thickness of insulation as per the requirements of Table 6.8.3 in Section 6.8.

#### Section 7 Analysis – Service Water Heating

The Duval County Unified Courthouse Facility uses five Instantaneous Electric Water Heaters (IEW) to serve its domestic hot water needs.

#### Section 7.2 Compliance Paths

There are two paths to follow compliance for Section 7, the Mandatory Provisions and Prescriptive Path or the Energy Cost Budget Method Path. The Mandatory Provisions and Prescriptive Path has been selected in order to analyze the efficiency of the water heaters specified for the facility.

#### Section 7.4 Mandatory Provisions

All necessary hot water pipes are insulated as per Section 7.4.3. All water heaters have the ability to heat up to a maximum of 125 °F and are circulated with a 550 GPM Booster Pump.

#### Section 7.5 Prescriptive Path

No service hot water produced by the IEW's is used for additional space heating.

#### Section 7.8 Performance Requirements for Water Heating Equipment

No submittals have been made available for the efficiency rates of the domestic hot water heaters, but the Plumbing Specifications require that all IEW's be compliant with Section 7 of Standard 90.1.

#### Section 9 Analysis – Lighting

#### Section 9.2 Compliance Paths

This section has two methods of determining compliance for lighting fixtures, the Building Area Method or the Space-By-Space Method. The Building Area Method has been chosen for The Duval County Unified Courthouse Facility because it has the typical spaces of a courthouse and "Courthouse" is a possible Building Area Type as per Table 9.5.1 in Section 9.

#### Section 9.4 Mandatory Provisions

The interior lighting is automatically controlled based a time-of-day schedule on occupancy hours or connected to an occupancy sensor.

#### Section 9.5 Building Area Method Compliance Path

Each floor's lighting was inventoried separately and then summed into a total wattage for the entire usable space of the facility. The analysis is summarized in Table 5 below. The total watts/sf of the facility was calculated to be 1.21, which is only 0.01 watt/sf over the requirement listed for the Courthouse Building Area Type mentioned in the section.

Building Area Method Lighting Power Density Analysis											
Fixture	Level 1	Level 2	Level 3	Level 4	Level 5	Level 6	Level 7	Watts/ Fixture	Total Watts		
A2	245	91	27	27	38	38	0	64	29824		
A3	42	0	0	0	0	0	0	96	4032		
A4	59	0	0	0	0	0	0	216	12744		
A5	27	38	51	51	43	43	0	96	24288		
B2	230	664	72	72	151	151	320	64	106240		
B3	419	257	0	0	20	22	8	96	69696		

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L2	69	106	85	85	80	80	27	64	34048
D2	75	310	215	215	160	250	397	64	103808
D3	0	71	48	48	48	48	0	96	25248
F2	2	31	44	44	41	41	2	64	13120
J2	251	53	48	48	50	50	42	64	34688
J2E	22	0	0	0	0	0	0	64	1408
М	0	50	14	14	12	12	346	50	22400
N1	0	280	378	378	320	320	0	54	90504
N2	67	262	13	13	16	16	619	54	54324
P1	0	0	0	0	4	4	0	100	800
R1	20	54	92	92	82	82	55	39	18603
R2	38	0	0	0	0	0	0	56	2128
U	20	0	0	0	0	0	0	64	1280
W	44	42	40	40	32	32	14	64	15616
Х	101	118	70	70	75	75	55	20	11280
ZP1	0	42	98	98	58	58	0	336	118944
ZP2	43	83	53	53	61	61	212	104	58864
ZP4	13	20	25	25	16	16	6	416	50336
Level SF	165858	157508	86990	81571	81511	87404	87048		
							Total	Area	747890
							Total V	Vattage	904223
							Watt	cs/SF	1.209
							90.1 Re Watt	equired cs/SF	1.2
							Comp	liance	YES

Table 5

#### 90.1 Conclusion

After the preceding calculations and analyses based on the prescriptive methods have been performed, it has been determined that The Duval County Unified Courthouse Facility is mostly compliant with Standard 90.1. The area of the building that is least compliant is Section 6 – Building Envelope. The building sacrifices compliance with fenestration ratios for aesthetic appeal.

Three out of four perimeter walls exceed the 40% maximum fenestration value. The designers seem to have made up for this, however, by using much more efficient glazing with lower U-Values and lower SHGC. The exterior mass walls, however, did not comply with the U-Value requirement. This is due to the metal stud framing on the interior creating non-continuous insulation. The other area that the facility does not fully comply with is the Fan Power Limitations. The AHU fans that serve the CAV zoned courtrooms are slightly over the HP requirement. The other noncompliant fans are in the large AHU's that serve the auxiliary spaces on levels 2-7. These are possibly out of compliance due to the large pressure needed to transfer air around the large spaces on multiple floors.

Most aspects of the facility just met the requirements of the standard and may have room for some improvement. The lighting power density is barely adequate when compared to the requirements of the section (1.21 actual Watts/sf versus 1.20 required Watts/sf). Even with nearly the entire facility being equipped with fluorescents, there are more efficient energy-saver fluorescent lamps available that can be used to decrease the facilities lighting power density. The glazing however exceeds the requirements very well. The specified U-Values are 11% to 48% better than those required. The SHGC is rated at 44% better than the required value.

# References

ASHRAE Standard 62.1 – 2007

ASHRAE Standard 90.1 – 2007

ASHRAE Handbook of Fundamentals

ASHRAE Handbook of HVAC Systems & Equipment

Fan Power Limitation Requirements										
Fan	Specified HP	CFM	Туре	Prescribed HP	Compliance					
AHU-2E-1	15	11000	VAV	16.5	YES					
AHU-3E-1	20	14100	VAV	21.15	YES					
AHU-3E-2	7.5	3300	CAV	3.63	NO					
AHU-4E-1	20	14100	VAV	21.15	YES					
AHU-4E-2	7.5	4300	CAV	4.73	NO					
AHU-5E-1	20	14100	VAV	21.15	YES					
AHU-6E-1	20	14100	VAV	21.15	YES					
AHU-2W-1	15	11000	VAV	16.5	YES					
AHU-3W-1	20	14100	VAV	21.15	YES					
AHU-3W-2	7.5	3300	CAV	3.63	NO					
AHU-4W-1	20	14100	VAV	21.15	YES					
AHU-4W-2	7.5	4300	CAV	4.73	NO					
AHU-5W-1	20	14100	VAV	21.15	YES					
AHU-6W-1	20	14100	VAV	21.15	YES					
AHU-2E-2	30	24300	VAV	36.45	YES					
AHU-2E-3	75	50000	VAV	75	YES					
AHU-7E-1	75	46000	VAV	69	NO					
AHU-7E-2	75	46000	VAV	69	NO					
AHU-7E-3	75	46000	VAV	69	NO					
AHU-1W-1	75	50000	VAV	75	YES					
AHU-2W-2	25	18800	VAV	28.2	YES					
AHU-2W-3	20	16000	VAV	24	YES					
AHU-7W-1	75	46000	VAV	69	NO					
AHU-7W-2	75	46000	VAV	69	NO					
AHU-7W-3	75	46000	VAV	69	NO					
MAU-2E-1S	60	40000	VAV	60	YES					

# **Appendix A – Fan Power Compliance**

MAU-2E-1E	25	25000	VAV	37.5	YES
MAU-2W-1S	60	40000	VAV	60	YES
MAU-2W-1E	25	25000	VAV	37.5	YES
MAU-7-1	60	40000	VAV	60	YES
EF-1E-1	2	11250	VAV	16.875	YES
EF-1E-2	1	3030	VAV	4.545	YES
EF-1E-3	0.33	1310	VAV	1.965	YES
EF-1E-4	5	18770	VAV	28.155	YES
EF-2E-1	5	10050	VAV	15.075	YES
EF-5E-1	0.75	3300	CAV	3.63	YES
EF-7E-1	3	5000	VAV	7.5	YES
EF-7E-2	3	20000	VAV	30	YES
EF-S2E-1	15	20000	VAV	30	YES
EF-S2E-2	5	10000	VAV	15	YES
EF-S2E-3	5	15000	VAV	22.5	YES
EF-S7E-1	25	40000	VAV	60	YES
SPF-E-1	0.75	1440	VAV	2.16	YES
SPF-E-2	1.5	3900	VAV	5.85	YES
SPF-E-3	1.5	2900	VAV	4.35	YES
SPF-E-4	2	4000	VAV	6	YES
SPF-E-5	3	7200	VAV	10.8	YES
SPF-E-6	3	6000	VAV	9	YES
SPF-E-7	5	10000	VAV	15	YES
EPF-E-1	0.75	2250	VAV	3.375	YES
EPF-E-2	0.75	2250	VAV	3.375	YES
EPF-E-3	1	2500	VAV	3.75	YES
EPF-E-4	1.5	5000	VAV	7.5	YES
SF-E-1	1.5	8000	CAV	8.8	YES
EF-1W-1	5	18770	VAV	28.155	YES
EF-1W-2	0.5	1900	VAV	2.85	YES

	EF-1W-3	1	3200	VAV	4.8	YES
	EF-2W-1	3	9085	VAV	13.6275	YES
	EF-2W-2	0.75	2000	CAV	2.2	YES
	EF-7W-1	3	5000	VAV	7.5	YES
	EF-S2W-1	15	20000	VAV	30	YES
	EF-S2W-2	20	30000	VAV	45	YES
	EF-S2W-3	15	20000	VAV	30	YES
	SPF-W-1	0.75	1440	VAV	2.16	YES
ľ	SPF-W-2	1.5	3600	VAV	5.4	YES
	SPF-W-3	1.5	2900	VAV	4.35	YES
	SPF-W-4	2	4000	VAV	6	YES
	SPF-W-5	3	6700	VAV	10.05	YES
	SPF-W-6	3	6000	VAV	9	YES
	SPF-W-7	5	10000	VAV	15	YES
	EPF-W-1	0.75	2250	VAV	3.375	YES
	EPF-W-2	0.75	2250	VAV	3.375	YES
	EPF-W-3	1	2500	VAV	3.75	YES
ſ	EPF-W-4	1.5	5000	VAV	7.5	YES
ľ	EPF-W-5	2	9000	VAV	13.5	YES
ľ	EPF-W-6	1	5000	VAV	7.5	YES

# **Appendix B – Ventilation Calculations**

	Area	
Space	<b>(SF)</b>	CFM
AHU 1W-1	T	
Office Space	1410	1480
Breakroom	284	480
Storage	177	480
Evidence	1169	715
Open Office	4231	3240
Secure Files	1641	800
Office Space	813	1480
Lobby	501	1480
Secure Storage	299	2185
Office Space	2638	2185
Tellers Offices	1497	880
Closet	47	400
Security/Lobby	7535	6300
Office Space	516	350
Electrical Closet	96	1000
Comm. Closet	89	400
Corridor	1102	710
Corridor	717	1670
Breakroom	145	1670
Office Space	571	1670
Electrical Closet	118	1000
Comm. Closet	110	450
Office Space	3282	2160
Lobby	449	2160
Breakroom	205	2160
File Storage	1850	2160
Office Space	166	160
AHU 2W-1		
Courtroom	1794	2750
Courtroom	1795	2750
Courtroom	1799	2750
Courtroom	1805	2750
AHU 7W-3		
Deposition	320	400
Meeting Rooms	198	200
	SpaceAHU 1W-1Office SpaceBreakroomStorageEvidenceOpen OfficeSecure FilesOffice SpaceLobbySecure StorageOffice SpaceClosetSecurity/LobbyOffice SpaceElectrical ClosetCorridorCorridorBreakroomOffice SpaceElectrical ClosetCorridorBreakroomOffice SpaceElectrical ClosetCorridorOffice SpaceElectrical ClosetCorridorBreakroomOffice SpaceElectrical ClosetComm. ClosetOffice SpaceOffice SpaceCourtroomGoffice SpaceCourtroomCourtroomCourtroomCourtroomCourtroomDepositionMeeting Rooms	Area SpaceArea (SF)AHU 1W-1Office Space1410Breakroom284Storage177Evidence1169Open Office4231Open Office Space813Office Space813Lobby501Secure Files1641Office Space2638Tellers Offices1497Security/Lobby7535Office Space516Electrical Closet96Corridor1102Corridor1102Corridor1102Corridor1102Corridor1112Breakroom145Office Space571Breakroom145Office Space110Corridor1102Corridor1102Electrical Closet118Office Space166State110Office Space166Deposition1794Courtroom1795Courtroom1795Courtroom1795Courtroom1795Courtroom1795Deposition320Meeting Rooms198

69	Vestibule	55	50
74	Jury Room	273	250
	Corridor	390	50
71	Jury Room	262	250
68	Storage	92	50
68	Comm. Closet	101	400
66	Meeting Rooms	191	200
66	Vestibule	56	50
64	Meeting Rooms	189	200
64	Vestibule	56	50
58	Electrical Closet	111	1000
57	Storage	84	200
59	Jury Room	268	250
	Corridor	378	50
61	Jury Room	270	250
55	Meeting Rooms	197	200
55	Vestibule	54	50
53	Vestibule	58	50
53	Meeting Rooms	196	200
65	Deposition	255	515
54	Deposition	121	565
50	Comm. Closet	161	400
49	Security Office	119	50
76	Jury Room	325	350
	Corridor	391	100
79	Evidence	69	50
79	AV	26	150
77	Meeting Rooms	217	225
77	Vestibule	41	50
62	Meeting Rooms	251	225
62	Vestibule	66	50
60	AV	26	200
	Corridor	223	100
63	Evidence	79	50
63	Meeting Rooms	273	225
63	Vestibule	66	50
73	Vestibule	60	50
73	Meeting Rooms	279	225
72	Evidence	67	50
72	AV	35	200

	Corridor	222	100
75	Meeting Rooms	257	225
75	Vestibule	68	50
	Corridor	1958	350

Building		Duval	County U	nified Courthouse Faciliy									
System 1	ag/Name:	1W-1											
Operatin	g Condition Description:	ID											
Units (se	lect from pull-down list)	IP											
Inputs fo	r System	Name	Units		S	System	[						
	Floor area served by system	As	st	100% diversity	_	31658							
	Design primary supply fan airflow rate	PS Vosd	r cfm	100% diversity	_	39 825							
	OA reg'd per unit area for system (Weighted average)	Ras	cfm/sf			0.07							
	OA req'd per person for system area (Weighted average)	Rps	cfm/p			5.0							
Inputs fo	r Potentially Critical zones												
	Zone Name	Zone ti	itle turns p	urple italic for critical zone(s)			Office space	Breakroom	Storage	Evidence	Open Office	Secure Case	Office space
	Zone Tag						1W1-14	1W1-13	1W1-13	1W1-15	1W1-16	1W1-17	1W1-18
							Office space	Break rooms	Storage	Storage	Office space	Storage	Office space
	Space type		Select fr	om pull-down list					rooms	rooms		rooms	
	Floor Area of zone	Az	sf				1,410	284	177	1169	4231	1641	813
	Design population of zone	Pz	Р	(default value listed; may be ov	errido	den)	7.05	i 7.1	0	0	21.155	0	4.065
	Design total supply to zone (primary plus local recirculated)	Vdzd	cfm				1,480	480	480	715	3240	800	1480
1	Induction Terminal Unit, Dual Fan Dual Duct or Transfer Fan?	_	Select fr	om pull-down list or leave blank	if N//	Ą							
Innuts fo	Local recirc. air % representative of ave system return air	Er					75%	75%	75%	75%	75%	75%	75%
inputs 10	Percent of total design airflow rate at conditioned analyzed	Ds	%			100%	100%	100%	100%	100%	100%	100%	100%
	Air distribution type at conditioned analyzed	20	Select fr	om pull-down list	<u> </u>		CS	CS	CS	CS	CS	CS	CS
	Zone air distribution effectiveness at conditioned analyzed	Ez		•			1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Primary air fraction of supply air at conditioned analyzed	Ep											
Results		_											
	Ventilation System Efficiency	EV	afaa			0.82							
	Outdoor air make required for system	VOL Vot/As	cfm/sf			4000							
	Outdoor air per person served by system (including diversity)	Vot/Ps	cfm/n			14.8							
	Outdoor air as a % of design primary supply air	Ypd	cfm			11%							
Detailed	Calculations												
initial Ca	Primary supply air flow to system at conditioned analyzed	Vns	cfm	- VodDs	_	30825							
	UncorrectedOA requirement for system	Vou	cfm	= Rps Ps + Ras As	_	3745							
	Uncorrected OA reg'd as a fraction of primary SA	Xs	0	= Vou / Vps	=	0.09							
Initial Ca	Iculations for individual zones												
	OA rate per unit area for zone	Raz	cfm/sf				0.06	0.06	0.12	0.12	0.06	0.12	0.06
	OA rate per person	Rpz	cfm/p				5.00	5.00	0.00	0.00	5.00	0.00	5.00
	Total supply air to zone (at condition being analyzed)	Vdz	cfm				1480	480	480	715	3240	800	1480
	Unused OA req'd to breathing zone	Vbz	cfm	= Rpz Pz + Raz Az	=		119.9	52.5	21.2	140.3	359.6	196.9	69.1
	Unused UA requirement for zone	Voz	ctm	= VDZ/EZ	=		120	53	21	140	360	197	69
	Fraction of zone supply from fully mixed primary air	Fa Fb		= Ep + (I-Ep)El	=		1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Fraction of zone OA not directly recirc. from zone	Fc		$= 1 - (1 - E_z)(1 - E_p)(1 - E_r)$	_		1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Unused OA fraction required in supply air to zone	Zd		= Voz / Vdz	=		0.08	0.11	0.04	0.20	0.11	0.25	0.05
	Unused OA fraction required in primary air to zone	Zp		= Voz / Vpz	=		0.08	0.11	0.04	0.20	0.11	0.25	0.05
System \	/entilation Efficiency												
	Zone Ventilation Efficiency (App A Method)	Evz		= (Fa + FbXs - FcZ) / Fa	=		1.01	0.98	1.05	0.90	0.98	0.85	1.05
	System Ventilation Efficiency (App A Method)	Ev		= min (Evz)	=	0.82							
Minimum	Ventilation System Efficiency (Table 6.3 Method)	Ev		= Value from Table 6.3	=	0.88							
Minimum	Outdoor air Intake airflow	Vot	ofm		_	4569							
	OA intake regid as a fraction of primary SA	Y	CIIII		_	4508							
	Outdoor Air Intake Flow required to System (Table 6.3 Method)	Vot	cfm	= Vou / Ev	-	4276	291.88						
	OA intake reg'd as a fraction of primary SA (Table 6.3 Method)	Y		= Vot / Vps	=	0.11	0.06						
OA Tem	at which Min OA provides all cooling												
	OAT below which OA Intake flow is @ minimum		Deg F	= {(Tp-dTsf)-(1-Y)*(Tr+dTr	=	-76							

Building		Duval	County U	nified Courthouse Faciliy									
System 1	ag/Name:	1W-1											
Operatin	g Condition Description:												
Units (se	lect from pull-down list)	IP											
Inputs fo	r System Floor area served by system Population of area served by system (including diversity) Design primary supply fan airflow rate OA req'd per unit area for system (Weighted average) OA req'd per person for system area (Weighted average) r Potentially Critical zones	<u>Name</u> As Ps Vpsd Ras Rps	Units sf P cfm cfm/sf cfm/p	100% diversity	~	System   31658   309   39,825   0.07   5.0						Pote	ntially Critical 2
	Zone Name	_					Lobby	Secure	Office space	Tellers	Closet	Security/Lobb	Office space
	Zana Tan	Zone ti	tle turns p	ourple italic for critical zone(s)			414/4 4.0	Storage	419/4 40	Offices	419/4 04	V	41444 0
	Zone Tag						1W1-18	1W1-19 Storage	1W1-19 Office space	1W1-20	1W1-21 Storago	1W1-22 Main optry	1W1-8
	Space type		Select f	rom pull-down list			Lobbles	rooms	Office space	Office space	rooms	lobbies	Office space
	Floor Area of zone	Az	sf				501	299	2638	1497	47	7535	516
	Design population of zone	Pz	P	(default value listed; may be over	errido	den)	75.15	0	13.19	7.485	0	75.35	2.58
	Design total supply to zone (primary plus local recirculated)	Vdzd	cfm				1480	2185	2185	880	400	6300	350
	Induction Terminal Unit, Dual Fan Dual Duct or Transfer Fan?	Er	Select f	rom puil-down list or leave blank	if N//	A	750/	750/	750/	750/	750/	750/	750/
Innute fo	r Operating Condition Analyzed						15%	15%	(5%)	(5%)	/5%	75%	/5%
inputs to	Percent of total design airflow rate at conditioned analyzed	Ds	%			100%	100%	100%	100%	100%	100%	100%	100%
	Air distribution type at conditioned analyzed	20	Select f	rom pull-down list	_		CS	CS	CS	CS	CS	CS	CS
	Zone air distribution effectiveness at conditioned analyzed	Ez					1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Primary air fraction of supply air at conditioned analyzed	Ep											
Results													
	Ventilation System Efficiency	Ev				0.82							
	Outdoor air intake required for system	Vot	cfm			4568							
	Outdoor air per unit floor area	Vot/As	cfm/st			0.14							
	Outdoor air per person served by system (including diversity)	V00/PS Vpd	cfm			14.0							
	outdoor an do a 70 or doorgn primary suppry an	ipu	onn			11/0							
Detailed	Calculations												
Initial Ca	culations for the System as a whole												
	Primary supply air flow to system at conditioned analyzed	Vps	cfm	= VpdDs	=	39825							
	UncorrectedOA requirement for system	Vou	cfm	= Rps Ps + Ras As	=	3745							
Initial Ca	Uncorrected OA regid as a fraction of primary SA	Xs		= Vou / Vps	=	0.09							
initial Ca		Boz	ofm/of				0.06	0.12	0.06	0.06	0.12	0.06	0.06
	OA rate per person	Roz	cfm/p				5.00	0.12	5.00	5.00	0.12	5.00	5.00
	Total supply air to zone (at condition being analyzed)	Vdz	cfm				1480	2185	2185	880	400	6300	350
	Unused OA reg'd to breathing zone	Vbz	cfm	= Rpz Pz + Raz Az	=		405.8	35.9	224.2	127.2	5.6	828.9	43.9
	Unused OA requirement for zone	Voz	cfm	= Vbz/Ez	=		406	36	224	127	6	829	44
	Fraction of zone supply not directly recirc. from zone	Fa		= Ep + (1-Ep)Er	=		1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Fraction of zone supply from fully mixed primary air	Fb		= Ep	=		1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Fraction of zone OA not directly recirc. from zone	Fc		= 1-(1-Ez)(1-Ep)(1-Er)	=		1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Unused OA fraction required in supply air to zone	Zd		= Voz / Vdz	=		0.27	0.02	0.10	0.14	0.01	0.13	0.13
Suctor	Unused OA fraction required in primary air to zone	Zp		= Voz / Vpz	=		0.27	0.02	0.10	0.14	0.01	0.13	0.13
System	Zono Ventilation Efficiency (App & Method)	Eva			_		0.92	1.09	0.00	0.05	1.09	0.06	0.07
	System Ventilation Efficiency (App A Method)	Evz		$= \min(Fyz)$	_	0.82	0.82	1.08	0.99	0.95	1.08	0.96	0.97
	Ventilation System Efficiency (Table 6.3 Method)	Ev		= Value from Table 6.3	<u> </u>	0.88							
Minimum	outdoor air intake airflow												
	Outdoor Air Intake Flow required to System	Vot	cfm	= Vou / Ev	=	4568							
	OA intake req'd as a fraction of primary SA	Y		= Vot / Vps	=	0.11							
	Outdoor Air Intake Flow required to System (Table 6.3 Method)	Vot	cfm	= Vou / Ev	=	4276							
	OA intake req'd as a fraction of primary SA (Table 6.3 Method)	Y		= Vot / Vps	=	0.11							
OA Tem	at which Min OA provides all cooling		Deve	(/T		70							
	OAT below which OA Intake flow is @ minimum		Deg F	$= {(1p-d1st)-(1-Y)^{(1r+d1r)}}$	=	-76							

Building: System Tag/Name: Operating Condition Description:	Duval 1W-1	County U	nified Courthouse Faciliy									
Units (select from pull-down list)	IP											
Inputs for System Floor area served by system Population of area served by system (including diversity) Design primary supply fan airflow rate OA req'd per unit area for system (Weighted average) OA req'd per person for system area (Weighted average) Inputs for Potentially Critical zones	Name As Ps Vpsd Ras Rps	Units sf P cfm cfm/sf cfm/p	100% diversity	5	System   31658   309   39,825   0.07   5.0	ones						
Zone Name	_					Elect. Closet	Comm.	Corridor	Corridor	Breakroom	Office space	Elect. Closet
Zone Tag	Zone ti	itle turns p	urple italic for critical zone(s)			1W1-11	Closet	1W1-10	1W1-7	1W1-7	1W1-7	1W1-6
Zono rug						Electrical	Telephone	Corridors	Corridors	Break rooms	Office space	Electrical
Space type		Select f	rom pull-down list			equipment rooms	closets					equipment rooms
Floor Area of zone	Az D7	st	(default value listed; may be av	orrida	lon)	96	89	1102	717	145	571	118
Design population of zone (primary plus local recirculated)	PZ Vdzd	r cfm	(default value listed; may be ove	emac	ien)	1000	400	710	1670	3.625	2.800	1000
Induction Terminal Unit. Dual Fan Dual Duct or Transfer Fan?	Vuzu	Select f	om pull-down list or leave blank	if N/A	Ą	1000	400	710	1070	1070	1070	1000
Local recirc. air % representative of ave system return air	Er		••••••			75%	75%	75%	75%	75%	75%	75%
Inputs for Operating Condition Analyzed				_								
Percent of total design airflow rate at conditioned analyzed	Ds	%			100%	100%	100%	100%	100%	100%	100%	100%
Air distribution type at conditioned analyzed	<b>F</b> -	Select f	om pull-down list			CS 1.00	CS	CS	CS	CS	CS	CS
Zone all distribution effectiveness at conditioned analyzed	EZ					1.00	1.00	1.00	1.00	1.00	1.00	1.00
Results	∟р											
Outdoor air intake required for system Outdoor air per unit floor area Outdoor air per person served by system (including diversity) Outdoor air as a % of design primary supply air	Vot Vot/As Vot/Ps Ypd	cfm cfm/sf cfm/p cfm			4568 0.14 14.8 11%							
Detailed Calculations												
Primary supply air flow to system at conditioned analyzed	Vps	cfm	= VpdDs	=	39825							
UncorrectedOA requirement for system	Vou	cfm	= Rps Ps + Ras As	=	3745							
Uncorrected OA req'd as a fraction of primary SA Initial Calculations for individual zones	Xs		= Vou / Vps	=	0.09							
OA rate per unit area for zone	Raz	cfm/sf				0.06	0.00	0.06	0.06	0.06	0.06	0.06
OA rate per person	Rpz	cfm/p				0.00	0.00	0.00	0.00	5.00	5.00	0.00
Total supply air to zone (at condition being analyzed)	Vdz	cfm				1000	400	710	1670	1670	1670	1000
Unused OA requirement for zone	VDZ	cim	= Kpz Pz + Kaz Az	=		5.8	0.0	66.1	43.0	26.8	48.5	7.1
Fraction of zone supply not directly recirc, from zone	Fa	CIIII	= VD2/L2 = Ep + (1-Ep)Er	_		1.00	1 00	1 00	1 00	1.00	1 00	1 00
Fraction of zone supply from fully mixed primary air	Fb		= Ep	_		1.00	1.00	1.00	1.00	1.00	1.00	1.00
Fraction of zone OA not directly recirc. from zone	Fc		= 1-(1-Ez)(1-Ep)(1-Er)	=		1.00	1.00	1.00	1.00	1.00	1.00	1.00
Unused OA fraction required in supply air to zone	Zd		= Voz / Vdz	=		0.01	0.00	0.09	0.03	0.02	0.03	0.01
Unused OA fraction required in primary air to zone	Zp		= Voz / Vpz	=		0.01	0.00	0.09	0.03	0.02	0.03	0.01
System Ventilation Efficiency	E.e.					1.00	1.00	1.00	1.07	1.00	1.00	1.00
System Ventilation Efficiency (App A Method)	Evz Ev		= (ra + rbs - rcz)/ra $= min (Fvz)$	=	0.82	1.09	1.09	1.00	1.07	1.00	1.00	1.09
Ventilation System Efficiency (Table 6.3 Method)	Ev		= Value from Table 6.3	=	0.88							
Minimum outdoor air intake airflow												
Outdoor Air Intake Flow required to System	Vot	cfm	= Vou / Ev	=	4568							
OA intake req'd as a fraction of primary SA	Y		= Vot / Vps	=	0.11							
Outdoor Air Intake Flow required to System (Table 6.3 Method	) Vot	ctm	= Vou / Ev	=	4276							
OA intake requias a fraction of primary SA (Table 6.3 Method) OA Temp at which Min OA provides all cooling	T		= vot / vps	=	0.11							
OAT below which OA Intake flow is @ minimum		Deg F	= {(Tp-dTsf)-(1-Y)*(Tr+dTr	=	-76							

Building		Duval (	County L	Jnifie	d Courthouse Faciliy								
System 1	ag/Name:	1W-1											
Operatin	g Condition Description:												
Units (se	lect from pull-down list)	IP											
Inputs fo	r System	Name	Units				System	[					
	Floor area served by system	As	sf		4000/ disconsites	_	31658						
	Population of area served by system (including diversity)	PS Vood	P		100% diversity	_	309						
	OA regid per unit area for system (Weighted average)	Ras	cfm/sf			_	0.07						
	OA req'd per person for system area (Weighted average)	Rps	cfm/p				5.0						
Inputs fo	r Potentially Critical zones	•	•			-							
	Zone Name	-			and the second second			Comm.	Office space	Lobby	Breakroom	File Storage	Office space
	Zono Tag	Zone til	le turns	ourple	e italic for critical zone(s)			Closet	11/0/1_4	110/1 4	11/1/1 /	110/1 4	11/1/1_1
	Zone rag							Telephone	Office space	Lobbies	Break rooms	Storage	Office space
	Space type							closets	onice space	LODDICS	Dicukrooms	rooms	onice space
			Select	rom p	oull-down list								
	Floor Area of zone	Az	sf					110	3282	449	205	1850	166
	Design population of zone	Pz	P	(def	ault value listed; may be o	/erride	den)	0	16.41	67.35	5.125	0	0.83
	Induction Terminal Unit, Dual Fan Dual Duct or Transfer Fan?	vuzu	Select	rom r	oull-down list or leave blan	k if N/	А	450	2160	2160	2160	2160	160
	Local recirc. air % representative of ave system return air	Er	001000	10111			n i	75%	75%	75%	75%	75%	75%
Inputs fo	r Operating Condition Analyzed												
	Percent of total design airflow rate at conditioned analyzed	Ds	%				100%	100%	100%	100%	100%	100%	100%
	Air distribution type at conditioned analyzed	-	Select	rom p	oull-down list			CS	CS	CS	CS	CS	CS
	Zone air distribution effectiveness at conditioned analyzed	EZ					l	1.00	1.00	1.00	1.00	1.00	1.00
Results	Filmary an maction of supply an at conditioned analyzed	цρ							11				
	Ventilation System Efficiency	Ev					0.82						
	Outdoor air intake required for system	Vot	cfm				4568						
	Outdoor air per unit floor area	Vot/As	cfm/sf				0.14						
	Outdoor air per person served by system (including diversity)	Vot/Ps	cfm/p				14.8						
	Outdoor air as a % of design primary supply air	тра	cim				11%						
Detailed	Calculations												
Initial Ca	culations for the System as a whole												
	Primary supply air flow to system at conditioned analyzed	Vps	cfm	=	VpdDs	=	39825						
	Uncorrected OA regulation of primary SA	Vou	cfm	=	Rps Ps + Ras As	=	3745						
Initial Ca	culations for individual zones	A5		=	vou/vps	=	0.09						
	OA rate per unit area for zone	Raz	cfm/sf					0.00	0.06	0.06	0.06	0.12	0.06
	OA rate per person	Rpz	cfm/p					0.00	5.00	5.00	5.00	0.00	5.00
	Total supply air to zone (at condition being analyzed)	Vdz	cfm					450	2160	2160	2160	2160	160
	Unused OA req'd to breathing zone	Vbz	cfm	=	Rpz Pz + Raz Az	=		0.0	279.0	363.7	37.9	222.0	14.1
	Unused OA requirement for zone	Voz	cfm	=	Vbz/Ez	=		0	279	364	38	222	14
	Fraction of zone supply not directly recirc. from zone	Fa		=	Ep + (1-Ep)Er	=		1.00	1.00	1.00	1.00	1.00	1.00
	Fraction of zone supply from fully mixed primary air	FD		=	Ep 1 (1 $E_7$ )(1 $E_7$ )(1 $E_7$ )	=		1.00	1.00	1.00	1.00	1.00	1.00
	Linused OA fraction required in supply air to zone	7d		=	$V_{02} / V_{02}$	_		0.00	0.13	0.17	0.02	0.10	0.00
	Unused OA fraction required in supply an to zone	Zp		_	Voz / Voz	_		0.00	0.13	0.17	0.02	0.10	0.09
System \	entilation Efficiency							1.00					1.50
	Zone Ventilation Efficiency (App A Method)	Evz		=	(Fa + FbXs - FcZ) / Fa	=		1.09	0.96	0.93	1.08	0.99	1.01
	System Ventilation Efficiency (App A Method)	Ev		=	min (Evz)	=	0.82						
Minim	Ventilation System Efficiency (Table 6.3 Method)	Ev		=	Value from Table 6.3	=	0.88						
winimum	Outdoor Air Intake Airnow	Vot	cfm	_	Vou / Ev	_	4569						
	OA intake regid as a fraction of primary SA	Y	CIIII	_	Vot / Vos	_	0.11						
	Outdoor Air Intake Flow required to System (Table 6.3 Method)	Vot	cfm	=	Vou / Ev	=	4276						
	OA intake req'd as a fraction of primary SA (Table 6.3 Method)	Y		=	Vot / Vps	=	0.11						
OA Temp	at which Min OA provides all cooling		_										
	OAT below which OA Intake flow is @ minimum		Deg F	=	{(Tp-dTsf)-(1-Y)*(Tr+dTr	=	-76						

Building: System Tag/Name:	Duval 0 2W-1	County L	Inifie	d Courthouse Faciliy						
Operating Condition Description:	ID.									
Units (select from pull-down list)	IP									
Inputs for System Floor area served by system Population of area served by system (including diversity) Design primary supply fan airflow rate OA req'd per unit area for system (Weighted average) OA req'd per person for system area (Weighted average) Inputs for Potentially Critical zones	<u>Name</u> As Ps Vpsd Ras Rps	<u>Units</u> sf Cfm cfm/sf cfm/p		100% diversity		System 7193 504 11,000 0.06 5.0		Potentially (	ritical Zones	
Zone Name	Zone tit	tle turns i	ouroli	e italic for critical zone(s)			Courtroom	Courtroom	Courtroom	Courtroom
	20/10 11		Juiph				2W1-1.2W1-	2W1-13.2W1-	2W1-14.2W1-	2W1-15.2W1-
Zone Tag							12	2	3	3
Space type		Select f	rom	oull-down list			Courtrooms	Courtrooms	Courtrooms	Courtrooms
Floor Area of zone	Az	sf					1,794	1795	1799	1805
Design population of zone	Pz	P	(def	ault value listed; may be ov	/errid	den)	125.58	125.65	125.93	126.35
Design total supply to zone (primary plus local recirculated)	Vdzd	cfm					2,750	2750	2750	2750
Induction Terminal Unit, Dual Fan Dual Duct or Transfer Fan?	-	Select f	rom	pull-down list or leave blank	k if N/	A	750/	750/	750/	750/
Local recirc. air % representative of ave system return air	Er						75%	75%	75%	75%
Inputs for Operating Condition Analyzed	Do	0/				100%	100%	100%	100%	100%
Air distribution type at conditioned analyzed	05	70 Soloct f	rom	oull-down list		100%	00%			
Zone air distribution effectiveness at conditioned analyzed	Fz	Oelecti	ioiii	Sul-down list			1.00	1 00	1.00	1.00
Primary air fraction of supply air at conditioned analyzed	Ep						1.00	1.00	1.00	1.00
Results	-r									J
Ventilation System Efficiency	Ev					1.00				
Outdoor air intake required for system	Vot	cfm				2952				
Outdoor air per unit floor area	Vot/As	cfm/sf				0.41				
Outdoor air per person served by system (including diversity)	Vot/Ps	cfm/p				5.9				
Outdoor air as a % of design primary supply air	Ypd	cfm				27%				
Detailed Calculations										
Drimony supply of flow to system as a whole	Vno	ofm	_	VindDa	_	11000				
LincorrectedOA requirement for system	Vou	cfm	=	$P_{DS} = P_{S} + P_{SS} \Delta_{S}$	_	20/0				
Uncorrected OA regid as a fraction of primary SA	Xs	CIIII	_	Vou / Vos	_	0.27				
Initial Calculations for individual zones	7.0			100,100		0.27				
OA rate per unit area for zone	Raz	cfm/sf					0.06	0.06	0.06	0.06
OA rate per person	Rpz	cfm/p					5.00	5.00	5.00	5.00
Total supply air to zone (at condition being analyzed)	Vdz	cfm .					2750	2750	2750	2750
Unused OA req'd to breathing zone	Vbz	cfm	=	Rpz Pz + Raz Az	=		735.5	736.0	737.6	740.1
Unused OA requirement for zone	Voz	cfm	=	Vbz/Ez	=		736	736	738	740
Fraction of zone supply not directly recirc. from zone	Fa		=	Ep + (1-Ep)Er	=		1.00	1.00	1.00	1.00
Fraction of zone supply from fully mixed primary air	Fb		=	Ep	=		1.00	1.00	1.00	1.00
Fraction of zone OA not directly recirc. from zone	Fc		=	1-(1-Ez)(1-Ep)(1-Er)	=		1.00	1.00	1.00	1.00
Unused OA fraction required in supply air to zone	Zd		=	Voz / Vdz	=		0.27	0.27	0.27	0.27
Unused OA traction required in primary air to zone	Zp		=	voz / Vpz	=		0.27	0.27	0.27	0.27
System ventilation Efficiency	<b>F.</b>						1.00	1.00	1.00	1.00
System Ventilation Efficiency (App A Method)	EVZ		=	(Fa + FDAS - FCZ) / Fa min (Evz)	=	1.00	1.00	1.00	1.00	1.00
Ventilation System Efficiency (App A Method)	Ev		-	Value from Table 6.3	=	0.88				
Minimum outdoor air intake airflow	2.0		_	value nom rable 0.5	-	0.00				
Outdoor Air Intake Flow required to System	Vot	cfm	=	Vou / Ev	=	2952				
OA intake reg'd as a fraction of primary SA	Y	0111	=	Vot / Vps	=	0.27				
Outdoor Air Intake Flow required to System (Table 6.3 Method	Vot	cfm	=	Vou / Ev	=	3348				
OA intake reg'd as a fraction of primary SA (Table 6.3 Method)	Y		=	Vot / Vps	=	0.30				
OA Temp at which Min OA provides all cooling										
OAT below which OA Intake flow is @ minimum		Deg F	=	{(Tp-dTsf)-(1-Y)*(Tr+dTr	=	9				

Building		Duval	County U	nified Courthouse Faciliy									
System 7	Fag/Name:	7W-3											
Operatin	g Condition Description:	ID											
Units (se	lect from pull-down list)	IP											
Inputs fo	r System	Name	Units		Syste	em							
	Floor area served by system	As	sf	100% divorcity	9,4	454							
	Design primary supply fan airflow rate	PS Vosd	r cfm	100% diversity	9	255							
	OA reg'd per unit area for system (Weighted average)	Ras	cfm/sf		0,1	0.06							
	OA req'd per person for system area (Weighted average)	Rps	cfm/p			5.0							
Inputs fo	r Potentially Critical zones										<b>•</b> • •		C.
	Zone Name	Zone ti	itle turns p	urple italic for critical zone(s)			Deposition	Meeting Rooms	Vestibule	Jury room	Corridor	Jury Room	Storage
	Zone Tag					F	7W3-70	7W3-69	7W3-69	7W3-74	Considere	7W3-71	7W3-68
	Space type						eeting	eeting	corridors	eeting	Contuors	eeting	rooms
		<b>A</b> –	Select fi	om pull-down list		-		400		070		000	
	Floor Area of zone	AZ D7	ST	(default value listed; may be eve	orriddon)	-	320	198	55	2/3	390	262	92
	Design population of zone (primary plus local recirculated)	PZ Vdzd	r cfm	(default value listed; may be ove	ernaden)	-	10	9.9	250	13.00	50	250	50
1	Induction Terminal Unit. Dual Fan Dual Duct or Transfer Fan?	vuzu	Select fi	om pull-down list or leave blank	if N/A	ŀ	400	230	230	230	50	230	50
1	Local recirc. air % representative of ave system return air	Er		,		ł	75%	75%	75%	75%	75%	75%	75%
Inputs fo	r Operating Condition Analyzed												
	Percent of total design airflow rate at conditioned analyzed	Ds	%		10	0%	100%	100%	100%	100%	100%	100%	100%
	Air distribution type at conditioned analyzed	_	Select fr	om pull-down list			CS	CS	CS	CS	CS	CS	CS
	Zone air distribution effectiveness at conditioned analyzed	Ez				-	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Results	Primary air fraction of supply air at conditioned analyzed	Ер											
Results	Ventilation System Efficiency	Fv			0.	71							
	Outdoor air intake required for system	Vot	cfm		23	37							
	Outdoor air per unit floor area	Vot/As	cfm/sf		0.	25							
	Outdoor air per person served by system (including diversity)	Vot/Ps	cfm/p		10	0.7							
	Outdoor air as a % of design primary supply air	Ypd	cfm		2	25%							
Detailed	Calculations												
Initial Ca	Iculations for the System as a whole												
	Primary supply air flow to system at conditioned analyzed	Vps	cfm	= VpdDs	= 92	255							
	UncorrectedOA requirement for system	Vou	cfm	= Rps Ps + Ras As	= 10	663							
	Uncorrected OA req'd as a fraction of primary SA	Xs		= Vou / Vps	= 0	).18							
Initial Ca	Iculations for individual zones	_											
	OA rate per unit area for zone	Raz	cfm/sf				0.06	0.06	0.06	0.06	0.06	0.06	0.12
	OA rate per person	Rpz	ctm/p				5.00	5.00	0.00	5.00	0.00	5.00	0.00
	Linused OA regid to breathing zone	Vuz Vhz	cfm	- Roz Pz + Raz Az	-		400	250	250	250	23.4	∠50 81.2	50
	Unused OA requirement for zone	Voz	cfm	= Vbz/Ez	_		99	61	3.5	85	23.4	81	11.0
	Fraction of zone supply not directly recirc. from zone	Fa	5	= Ep + (1-Ep)Er	=		1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Fraction of zone supply from fully mixed primary air	Fb		= Ep	=		1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Fraction of zone OA not directly recirc. from zone	Fc		= 1-(1-Ez)(1-Ep)(1-Er)	=		1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Unused OA fraction required in supply air to zone	Zd		= Voz / Vdz	=		0.25	0.25	0.01	0.34	0.47	0.32	0.22
0	Unused OA fraction required in primary air to zone	Zp		= Voz / Vpz	=		0.25	0.25	0.01	0.34	0.47	0.32	0.22
System	Zene Ventilation Efficiency (Ann A Method)	<b>E</b>					0.02	0.02	4 47	0.04	0.74	0.05	0.00
	System Ventilation Efficiency (App A Method)	Ev2 Ev		= (ra + rbAs - rcz) / ra $= min (Fvz)$	- 0	71	0.93	0.93	1.17	0.84	0.71	0.85	0.96
	Ventilation System Efficiency (Table 6.3 Method)	Ev		= Value from Table 6.3	= 0.	68							
Minimun	outdoor air intake airflow												
	Outdoor Air Intake Flow required to System	Vot	cfm	= Vou / Ev	= 23	337							
	OA intake req'd as a fraction of primary SA	Y		= Vot / Vps	= 0	.25							
	Outdoor Air Intake Flow required to System (Table 6.3 Method)	Vot	cfm	= Vou / Ev	= 24	439							
04 T-	OA intake req'd as a fraction of primary SA (Table 6.3 Method)	Y		= Vot / Vps	= 0	).26							
OA Tem	OAT below which OA lotake flow is @ minimum		Dec E	- //Tn-dTef)//1-V)*/Tr+dTr	_	5							
	OAT BEIOW WHICH OA III.ake now is the minimulf		Degi		-	J							

Building:	Du	uval C	ounty Ur	ified Courthouse Faciliy									
System Tag/Name:	71	W-3											
Units (select from pull-down list)	IP	<b>,</b>											
Inputs for System	Na	lame	<u>Units</u>		S	/stem							
Floor area served by system Population of area served by system (includ	ing diversity) Ps	IS Ic	ST P	100% diversity		9,454							
Design primary supply fan airflow rate	Vr	s bsd	cfm	loonal diversity		9.255							
OA req'd per unit area for system (Weighted	laverage) Ra	las	cfm/sf			0.06							
OA req'd per person for system area (Weig	hted average) Rp	lps	cfm/p			5.0							
Inputs for Potentially Critical zones													
Zone Name	Zo	one titl	le turns pl	Irple italic for critical zone(s)			Comm. Closet	Meeting rooms	Vestibule	Meeting Rooms	Vestibule	Elect. Closet	Storage
Zone Tag							7W3-68	7W3-66	7W3-66	7W3-64	7W3-64	7W3-58	7W3-57
Space time							Telephone	Conference/m	Corridors	Conference/m	Corridors	Electrical	Storage
Space type			Select fro	om pull-down list			closets	eeting		eeting		rooms	rooms
Floor Area of zone	Az	z	sf	•••••			101	191	56	189	56	111	84
Design population of zone	Pz	z	P	default value listed; may be over	erridde	en)	0	9.55	0	9.45	0	0	0
Design total supply to zone (primary plus loo	cal recirculated) Vo	'dzd	cfm			_	400	200	50	200	50	1000	200
Induction Terminal Unit, Dual Fan Dual Duc	t or Transfer Fan?		Select fro	om pull-down list or leave blank	if N/A	Ļ	750/	750/	750/	750/	350/	750/	750/
Local recirc. air % representative of ave sys	tem return air Er	1					15%	75%	75%	75%	(5%	75%	(5%
Percent of total design airflow rate at condition	oned analyzed De	s	%			100%	100%	100%	100%	100%	100%	100%	100%
Air distribution type at conditioned analyzed			Select fro	om pull-down list			CS	CS	CS	CS	CS	CS	CS
Zone air distribution effectiveness at condition	oned analyzed Ez	z				[	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Primary air fraction of supply air at condition	ed analyzed Ep	р											
Kesults Vontilation System Efficiency	E,					0 71							
Outdoor air intake required for system	Vo	ot.	cfm			2337							
Outdoor air per unit floor area	Vo	ot/As	cfm/sf			0.25							
Outdoor air per person served by system (in	cluding diversity) Vo	ot/Ps	cfm/p			10.7							
Outdoor air as a % of design primary supply	air Yr	pd	cfm			25%							
Detailed Calculations													
Initial Calculations for the System as a whole													
Primary supply air flow to system at conditio	ned analvzed Vr	bs	cfm	= VpdDs	=	9255							
UncorrectedOA requirement for system	Vo	ou	cfm	= Rps Ps + Ras As	=	1663							
Uncorrected OA req'd as a fraction of prima	ry SA Xs	s		= Vou / Vps	=	0.18							
Initial Calculations for individual zones													
OA rate per unit area for zone	Ra	laz	cfm/sf				0.00	0.06	0.06	0.06	0.06	0.06	0.12
OA rate per person	Rp (	lpz lala	cfm/p				0.00	5.00	0.00	5.00	0.00	0.00	0.00
Linused OA regid to breathing zono	anaiyzeu) Vo	uz 'hz	cfm	- Rnz Pz + Raz Az	_		400	200	50	200	50	67	200
Unused OA requirement for zone	Vi	OZ	cfm	= Vbz/Ez	=		0.0	59	3.4	59	3.4	0.7	10.1
Fraction of zone supply not directly recirc. fr	om zone Fa	a		= Ep + (1-Ep)Er	=		1.00	1.00	1.00	1.00	1.00	1.00	1.00
Fraction of zone supply from fully mixed prin	nary air Fb	b		= Ep	=		1.00	1.00	1.00	1.00	1.00	1.00	1.00
Fraction of zone OA not directly recirc. from	zone Fo	c		= 1-(1-Ez)(1-Ep)(1-Er)	=		1.00	1.00	1.00	1.00	1.00	1.00	1.00
Unused OA fraction required in supply air to	zone Zo	d		= Voz / Vdz	=		0.00	0.30	0.07	0.29	0.07	0.01	0.05
Unused OA fraction required in primary air t	o zone Zp	p		= Voz / Vpz	=		0.00	0.30	0.07	0.29	0.07	0.01	0.05
Zono Ventilation Efficiency (App A Method)	E,	1/7		- (Eq. + EbYe - Ec7) / Eq.			1 10	0.00	1 1 1	0.00	1 1 1	1 17	1 1 2
System Ventilation Efficiency (App A Method)	d) Ev	V		= (i a + i b/s - rcz) / ra = min (Evz)	=	0.71	1.18	0.88	1.11	0.89	1.11	1.17	1.13
Ventilation System Efficiency (Table 6.3 Me	thod) Ev	v		= Value from Table 6.3	=	0.68							
Minimum outdoor air intake airflow													
Outdoor Air Intake Flow required to System	Vo	'ot	cfm	= Vou / Ev	=	2337							
OA intake req'd as a fraction of primary SA	Y			= Vot / Vps	=	0.25							
Outdoor Air Intake Flow required to System	(Table 6.3 Method) Vo	ot	cfm	= Vou / Ev	=	2439							
OA Intake req d as a fraction of primary SA	Table 6.3 Method) Y			= vot / vps	=	0.26							
OAT below which OA Intake flow is @ minin	num		Deg F	= {(Tp-dTsf)-(1-Y)*(Tr+dTr	=	5							

Building		Duval	County U	nified Courthouse Faciliy									
System 1	ag/Name:	7W-3											
Operatin	g Condition Description:	10				_							
Units (se	lect from pull-down list)	IP											
Inputs fo	r System	Name	<u>Units</u>		Syste	m							
	Floor area served by system Population of area served by system (including diversity)	As Pc	ST D	100% divorsity	9,4	54							
	Design primary supply fan airflow rate	Vosd	cfm		92	255							
	OA req'd per unit area for system (Weighted average)	Ras	cfm/sf		0.	.06							
	OA req'd per person for system area (Weighted average)	Rps	cfm/p		ę	5.0							
Inputs fo	r Potentially Critical zones											•	
	Zone Name	Zone ti	itle turns p	ourple italic for critical zone(s)			Jury room	Corridor	Jury Room	Meeting rooms	Vestibule	Meeting Rooms	Vestibule
	Zone Tag						7W3-59		7W3-61	7W3-55	7W3-55	7W3-53	7W3-53
						C	Conference/m	Corridors	Conference/m	Conference/m	Corridors	Conference/m	Corridors
	Space type		Select f	rom pull-down list			eeting		eeting	eeting		eeting	
	Floor Area of zone	Az	sf				268	378	270	197	54	196	58
1	Design population of zone	Pz	Р	(default value listed; may be ov	erridden)		13.4	0	13.5	9.85	0	9.8	0
1	Design total supply to zone (primary plus local recirculated)	Vdzd	cfm				250	50	250	200	50	200	50
1	Induction Terminal Unit, Dual Fan Dual Duct or Transfer Fan?	<b>F</b> -	Select f	rom pull-down list or leave blank	it N/A	Ļ	7501	750/	750/	750/			750/
Innuts fo	Local redirc. air % representative of ave system return air	Εſ					75%	75%	75%	/5%	/5%	/5%	/5%
inputato	Percent of total design airflow rate at conditioned analyzed	Ds	%		100	)%	100%	100%	100%	100%	100%	100%	100%
	Air distribution type at conditioned analyzed		Select f	rom pull-down list			CS	CS	CS	CS	CS	CS	CS
	Zone air distribution effectiveness at conditioned analyzed	Ez					1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Primary air fraction of supply air at conditioned analyzed	Ep											
Results		-											
	Ventilation System Efficiency	EV	afaa		0./	/1 7							
	Outdoor air intake required for system	VOL Vot/As	cfm/sf		233	57 25							
	Outdoor air per person served by system (including diversity)	Vot/Ps	cfm/p		10	.7							
	Outdoor air as a % of design primary supply air	Ypd	cfm		25	5%							
		-											
Detailed	Calculations												
initial Ca	Primary supply air flow to system at conditioned analyzed	Vns	cfm	– VodDe	- 02	55							
	UncorrectedOA requirement for system	Vou	cfm	= Rps Ps + Ras As	= 16	63							
	Uncorrected OA reg'd as a fraction of primary SA	Xs	0	= Vou / Vps	= 0.	.18							
Initial Ca	Iculations for individual zones												
	OA rate per unit area for zone	Raz	cfm/sf				0.06	0.06	0.06	0.06	0.06	0.06	0.06
	OA rate per person	Rpz	cfm/p				5.00	0.00	5.00	5.00	0.00	5.00	0.00
	Total supply air to zone (at condition being analyzed)	Vdz	cfm				250	50	250	200	50	200	50
	Unused OA requirement for any	Vbz	ctm	= Rpz Pz + Raz Az	=		83.1	22.7	83.7	61.1	3.2	60.8	3.5
	Unused UA requirement for zone	Voz	ctm	= VDZ/EZ	=		83	23	84	61	3	61	3
	Fraction of zone supply from fully mixed primary air	Fa Fb		= Ep + (1-Ep)El	=		1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Fraction of zone OA not directly recirc. from zone	Fc		$= 1 - (1 - E_z)(1 - E_p)(1 - E_r)$	_		1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Unused OA fraction required in supply air to zone	Zd		= Voz / Vdz	=		0.33	0.45	0.33	0.31	0.06	0.30	0.07
	Unused OA fraction required in primary air to zone	Zp		= Voz / Vpz	=		0.33	0.45	0.33	0.31	0.06	0.30	0.07
System \	/entilation Efficiency												
	Zone Ventilation Efficiency (App A Method)	Evz		= (Fa + FbXs - FcZ) / Fa	=		0.85	0.73	0.84	0.87	1.11	0.88	1.11
	System Ventilation Efficiency (App A Method)	Ev		= min (Evz)	= 0.7	71							
Minder	Ventilation System Efficiency (Table 6.3 Method)	Ev		= Value from Table 6.3	= 0.6	58							
Minimum	Outdoor air Intake airflow	Vot	ofm		- 00	37							
	OA intake regid as a fraction of primary SA	Y	cim	= Vot / Vos	- 23	25							
	Outdoor Air Intake Flow required to System (Table 6.3 Method)	Vot	cfm	= Vou / Ev	= 24	39							
	OA intake reg'd as a fraction of primary SA (Table 6.3 Method)	Y		= Vot / Vps	= 0.	.26							
OA Temp	at which Min OA provides all cooling												
	OAT below which OA Intake flow is @ minimum		Deg F	= {(Tp-dTsf)-(1-Y)*(Tr+dTr	=	5							

Building	•	Duval	County U	nified Courthouse Faciliy								
System 1	Γαα/Name:	7W-3	oounty o			1						
Operatin	g Condition Description:											
Units (se	lect from pull-down list)	IP										
Inputs fo	r System	Name	<u>Units</u>		Systen	1						
	Floor area served by system	As	sf		9,45	4						
	Population of area served by system (including diversity)	Ps	P	100% diversity	21	8						
	Design primary supply fan airflow rate	Vpsd	cfm		9,25	5						
	OA req'd per unit area for system (Weighted average)	Ras	ctm/st		0.0	6						
	OA regid per person for system area (Weighted average)	Rps	ctm/p		5	0	Determination (					
inputs to	r Potentially Critical zones					den estiten	Potentially C	ritical Zones	O a sourites	In the second second	O a mai d a m	Feddamaa
	Zone Name	Zone ti	itla turns r	urple italic for critical zone(s)		deposition	Deposition	Comm.	Security	Jury room	Corridor	Evidence
	Zone Tag	20110 11	ue turns p			71/2-65	7\\\/2_54	7W2-50	7W2-49	7\\/2_76		7\/2_70
	Zone rag					Conference/	m Conference/m	Telephone	Office space	Conference/m	Corridors	Storage
	Space type					eeting	eeting	closets	Once space	eeting	Contuors	rooms
	opade type		Select f	om pull-down list		cetting	coung	0103613		coung		rooms
	Floor Area of zone	Az	sf			25	5 121	161	119	325	391	69
	Design population of zone	Pz	P	(default value listed: may be over	rridden)	12.7	6.05	0	0.595	16.25	0	0
	Design total supply to zone (primary plus local recirculated)	Vdzd	cfm		,	51	5 565	400	50	350	100	50
	Induction Terminal Unit, Dual Fan Dual Duct or Transfer Fan?		Select f	om pull-down list or leave blank	if N/A							
	Local recirc. air % representative of ave system return air	Er				759	% 75%	75%	75%	75%	75%	75%
Inputs fo	r Operating Condition Analyzed											
	Percent of total design airflow rate at conditioned analyzed	Ds	%		100	<mark>ا 100</mark>	% 100%	100%	100%	100%	100%	100%
	Air distribution type at conditioned analyzed		Select f	om pull-down list		C	S CS	CS	CS	CS	CS	CS
	Zone air distribution effectiveness at conditioned analyzed	Ez				1.0	0 1.00	1.00	1.00	1.00	1.00	1.00
	Primary air fraction of supply air at conditioned analyzed	Ep										
Results		_										
	Ventilation System Efficiency	Ev	,		0.7	-						
	Outdoor air intake required for system	Vot	ctm		233	-						
	Outdoor air per unit floor area	Vot/As	ctm/st		0.2							
	Outdoor air per person served by system (including diversity)	Vot/Ps	ctm/p		10.	, ,						
	Outdoor air as a % of design primary supply air	үра	ctm		25	/o						
Detailed	Calculations											
Initial Ca	Iculations for the System as a whole											
initial Od	Primary supply air flow to system at conditioned analyzed	Vns	cfm	- VodDs	- 925	5						
	UncorrectedOA requirement for system	Vou	cfm	= Rps Ps + Ras As	= 166	3						
	Uncorrected OA regid as a fraction of primary SA	Xs	onn	$= V_{01}/V_{DS}$	= 0.1	8						
Initial Ca	Iculations for individual zones					-						
	OA rate per unit area for zone	Raz	cfm/sf			0.0	0.06	0.00	0.06	0.06	0.06	0.12
	OA rate per person	Rpz	cfm/p			5.0	0 5.00	0.00	5.00	5.00	0.00	0.00
	Total supply air to zone (at condition being analyzed)	Vdz	cfm			51	5 565	400	50	350	100	50
	Unused OA reg'd to breathing zone	Vbz	cfm	= Rpz Pz + Raz Az	=	79.	.1 37.5	0.0	10.1	100.8	23.5	8.3
	Unused OA requirement for zone	Voz	cfm	= Vbz/Ez	=	7	9 38	0	10	101	23	8
	Fraction of zone supply not directly recirc. from zone	Fa		= Ep + (1-Ep)Er	=	1.0	0 1.00	1.00	1.00	1.00	1.00	1.00
	Fraction of zone supply from fully mixed primary air	Fb		= Ep	=	1.0	0 1.00	1.00	1.00	1.00	1.00	1.00
	Fraction of zone OA not directly recirc. from zone	Fc		= 1-(1-Ez)(1-Ep)(1-Er)	=	1.0	0 1.00	1.00	1.00	1.00	1.00	1.00
	Unused OA fraction required in supply air to zone	Zd		= Voz / Vdz	=	0.1	5 0.07	0.00	0.20	0.29	0.23	0.17
	Unused OA fraction required in primary air to zone	Zp		= Voz / Vpz	=	0.1	5 0.07	0.00	0.20	0.29	0.23	0.17
System V	/entilation Efficiency											
	Zone Ventilation Efficiency (App A Method)	Evz		= (Fa + FbXs - FcZ) / Fa	=	1.0	3 1.11	1.18	0.98	0.89	0.95	1.01
	System Ventilation Efficiency (App A Method)	Ev		= min (Evz)	= 0.7							
	Ventilation System Efficiency (Table 6.3 Method)	Ev		= Value from Table 6.3	= 0.6	3						
Minimum	outdoor air intake airflow											
	Outdoor Air Intake Flow required to System	Vot	cfm	= Vou / Ev	= 233	7						
	OA intake req'd as a fraction of primary SA	Y		= Vot / Vps	= 0.2	5						
	Outdoor Air Intake Flow required to System (Table 6.3 Method)	Vot	cfm	= Vou / Ev	= 243	9						
	OA intake req'd as a fraction of primary SA (Table 6.3 Method)	Y		= Vot / Vps	= 0.2	6						
OA Tem	o at which Min OA provides all cooling					_						
	OAT below which OA Intake flow is @ minimum		Deg F	= {(Ip-d1st)-(1-Y)*(Ir+dTr	=	5						

Building:		Duval	County U	nified Courthouse Faciliy									
System Ta	ng/Name:	7W-3											
Uperating	Condition Description: act from null-down list)	IP											
01110 (001													
Inputs for	System Floor area served by system	Name	Units of		Sys	stem							
	Population of area served by system (including diversity)	Ps	P	100% diversity		218							
	Design primary supply fan airflow rate	Vpsd	cfm			9,255							
	OA req'd per unit area for system (Weighted average)	Ras	cfm/sf			0.06							
	OA req'd per person for system area (Weighted average)	Rps	cfm/p			5.0							
Inputs for	Potentially Critical zones					Г	A.V/	Masting	Veetikule	Maating	Veetikule	A\/	Considere
	Zone Name	Zone ti	tle turns p	urple italic for critical zone(s)			AV	Rooms	vestibule	Rooms	vestibule	AV	Corridors
	Zone Tag					F	7W3-79	7W3-77	7W3=77	7W3-62	7W3-62	7W3-60	<b>A</b>
	Snace type						Electrical	Conterence/m	Corridors	Conference/m	Corridors	Electrical	Corridors
			Select fr	om pull-down list			rooms	comg		coung		rooms	
	Floor Area of zone	Az	sf			[	26	217	41	251	66	26	223
	Design population of zone	Pz	P	(default value listed; may be over	erridden	ר)	0	10.85	0	12.55	0	0	0
	Design total supply to zone (primary plus local recirculated)	Vdzd	ctm Select fr	om pull-down list or loove block	if N/A	-	150	225	50	225	50	200	100
	Local recirc, air % representative of ave system return air	Er	Jelect II	on pundown nat or reave bidlik	11 11/71	ŀ	75%	75%	75%	75%	75%	75%	75%
Inputs for	Operating Condition Analyzed				_		. 076				. 576		
	Percent of total design airflow rate at conditioned analyzed	Ds	%			100%	100%	100%	100%	100%	100%	100%	100%
	Air distribution type at conditioned analyzed	_	Select fr	om pull-down list		_	CS	CS	CS	CS	CS	CS	CS
	Zone air distribution effectiveness at conditioned analyzed	Ez				Ļ	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Results	Primary an traction of supply all at conditioned analyzed	Ер											
recounte	Ventilation System Efficiency	Ev				0.71							
	Outdoor air intake required for system	Vot	cfm		:	2337							
	Outdoor air per unit floor area	Vot/As	cfm/sf			0.25							
	Outdoor air per person served by system (including diversity)	Vot/Ps	cfm/p			10.7							
	Outdoor air as a % of design primary supply air	тра	cim			25%							
Detailed C	alculations												
Initial Calo	culations for the System as a whole												
	Primary supply air flow to system at conditioned analyzed	Vps	cfm	= VpdDs	=	9255							
	UncorrectedOA requirement for system	Vou	cfm	= Rps Ps + Ras As	=	1663							
Initial Cal	culations for individual zones	AS		= vou / vps	=	0.18							
initian our	OA rate per unit area for zone	Raz	cfm/sf				0.06	0.06	0.06	0.06	0.06	0.06	0.06
	OA rate per person	Rpz	cfm/p				0.00	5.00	0.00	5.00	0.00	0.00	0.00
	Total supply air to zone (at condition being analyzed)	Vdz	cfm				150	225	50	225	50	200	100
	Unused OA req'd to breathing zone	Vbz	cfm	= Rpz Pz + Raz Az	=		1.6	67.3	2.5	77.8	4.0	1.6	13.4
	Unused OA requirement for zone	Voz	cfm	= Vbz/Ez	=		2	67	2	2 78	4	2	13
	Fraction of zone supply from fully mixed primary air	Fa Fb		= Ep + (1-Ep)Er = Ep	=		1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Fraction of zone OA not directly recirc. from zone	Fc		= 1-(1-Ez)(1-Ep)(1-Er)	=		1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Unused OA fraction required in supply air to zone	Zd		= Voz / Vdz	=		0.01	0.30	0.05	0.35	0.08	0.01	0.13
	Unused OA fraction required in primary air to zone	Zp		= Voz / Vpz	=		0.01	0.30	0.05	0.35	0.08	0.01	0.13
System Vo	entilation Efficiency	_											
	Zone ventilation Efficiency (App A Method)	EVZ Ev		= (Fa + FbXs - FcZ) / Fa = min (Evz)	=	0.71	1.17	0.88	1.13	0.83	1.10	1.17	1.05
	Ventilation System Efficiency (Table 6.3 Method)	Ev		= Value from Table 6.3	-	0.68							
Minimum	outdoor air intake airflow												
	Outdoor Air Intake Flow required to System	Vot	cfm	= Vou / Ev	=	2337							
	OA intake req'd as a fraction of primary SA	Y		= Vot / Vps	=	0.25							
	Outdoor Air Intake Flow required to System (Table 6.3 Method)	Vot	cfm	= Vou / Ev	=	2439							
OA Temp	at which Min OA provides all cooling	T		= vot / vps	=	0.26							
571 T 0.11p	OAT below which OA Intake flow is @ minimum		Deg F	= ${(Tp-dTsf)-(1-Y)*(Tr+dTr)}$	=	5							

Building		Duval	County U	nified Courthouse Faciliy									
System Operatin	ag/Name: a Condition Description:	7W-3											
Units (se	lect from pull-down list)	IP											
Inputs fo	r System Floor area served by system Population of area served by system (including diversity) Design primary supply fan airflow rate OA req'd per unit area for system (Weighted average) OA req'd per person for system area (Weighted average)	<u>Name</u> As Ps Vpsd Ras Rps	<u>Units</u> sf P cfm cfm/sf cfm/p	100% diversity	Sy	9,454 218 9,255 0.06 5.0							
Inputs to	Zone Name					Г	Evidence	Meeting	Vestibule	Vestibule	Meeting	Evidence	AV
		Zone ti	itle turns p	urple italic for critical zone(s)		-	714/2 62	Rooms	714/2 62	714/2 72	Rooms	714/0 70	714/2 72
						F	Storage	Conference/m	Corridors	Corridors	Conference/m	Storage	Electrical
	Space type		Select fr	om pull-down list			rooms	eeting			eeting	rooms	equipment rooms
	Floor Area of zone	Az	sf				79	273	66	60	279	67	35
	Design population of zone Design total supply to zone (primary plus local recirculated)	PZ Vdzd	P cfm	(default value listed; may be ove	erriaae	n)	50	13.65	<u> </u>	50	13.95	<u> </u>	200
	Induction Terminal Unit, Dual Fan Dual Duct or Transfer Fan?	V GEG	Select fr	om pull-down list or leave blank	if N/A						220		200
	Local recirc. air % representative of ave system return air	Er					75%	75%	75%	75%	75%	75%	75%
Inputs fo	Percent of total design airflow rate at conditioned analyzed	Ds	%			100%	100%	100%	100%	100%	100%	100%	100%
	Air distribution type at conditioned analyzed	20	Select fr	om pull-down list		10070	CS	CS	CS	CS	CS	CS	CS
	Zone air distribution effectiveness at conditioned analyzed	Ez				Ę	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Beculto	Primary air fraction of supply air at conditioned analyzed	Ep											
Results	Ventilation System Efficiency	Ev				0.71							
	Outdoor air intake required for system	Vot	cfm			2337							
	Outdoor air per unit floor area	Vot/As	cfm/sf			0.25							
	Outdoor air per person served by system (including diversity)	Vot/Ps	cfm/p			10.7							
	Outdoor air as a % of design primary supply air	үра	cfm			25%							
Detailed	Calculations												
Initial Ca	culations for the System as a whole												
	Primary supply air flow to system at conditioned analyzed	Vps	cfm	= VpdDs	=	9255							
	UncorrectedOA requirement for system	Vou	cfm	= Rps Ps + Ras As	=	1663							
Initial Ca	Incorrected OA regid as a fraction of primary SA	XS		= vou/vps	=	0.18							
inneiar oa	OA rate per unit area for zone	Raz	cfm/sf				0.12	0.06	0.06	0.06	0.06	0.12	0.06
	OA rate per person	Rpz	cfm/p				0.00	5.00	0.00	0.00	5.00	0.00	0.00
	Total supply air to zone (at condition being analyzed)	Vdz	cfm				50	225	50	50	225	50	200
	Unused OA req'd to breathing zone	Vbz	cfm	= Rpz Pz + Raz Az	=		9.5	84.6	4.0	3.6	86.5	8.0	2.1
	Unused OA requirement for zone	Voz	cfm	= Vbz/Ez	=		9	85	4	4	86	8	2
	Fraction of zone supply not directly recirc. from zone	Fa		= Ep + (1-Ep)Er	=		1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Fraction of zone supply from fully mixed primary air	FD		= Ep = 1 (1 Ez)(1 Ez)(1 Ez)	=		1.00	1.00	1.00	1.00	1.00	1.00	1.00
	Lipused OA fraction required in supply air to zone	FC Zd		$= 1-(1-E_2)(1-E_1)$	-		0.19	0.38	0.08	0.07	0.38	0.16	0.01
	Unused OA fraction required in primary air to zone	Zp		= Voz / Voz	_		0.19	0.38	0.08	0.07	0.38	0.16	0.01
System V	/entilation Efficiency	•											
	Zone Ventilation Efficiency (App A Method)	Evz		= (Fa + FbXs - FcZ) / Fa	=		0.99	0.80	1.10	1.11	0.80	1.02	1.17
	System Ventilation Efficiency (App A Method)	Ev		= min (Evz)	=	0.71							
No	Ventilation System Efficiency (Table 6.3 Method)	Ëv		= Value from Table 6.3	=	0.68							
Minimum	Outdoor air Intake airliow	Vet	ofm			2227							
	OA intake reg'd as a fraction of primary SA	Y	CITI		-	2337							
	Outdoor Air Intake Flow required to System (Table 6.3 Method)	Vot	cfm	= Vou / Ev	-	2439							
	OA intake reg'd as a fraction of primary SA (Table 6.3 Method)	Y		= Vot / Vps	=	0.26							
OA Tem	at which Min OA provides all cooling												
	OAT below which OA Intake flow is @ minimum		Deg F	= ${(Tp-dTsf)-(1-Y)*(Tr+dTr)}$	=	5							

Building:	Duval	County U	nifie	ed Courthouse Faciliv						
System Tag/Name:										
Operating Condition Description:										
Units (select from pull-down list)	IP									
					_					
Inputs for System	Name	Units			Ľ	System				
Floor area served by system	AS	SI			-	9,454				
Population of area served by system (including diversity)	PS Veed	P		100% diversity		210				
$\Omega$ regid per unit area for system (Weighted average)	Pas	ofm/of				9,200				
OA regid per unit alea for system area. (Weighted average)	Rns	cfm/p				0.00				
Inputs for Potentially Critical zones	it p3	cin/p				5.0				
							Corridor	Meeting	Vestibule	Corridors
Zone Name	Zone ti	tle turns p	urpl	e italic for critical zone(s)				Rooms	100110410	connucle
Zone Tag			1					7W3-75	7W3-75	
							Corridors	Conference/m	Corridors	Corridors
Space type								eeting		
		Select f	om	pull-down list						
Floor Area of zone	Az	sf					222	257	68	1958
Design population of zone	Pz	Р	(def	fault value listed; may be o	verrid	den)	0	12.85	0	0
Design total supply to zone (primary plus local recirculated)	Vdzd	cfm					100	225	50	350
Induction Terminal Unit, Dual Fan Dual Duct or Transfer Fan	?	Select f	om	pull-down list or leave blan	nk if N/	A				
Local recirc. air % representative of ave system return air	Er						75%	75%	75%	75%
Inputs for Operating Condition Analyzed						10051		10.55	10.55	10.55
Percent of total design airflow rate at conditioned analyzed	Ds	%		and dama link		100%	100%	100%	100%	100%
Air distribution type at conditioned analyzed	-	Select f	om	pull-down list			CS	CS	CS	CS
Zone air distribution effectiveness at conditioned analyzed	EZ						1.00	1.00	1.00	1.00
Primary air fraction of supply air at conditioned analyzed	Ep									
Kesuits	Ev.					0.71				
Outdoor air intake required for system	EV Vot	ofm				2227				
Outdoor air make required for system	Vot/Ac	ofm/of				2337				
Outdoor air per unit noor area	Vot/Ps	cfm/n				10.23				
Outdoor air per person served by system (including diversity)	Voirs	cfm				25%				
Outdoor all as a 70 of design primary supply all	ipu	CIIII				23/0				
Detailed Calculations										
Initial Calculations for the System as a whole										
Primary supply air flow to system at conditioned analyzed	Vps	cfm	=	VpdDs	=	9255				
UncorrectedOA requirement for system	Vou	cfm	=	Rps Ps + Ras As	=	1663				
Uncorrected OA req'd as a fraction of primary SA	Xs		=	Vou / Vps	=	0.18				
Initial Calculations for individual zones										
OA rate per unit area for zone	Raz	cfm/sf					0.06	0.06	0.06	0.06
OA rate per person	Rpz	cfm/p					0.00	5.00	0.00	0.00
Total supply air to zone (at condition being analyzed)	Vdz	cfm					100	225	50	350
Unused OA req'd to breathing zone	Vbz	cfm	=	Rpz Pz + Raz Az	=		13.3	79.7	4.1	117.5
Unused OA requirement for zone	Voz	cfm	=	Vbz/Ez	=		13	80	4	117
Fraction of zone supply not directly recirc. from zone	Fa		=	Ep + (1-Ep)Er	=		1.00	1.00	1.00	1.00
Fraction of zone supply from fully mixed primary air	Fb		=	Ep	=		1.00	1.00	1.00	1.00
Fraction of zone OA not directly recirc. from zone	Fc		=	1-(1-Ez)(1-Ep)(1-Er)	=		1.00	1.00	1.00	1.00
Unused OA fraction required in supply air to zone	Zd		=	Voz / Vdz	=		0.13	0.35	0.08	0.34
Unused OA fraction required in primary air to zone	Zp		=	Voz / Vpz	=		0.13	0.35	0.08	0.34
System Ventilation Efficiency	-									
Zone Ventilation Efficiency (App A Method)	Evz		=	(Fa + FbXs - FcZ) / Fa	=	0.74	1.05	0.83	1.10	0.84
System Ventilation Efficiency (App A Method)	EV		=	Mahua (EVZ)	=	0.71				
Ventuation System Efficiency (Table 6.3 Wethod)	EV		=	value from Table 6.3	=	0.68				
Outdoor Air Intake airriow	Vet	ofm		Vou / Ev		2227				
Outdoor Air Intake Flow required to System	VOT	CIIII	=	Vou / Ev	=	2337				
Overhalter of a statistic of the sector of primary SA	d) Vot	ofm	=	Vor / Vps	=	0.25				
Outdoor All Initiake Flow required to System (Table 6.3 Metho OA intake regid as a fraction of primary SA (Table 6.3 Metho		CITI	Ē.	Vot / Vos	-	2439				
OA make requise a raction of primary SA (Table 6.3 Metho			=	vot/vps	-	0.20				
or rollp at which will or provides all cooling										