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Broad Institute Expansion :

75 Ames Street

Cambridge, Massachusetts

Technical Report Two :

[Building and Plant Energy Analysis Report]

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Executive Summary

For Technical Report two the total building energy usage and cost was estimated using Trane Trace 700 on 75 Ames Street, a new high-rise in Cambridge Massachusetts containing labs, research and development, office and retail space. 75 Ames first 11 floors contain the offices, labs and retail, on the 12th floor is a vivarium. The total area is approximately 550,000 sf.

The TRACE model 700 model calculated a total heating load of 770,900 btuh and a cooling load of 2530.1 tons. The heating loads are greater than the cooling loads which makes since seeing as Massachusetts is a mostly cold place. But through further analysis of the load there seems to be an error in the heating value when compared to the engineers design. This is apparent when the 150,597 therms of natural gas needed for heating is compared with the 348,500 therms called for by the design engineers at BR+A. Cooling loads capacity per SF also seemed a bit high when compared to rules of thumb for office cooling loads having values of .95 and .98 tons/SF.

The Trace model came to within 8% of the total energy cost of electricity and natural gas consumption. Electricity estimation was very close with 8,954,124 kWh coming within .21% of the price determined by the mechanical engineers. Again the mistake in natural gas consumption is the reason for that 8% difference. The yearly bill calculated by trace came out to be \$2,040,282.41 making the cost per square foot only \$6.98 dollars.

The dilemma with the natural gas consumption is going to have to be investigated, and solved moving forward. Much can still be learned from this report. And may be looked back on as a reference to future assignments to see where a majority of the costs are incurred for the electrical consumption.

Building Overview

75 Ames Street is a new 250,000 sq. ft., 15-story high-rise addition to Kendal Square in Cambridge, Massachusetts (figure1 below). This building is designed to bring together the multiple Broad institute offices around the Cambridge area into one location attached to their main office at 7 Cambridge Center.

This structure is set to finish the Ames Street frontage and add to the current pedestrian walk space. This is done with a new pedestrian entrance to a 5 floor garage attached to Ames Street as well as 4000 sq. ft. of retail and restaurant space on the ground floor. The primary design is for offices and research & development labs which use a majority of the area. Some other notable areas of the 75 Ames are a vivarium on the 12th floor and 3 mechanical rooms making up the penthouse.

The exterior is mainly composed of a mixture of stone, terra cotta, Viracon vision glass and spandrel glass. The penthouse is primarily constructed of aluminum louvers and metal panels. The front façade adds to the vibrant community on Ames Street while the other three facades connect 75 Ames to the current Broad Institute main office next door at 7 Cambridge Center.



Figure 1: A look at the location of 75 Ames Street in Cambridge (courtesy of ELKUS | MANFREDI ARCHITECTS)

Mechanical System Overview

Four 115,000 CFM 100% outside air, air-handling units are located inside the mechanical rooms on M1, M2 and M3, supplying the basement through level 11. A fifth 100% outside air, air handler is located on M3 serving the vivarium on level 12. Two 230,000 CFM dedicated exhaust air handling units located on the roof exhaust through 8 air induction nozzles roughly 28 feet off the roof.

Level M2 hosts the heating plant consisting of two 500 BHP preheat fire tube boilers, four 120 BHP Reheats with one standby, two 215 BHP MPS boilers for humidification and process steam loads, and finally a pressure reducing LPS for humidifiers. Also on M2 is the chiller plant consisting of three 1000 ton chillers for air cooling air handing units 1 through 4 and two 450 ton chillers to serve vivarium (AHU-5) and fan coil units which serve freezer rooms, tel/data, electrical, and the penthouse for spot cooling. Each chiller has a corresponding cooling tower located on the roof.

The ducting on each floor was taken with future floor plan changes in mind. In order to achieve this, air-handling units 1 through 4 each connect to a main ring on each floor. This can be seen in the following figures 2 & 3 which show the supply and exhaust duct respectively. These rings then supply air to each zone on their floor. Since they are serving both labs and offices together

return air cannot be utilized since labs call for 100 % outside air. The only return air used in this building is 16000 CFM of air from the connector of 75 Ames Street to 7 Cambridge Center to level M1.

Figure 2: Dedicated Exhaust Ductwork

Figure 3: Supply Air Ductwork





Building Load Calculations

Using Trane TRACE 700 a building energy analysis was conducted for 75 Ames Street. Heating, cooling and energy usage were all found. Information for the model was obtained through construction documents, specs, and reports provided by the mechanical engineer, BR+A. The various assumptions, schedules, and design conditions for this model can be found below.

Design conditions

Cambridge is located in ASHRAE weather region 5A. This weather data is used by TRACE when Boston Massachusetts is selected for the weather information. These weather inputs can be found in appendix A. The interior design temperature and humidity as specified by the engineers at BR+A may be found in Tables 1 & 2 below. Table 1

Space	Temperature			
Space	Winter (F)	Summer (F)		
Office/Conference/Lobby	72	75		
Labs	72	75		
General Spaces	72	75		
Vivarium	68-75(ADJ)	68-75(ADJ)		
Shell/Mech./Elec. Spaces	60	Ventilation Only		
Loading Dock	60	Ventilation Only		

Table 2

Space	Humidity			
	Winter (%RH)	Summer (%RH)		
Office/Conference/Lobby	25 (+/-5)	50 (+/-5)		
Labs	25 (+/-5)	50 (+/-5)		
General Spaces	25 (+/-5)	50 (+/-5)		
Vivarium	25-40 (+/-5)	50 (+/-5)		

Model design

For design purposes air handlers one, two, three and four were modeled as one 460,000 CFM unit that serves the basement through to the 11th floor. Zones were decided by the similarity and proximity of rooms and the VAV boxes serving them.

Load assumptions

Room areas were exported from a Revit model of 75 Ames and small/unnecessary spaces were not included. Exterior wall and window areas were calculated using Revit and the construction drawings. U-values for exterior materials were found in the specifications. Each exterior area and material was added to the appropriate room.

Occupancy

Occupancy values were not directly given for spaces. So values were taken from ASHRAE Standard 62.1-2010. These values can be found in Appendix B.

Ventilation

75 Ames is set at 100% outside air for all spaces due to a ganged duct design which supplies both the labs and offices. Even with this fans still must maintain a minimum occupied and unoccupied ventilation rate to maintain occupant's safety. These ventilation rates can be seen in table 3 below along with the rooms requiring 100% outside air. Table 3

Space	%OA	Min ventilation
Labs	100	6-12 ACH
Tissue Culture Rooms	100	8-15 ACH
Office Area		20 CFM/Occupant
Auditorium/Seminar/Conf./Class		15 CFM/Occupant
Cagewash/Glasswash/Bottlewash	100	15-20 ACH
Equipment/Instrument Rooms	100	10-20 ACH
Animal Rooms 100		10-15
Animal Imaging		20 CFM/Person
Toilet/Janitor/Darkroom/Locker	100	10 ACH (Exhaust)
Mech. Spaces	100	2 ACH

Lighting and Equipment Electrical loads

Lighting and miscellaneous loads were both detailed in the design documents for 75 Ames. These loads are given in watts per square foot in table four below. For area not given a reasonable estimate was made by looking at ASHRAE 90.1 and the design documents. For rooms with large equipment the equipment specifications were examined to find the watts needed to operate.

Table 4

C 1 2 3	Loads			
Space	Lighting (Watts/SF)	Misc./Equipment (Watts/SF)		
Labs	2	10 Watts/SF		
Tissue Culture Rooms	2	20		
Office Area	1.2	2		
Auditorium/Seminar/Conf./Class	4	2		
Cagewash/Glasswash/Bottlewash	2	Per equip. cuts		
Equipment/Instrument Rooms	2	40		
Animal Rooms	Not given	Not given		
Animal Imaging	2	Per manufacturer		
Toilet/Janitor/Darkroom/Locker	1.5	1		
Mech. Spaces	Not given	Per equip. cuts		

Construction

Templates were designed in trace to act as the different facades of 75 Ames. Below Table 5 shows the various U values and shading coefficients. Vertical Glazing makes up nearly 40% of the building's exterior with no exterior shading, this could result in very high loads in perimeter rooms bringing up the yearly cooling and heating loads on the building

Table 5

Construction	U-value Btu/h-ft2-F	Shading Coefficient
Exterior Wall	0.083	
Roof	0.05	
Floor	0.15	
Windows	0.29	0.44

Schedules

Three main schedules were utilized in TRACE for the modeling of 75 Ames. Those schedules are lighting, miscellaneous and people. Since this is primarily an office/lab most activity occurs during normal work hours and the building load will significantly decrease at night. The schedules used can be found in Appendix C.

Calculated Load vs. Design Load Analysis

After running the model the system checksums sheet was used to analyze the heating and cooling airflows, along with the total heating and cooling coil capacities. System Checksums can be found in appendix D. A standard value of cooling capacity was found for an office building but none could be found for a lab so the lab is substituted with a hospital. As can be seen by table 6 below, the cooling capacity falls well above the standard for an office and just above that of a hospital. This could be a result of a large amount of glazing utilized by the building.

		Area	Supply Air P Area (CFN	Per Unit //SF)	TOTAL	. CFM	Capacity	Per Area	Total (tons)
			Cooling	Heating	Cooling	Heating	Heating (Btuh/sf)	Cooling (tons/SF)	Heating	Cooling
Calculated	AHU 1-2- 3-4	244,902	1.608	0.4217	393,868	103283	15.86	.0095	388,300	2,325.4
	AHU- 5	20,817	1.57	0.538	32,716	11,199	18.379	.0098	382600	204.7
Standard for office			0.25 - 0.9					.00278- .005		
Standard for hospitals			0.33 - 0.67					.003006		

Table 6

System Energy Consumption and Cost

In this report Trane TRACE was also used to calculate the use of electricity and gas for a typical year. Through this energy consumption the yearly operating cost is also found. This data is then compared to an E-quest report by BR+A containing the same information.

Fuel Costs

The following energy costs are real estimates per Massachusetts's average pricing.

Table 7

Utility Rates					
Electricity	\$0.201	Per kWh			
Natural Gas	\$1.597	Per Therm			

Results

The Trace model predicted electricity, total cost per year and cost per square foot relatively accurately. One main problem in the design was an under estimate of the natural gas usage by over 50%. This is clearly shown below in table 8 and figures 9 & 10.

Table 8

	Electricity (kWh)	Natural Gas (Therms)	Electricity Cost Per Year	Natural Gas Cost Per year	Total Cost per Year	Cost Per Square Foot
TRACE	8,954,124	150597.05	\$1,799,778.92	\$240,503.49	\$2,040,282.41	\$6.98
BR+A	8,973,000	348,500	\$1,803,573.00	\$556,554.50	\$2,360,127.50	\$7.57
Difference (%)	0.21036443	56.78707	0.210364427	56.78707317	13.55202578	7.772873269

Below in figures 7 and 8 is a breakdown of the monthly electricity consumption in a bar chart. Figure 7 is from the mechanical engineers at BR+A and totals consumption per month with a breakdown of where the load comes from. As seen by the graphs the energy consumption per month is relatively similar. Further below is the gas energy consumption figure 9 being BR+A's model and 10 being the Trace model. In comparing these two graphs it is evident where the severe lack in gas consumption from the trace to BR+A's model. Heating demand for the Trace model in May, June, July, August, September, and October are all nearly nonexistent. This problem was attempted to be solved but no method has worked as of yet. Possible reasons for this drastic difference could be a bad template, or missing equipment.



BR+A Electric Consumption (kWh x000,000)

Figure 4



Figure 5



BR+A Natural Gas Consumption (Btu x000,000,000)

Figure 6



Figure 7

2012

Below in Figure 11 is a graph of the cooling and heating profiles. It is clear here that heating is dominating the winter months and cooling takes over in the hotter months as expected.



Figure 8

Emissions

In order to find the building's carbon footprint using emissions profiles is suggested. Emission rates per electricity consumed are found using the National Renewable Energy Laboratory's report on Source Energy and Emission Factors for Energy Use in Buildings. These factors take into account electricity delivered (table 9), fuel delivered (table 10) and on site fuel combusted (table 11) can be found in the following tables. The last two figures (table 12 and figure 9 show the total pollutant output per year.

Table 9

Total Emission Factors for Delivered Electricity (lb of Pollutant per kWh of Electricity)					
Pollutant (lb)	Eastern factor	Electrical consumption per year (kWh/year)	Total Pollutants [lbs/year]		
CO2e	1.74E+00	8,954,124	15580175.76		
CO2	1.22E+00	8,954,124	10924031.28		
CH4	3.51E-03	8,954,124	31428.98		
N2O	2.97E-05	8,954,124	265.94		
NOX	1.95E-03	8,954,124	17460.54		
SOX	6.82E-03	8,954,124	61067.13		
со	5.46E-04	8,954,124	4888.95		
тлмос	6.45E-05	8,954,124	577.54		
Lead	8.95E-08	8,954,124	0.80		
Mercury	1.86E-08	8,954,124	0.17		
PM10	6.99E-05	8,954,124	625.89		
Solid Waste	1.39E-01	8,954,124	1244623.24		

2012

Table 10

Pre combustion Emission Factors for Fuel Delivered to Buildings (Ib pollutant per unit of fuel)					
Pollutant (lb)	Eastern	Fuel per 1000 cubic feet natural gas	Total Pollutants [lbs/year]		
CO2e	2.78E+01	10044.82324	279246.0859		
CO2	1.16E+01	10044.82324	116519.95		
CH4	7.04E-01	10044.82324	7071.56		
N2O	2.35E-04	10044.82324	2.36		
NOX	1.64E-02	10044.82324	164.74		
SOX	1.22E+00	10044.82324	12254.68		
СО	1.36E-02	10044.82324	136.61		
TNMOC	4.56E-05	10044.82324	0.46		
Lead	2.41E-07	10044.82324	0.00		
Mercury	5.51E-08	10044.82324	0.00		
PM10	8.17E-04	10044.82324	8.21		
PM- unspecified	1.42E-03	10044.82324	14.26		
Solid Waste	1.60E+00	10044.82324	14.26		

Table 11

Table 8 Emission Factors for On-Site Combustion in a Commercial Boiler (Ib of pollutant per unit of fuel)					
Pollutant (lb)	natural Gas	Fuel per 1000 cubic feet natural gas	Total Pollutants [lbs/year]		
CO2e	1.23E+02	10044.82324	1235513.258		
CO2	1.22E+02	10044.82324	1225468.43		
CH4	2.50E-03	10044.82324	25.11		
N2O	2.50E-03	10044.82324	25.11		
NOX	1.11E-01	10044.82324	1114.98		
SOX	6.32E-04	10044.82324	6.35		
СО	9.33E-02	10044.82324	937.18		
TNMOC	6.13E-03	10044.82324	61.57		
Lead	5.00E-07	10044.82324	0.01		
Mercury	2.60E-07	10044.82324	0.00		
PM10	8.40E-03	10044.82324	84.38		

Table 12

Total Pollutants (lb/yeart)									
CO2e	17094935.1								
CO2	12266019.66								
CH4	38525.65								
N2O	293.41								
NOX	18740.26								
SOX	73328.16								
CO	5962.74								
TNMOC	639.57								
Lead	0.81								
Mercury	0.17								
PM10	718.48								
PM-	14.26								
unspecified	14.20								
Solid Waste	1244637.5								



Figure 9

Conclusion

75 Ames Street contains various different rooms with different loads due to occupancy, space type, and heat gain through exterior walls and windows. Building loads and energy simulations were obtained by setting specific values for each room in TRACE 700, and setting up the heating and cooling plants. Overall trace came out with a reasonable estimate for cooling loads but the heating load design conditions needs to be further examined to find out why the value differs so much from the mechanical engineers values. Even with that glitch the cost estimate for a year was still only 8% off of the designed value.

Works Cited

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Appendix A

Boston, Ma – TRACE Weather Conditions

Region			Subregion				Location	
United State	s	-	North East		•		Boston, Massachusetts	-
Filename								
Latitude Longitude Altitude	42 d	leg leg	Time zone Design month Dé pressure	5 July	▼ in Ha		ASHRAE Climatic Data Station WMD # 725090 Select Locatic Station Name Boston	n
Summer	0ADB 0 *F 88 74	AWB _°F	Clearness 0.85	Ground reflect	Wind velocity mph		Winter Design 99.6 % 99 % Dry Bulb 7.7 12.3 Cooling Maximum DB / Mean Coincident WB 0.4 % 1 % 2 %	
Saturation C Coef A -0.31246149	urve Coefficients Coe 0.923011	ef B 131	Coef C	3 0.00	Coef D 103278286		Wet Bulb 73.1 71.7 70.3 Dew Point 65.45 64.6 63.8 Dehumid Maximum WB / Mean Coincident	-
Comments Created by C.	D.S. Marketing					,	0.4 % 1 % 2 % Dry Bulb 80.7 78.8 77.8 Wet Bulb 74.99 73.46 72.24 Dew Point 72.8 71.3 69.9	

Appendix B

-	People	Outdoor	Area C	utdoor		Defa	ult Values		
Occupancy Category	Air	Rate R _p	Air Air	Rate a	Notes	Occupant Density (see Note 4)	Combined Air Rate (s	l Outdoor see Note 5)	Air Class
	cfm/person	L/s-person	cfm/ft ²	L/s·m ²		#/1000 ft ² or #/100 m ²	cfm/person	L/s-person	
Correctional Facilities									
Cell	5	2.5	0.12	0.6		25	10	4.9	2
Dayroom	5	2.5	0.06	0.3		30	7	3.5	1
Guard stations	5	2.5	0.06	0.3		15	9	4.5	1
Booking/waiting	7.5	3.8	0.06	0.3		50	9	4.4	2
Educational Facilities									
Daycare (through age 4)	10	5	0.18	0.9		25	17	8.6	2
Daycare sickroom	10	5	0.18	0.9		25	17	8.6	3
Classrooms (ages 5-8)	10	5	0.12	0.6		25	15	7.4	1
Classrooms (age 9 plus)	10	5	0.12	0.6		35	13	6.7	1
Lecture classroom	7.5	3.8	0.06	0.3		65	8	4.3	1
Lecture hall (fixed seats)	7.5	3.8	0.06	0.3		150	8	4.0	1
Art classroom	10	5	0.18	0.9		20	19	9.5	2
Science laboratories	10	5	0.18	0.9		25	17	8.6	2
University/college laboratories	10	5	0.18	0.9		25	17	8.6	2
Wood/metal shop	10	5	0.18	0.9		20	19	9.5	2
Computer lab	10	5	0.12	0.6		25	15	7.4	1
Media center	10	5	0.12	0.6	А	25	15	7.4	1
Music/theater/dance	10	5	0.06	0.3		35	12	5.9	1
Multi-use assembly	7.5	3.8	0.06	0.3		100	8	4.1	1
Food and Beverage Servi	ce								
Restaurant dining rooms	7.5	3.8	0.18	0.9		70	10	5.1	2
Cafeteria/fast-food dining	7.5	3.8	0.18	0.9		100	9	4.7	2
Bars, cocktail lounges	7.5	3.8	0.18	0.9		100	9	4.7	2
Kitchen (cooking)	7.5	3.8	0.12	0.6		20	14	7.0	2
General									
Break rooms	5	2.5	0.06	0.3		25	10	5.1	1
Coffee stations	5	2.5	0.06	0.3		20	11	5.5	1
Conference/meeting	5	2.5	0.06	0.3		50	6	3.1	1
Corridors	_	-	0.06	0.3		_			1
Occupiable storage rooms for liquids or gels	5	2.5	0.12	0.6	в	2	65	32.5	2
Hotels, Motels, Resorts, I	Dormitories								
Bedroom/living room	5	2.5	0.06	0.3		10	11	5.5	1
Barracks sleeping areas	5	2.5	0.06	0.3		20	8	4.0	1
Laundry rooms, central	5	2.5	0.12	0.6		10	17	8.5	2
Laundry rooms within dwelling units	5	2.5	0.12	0.6		10	17	8.5	1
Lobbies/prefunction	7.5	3.8	0.06	0.3		30	10	4.8	1
Multipurpose assembly	5	2.5	0.06	0.3		120	6	2.8	1

TABLE 6-1 MINIMUM VENTILATION RATES IN BREATHING ZONE (This table is not valid in isolation; it must be used in conjunction with the accompanying notes.)

	People (Outdoor	Area O	utdoor		Defa	ult Values		
Occupancy	Air] R	Rate P	Air I R	Rate a	Notes	Occupant Density (see Note 4)	Combined Air Rate (s	Outdoor see Note 5)	Air
Category	cfm/person	L/s-person	cfm/ft ²	L/s·m ²		#/1000 ft ² or #/100 m ²	cfm/person	L/s-person	Class
Office Buildings									
Breakrooms	5	2.5	0.12	0.6		50	7	3.5	1
Main entry lobbies	5	2.5	0.06	0.3		10	11	5.5	1
Occupiable storage rooms for dry materials	5	2.5	0.06	0.3		2	35	17.5	1
Office space	5	2.5	0.06	0.3		5	17	8.5	1
Reception areas	5	2.5	0.06	0.3		30	7	3.5	1
Telephone/data entry	5	2.5	0.06	0.3		60	6	3.0	1
Miscellaneous Spaces									
Bank vaults/safe deposit	5	2.5	0.06	0.3		5	17	8.5	2
Banks or bank lobbies	7.5	3.8	0.06	0.3		15	12	6.0	1
Computer (not printing)	5	2.5	0.06	0.3		4	20	10.0	1
General manufacturing (excludes heavy indus- trial and processes using chemicals)	10	5.0	0.18	0.9		7	36	18	3
Pharmacy (prep. area)	5	2.5	0.18	0.9		10	23	11.5	2
Photo studios	5	2.5	0.12	0.6		10	17	8.5	1
Shipping/receiving	10	5	0.12	0.6	в	2	70	35	2
Sorting, packing, light assembly	7.5	3.8	0.12	0.6		7	25	12.5	2
Telephone closets	-	_	0.00	0.0		-			1
Transportation waiting	7.5	3.8	0.06	0.3		100	8	4.1	1
Warehouses	10	5	0.06	0.3	в	-			2
Public Assembly Spaces									
Auditorium seating area	5	2.5	0.06	0.3		150	5	2.7	1
Places of religious worship	5	2.5	0.06	0.3		120	6	2.8	1
Courtrooms	5	2.5	0.06	0.3		70	6	2.9	1
Legislative chambers	5	2.5	0.06	0.3		50	6	3.1	1
Libraries	5	2.5	0.12	0.6		10	17	8.5	1
Lobbies	5	2.5	0.06	0.3		150	5	2.7	1
Museums (children's)	7.5	3.8	0.12	0.6		40	11	5.3	1
Museums/galleries	7.5	3.8	0.06	0.3		40	9	4.6	1
Residential									
Dwelling unit	5	2.5	0.06	0.3	F,G	F			1
Common corridors	-	-	0.06	0.3					1
Retail									
Sales (except as below)	7.5	3.8	0.12	0.6		15	16	7.8	2
Mall common areas	7.5	3.8	0.06	0.3		40	9	4.6	1
Barbershop	7.5	3.8	0.06	0.3		25	10	5.0	2

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	People (Area O	utdoor		Defa	ult Values			
Occupancy Category	Air] K	Rate P	Air I R	Rate a	Notes	Occupant Density (see Note 4)	Combined Air Rate (s	l Outdoor see Note 5)	Air Class
Caregory	cfm/person	L/s-person	cfm/ft ²	L/s·m ²	•	#/1000 ft ² or #/100 m ²	cfm/person	L/s-person	Chillip
Beauty and nail salons	20	10	0.12	0.6		25	25	12.4	2
Pet shops (animal areas)	7.5	3.8	0.18	0.9		10	26	12.8	2
Supermarket	7.5	3.8	0.06	0.3		8	15	7.6	1
Coin-operated laundries	7.5	3.8	0.12	0.6		20	14	7.0	2
Sports and Entertainmen	ıt								
Sports arena (play area)	-	_	0.30	1.5	Е	_			1
Gym, stadium (play area)	_	-	0.30	1.5		30			2
Spectator areas	7.5	3.8	0.06	0.3		150	8	4.0	1
Swimming (pool & deck)	_	-	0.48	2.4	С	_			2
Disco/dance floors	20	10	0.06	0.3		100	21	10.3	2
Health club/aerobics room	20	10	0.06	0.3		40	22	10.8	2
Health club/weight rooms	20	10	0.06	0.3		10	26	13.0	2
Bowling alley (seating)	10	5	0.12	0.6		40	13	6.5	1
Gambling casinos	7.5	3.8	0.18	0.9		120	9	4.6	1
Game arcades	7.5	3.8	0.18	0.9		20	17	8.3	1
Stages, studios	10	5	0.06	0.3	D	70	11	5.4	1

TABLE 6-1 MINIMUM VENTILATION RATES IN BREATHING ZONE (Continued) (This table is not valid in isolation; it must be used in conjunction with the accompanying notes.)

GENERAL NOTES FOR TABLE 6-1

Related requirements: The rates in this table are based on all other applicable requirements of this standard being met.

Environmental Tobacco Smoke: This table applies to ETS-free areas. Refer to Section 5.17 for requirements for buildings containing ETS areas and ETS-free areas. Air density: Volumetric airflow rates are based on an air density of 0.075 lb_a/ft³ (1.2 kg_a/m³), which corresponds to dry air at a barometric pressure of 1 atm (101.3 kPa) and an air temperature of 70°F (21°C). Rates may be adjusted for actual density but such adjustment is not required for compliance with this standard.

3

4

Default occupant density The default occupant density shall be used when actual occupant density is not known. Default combined outdoor air rate (per person): This rate is based on the default occupant density. Unlisted occupancies: If the occupancy category for a proposed space or zone is not listed, the requirements for the listed occupancy category that is most similar in terms of 6 occupant density, activities and building construction shall be used.

ITEM-SPECIFIC NOTES FOR TABLE 6-1

For high school and college libraries, use values shown for Public Assembly Spaces—Libraries. Rate may not be sufficient when stored materials include those having potentially harmful emissions

С Rate does not allow for humidity control. Additional ventilation or dehumidification may be required to remove moisture. "Deck area" refers to the area surrounding the pool that would be expected to be wetted during normal pool use, i.e., when the pool is occupied. Deck area that is not expected to be wetted shall be designated as a space type (for example, spectator area").

Parte does not include special exhaust for stage effects, e.g., dry ice vapors, smoke.
 When combustion equipment is intended to be used on the playing surface, additional dilution vertilation and/or source control shall be provided.
 Default occupancy for dwelling units shall be two persons for studio and one-bedroom units, with one additional person for each additional bedroom.
 Air from one residential dwelling shall not be recirculated or transferred to any other space outside of that dwelling.

different sources can be applied to any other aspect of indoor air quality.

6.2.2.1.1 Design Zone Population. Design zone population (P_z) shall equal the largest (peak) number of people expected to occupy the ventilation zone during typical usage.

Exceptions:

- a. If the number of people expected to occupy the ventilation zone fluctuates, zone population equal to the average number of people shall be permitted, provided such average is determined in accordance with Section 6.2.6.2.
- b. If the largest or average number of people expected to occupy the ventilation zone cannot be established for a specific design, an estimated value for zone population shall be permitted, provided such value is the product of the net occupiable area of the ventilation zone and the default occupant density listed in Table 6-1.

6.2.2.2 Zone Air Distribution Effectiveness. The zone air distribution effectiveness (E_z) shall be no greater than the default value determined using Table 6-2.

Note: For some configurations, the default value depends upon space and supply air temperature.

Appendix C

_ [⊂] Schedule	Definition			
	Start		End	
Month	January	•	December	•
Day type	Cooling desig	an 🔺	Weekday 🔹	•
	Start time	End time	Percentage	
	Midnight	7 a.m.	0	▲
	7 a.m.	8 a.m.	30	
	8 a.m.	5 p.m.	100	
	5 p.m.	6 p.m.	30	
	6 p.m.	7 p.m.	1	
	7 p.m.	Midnight	0	
				-

Utilizations schedule for people occupying office

Utilizations for lights in an office

Schedule	Definition		
	Start		End
Month	January	-	December 🗨
Day type	Cooling desig	gn ▼	Weekday 💌
	Start time	End time	Percentage
	Midnight	6 a.m.	0
	6 a.m.	7 a.m.	10
	7 a.m.	8 a.m.	50
	8 a.m.	5 p.m.	100
	5 p.m.	6 p.m.	50
	6 p.m.	7 p.m.	10
	7 p.m.	Midnight	0
			▼

Utilization Of Ventilation for an Office

[_] Schedule	Definition			
Month Day type	Start January Cooling desid	▼ In ▼	End December _	- -
2.07.920	Start time Midnight 7 a.m. 6 p.m.	End time 7 a.m. 6 p.m. Midnight	Percentage 0 100 0	

Utilization Schedule for Misc. Loads in Office

Start time	End Time	Percenage
Midnight	7 a.m.	5
7 a.m.	8 a.m.	80
8 a.m.	10 a.m.	90
10 a.m.	Noon	95
Noon	2 p.m.	80
2 p.m.	4 p.m.	90
4 p.m.	5 p.m.	95
5 p.m.	6 p.m.	80
6 p.m.	7 p.m.	70
7 p.m.	8 p.m.	60
8 p.m.	9 p.m.	40
9 p.m.	10 p.m.	30
10 p.m.	Midnight	20



Alternative - 1 System Checksums Report Page 1 of 2

0.0	0.0	4.0	۶F
0.0	0.0	105.0	B/HR gr/lb
		on	

Main Clg Aux Clg Opt Vent

2,325.4 0.0

27,904.3 0.0 0.0

15,070.9 0.0 0.0

367,988 0 0

87.5 0.0

0.0

Total Capacity ton MBh

Sens Cap. MBh

Coil Airflow cfm

۴

COOLING COIL SELECTION

Total

2,325.4

27,904.3

Dataset Name: Project Name:

Appendix D

AHU-1-2-3-4

Peaked at Time: Outside Air:

Mo/Hr: 7 / 16 OADB/WB/HR: 88 / 74 / 105

Space Sens. + Lat.

Plenum Sens. + Lat

Percent Of Total

Btu/h

Btu/h

Btu/h Net Total

(%)

0

COOLING COIL PEAK

	0.0	0 105.0	s/WB/HR F gr/lb	9,001,966				0	0	20,574 0		4,140,000 5,924,168	885,470	897,834		3,007,223	0	0	0 0	11,636	52,331	2.993.256	, 0	D	Btu/h	Sensible O	Space P		Mo/Hr: 7 / OADB: 79	CLG SPACE P		
	0.0 0.0 0.0	51.2 51.0	Leave DE	100.00 Gr	S C		RA	0.0	D Ad			8 8	10	6	Int	¥	20	0		2.0		80	, 0	- -	(%))f Total	ercent		10	EAK		
	0.0	55.4	gr/lb	and Total =	iderfir Sup Ipply Air Le		\ Preheat D Iditional Re	haust Heat \ Preheat D	j Air Trans /Undr Sizir	ntilation Lo		Nilsc Sub Total =	People	Lights	ernal Load	- IPIOL GDC	Infiltration	Adjacent Fl	Floor	Wall Cond	Glass/Door	Glass Solar	Skylite Con	Skylite Sola								
Roof Wall Ext Door	Part Int Door ExFlr	Floor	0	8	Ht Pkup Ht Age		heat	Ħ,	Heat	vad		V			s	Į	}	loor	-	5	Cond		đ	AL .	2							
0 102,287 0		244,902	ARE pross Total	-1,505,4						-15,1						-1,480,3	4 400 9			-84,5	-1,425,7				Bt	Space Se	Space Pe		Mo/	HEATIN		
64,860 0			AS Glas ft ²	128 -2					0 0	0		0	00	0		- 10	20	0	0 0	541	-00	0 0	0	•	u/h	ens	eak		Hr. Heating)B: 9	IG COIL F		
0 8 0			(%)	2,306,952	00		00	92,052 3,677,057		0 7,196,459	, ,			0		1,020,408	0	0		-99,729	1,425,760	0 0	, .		Btu/h	Tot Sens	Coil Peak		g Design	PEAK	Variab	
Humidif Opt Vent Total	Aux Htg Preheat Reheat	Main Htg	H	100.00	0.00		0.00	-0.41 61.31	0.00	0.00 32.26		0.00	0.00	0.00		0.04	0.00	0	0.00	0.45	6.39	0.00	0.00	0.00	(%)	Of Total	Percent				le Volum	
-8,867.4 0.0 -31,289.1	0.0 -18,538.3 -2,335.3	-3,883.3	Capacity (MBh	No. People	ft²/ton	cfm/ft ²	% OA	ENGIN		Leakage Uwn Leakage Ups	Auxiliary	Exnaust Rm Exh	Return	MinStop/Rh	Infil	AHII Vent	Sec Fan	Main Fan	Terminal	Diffuser		AI		Fn Frict	En BidTD	RetIOA	Return	Ra Plenum	SADB	TEMP	e Reheat (30%	
484,019 0	0 393,868 103,282 5	103,282 5	SELECTION Coil Airflow	3,675	105.32	1.61	Cooling 100.0	EERING CK		0 0	, .	210,270 178,620	215,248	103,282	0	393,868	000 000	393,868	393,868	393,868	Cooling	RFLOWS		2.7	0.2	87.5	75.4	75.4	Cooling 55.0	ERATURES	Min Flow I	
1.8 27.9 0.0 0.0	9.0 51.1 1.2 71.1	1.2 85.0	Ent Lvg	-127.70	1	0.42	Heating 100.0	S				10,980	92,302	103,282	100,202	103,282	0	103,282	103,283	103,283	Heating			0.0	0.0	9.0	70.7	70.7	Heating 85.0		Default)	

Adj Air Trans Heat Dehumid. Ov Stzing Ov/Undr Sizing Exhaust Heat Sup. Fan Heat Ret. Fan Heat Duct Heat Pkup Underfir Sup Ht Pkup

0

53,434

0 53,434 1,549,427

. <u>.</u> .

Grand Total ==> Supply Air Leakage

9,162,794

169,850

27,904,260

100.00

0 0 -

000 - 4 Ceiling Load Ventilation Load

20,983 0

083

0 17,022,189 0

Sub Total ==:

8,714,159

129,574 120

> 6,843,733 1,080,051 1,622,818 4,140,865

i Co

950,477 1,622,818 4,140,865

129,574 0

σiα 4 5

Internal Loads Lights People Misc

Sub Total ==> Infiltration FIDOR Partition/Door Wall Cond

0 0 2,427,652

7,824

0

000

0

Adjacent Floor

Glass Splar Glass/Door Con

2,141,427 272,232 13,993 0

0 7,824

2,141,427 272,282 21,817 21,817 0 0 0 2,435,476

000

00

Root Cond Skylite

Skylite

000

0000

Ret. Fan Heat Duct Heat Pkup Underfir Sup Ht Pkup AHU-5 Ov/Undr Sizing Exhaust Heat Sup. Fan Heat Main Clg Aux Clg Opt Vent Ceiling Load Ventilation Load Project Name: Total Dataset Name Grand Total ==> Supply Air Leakage nternal Loads Glass Splar Glass/Door Col Skylite Solar Skylite Cond Dehumid. Ov Sizing Adj Air Trans Heat Misc People Lights Floor invelope Lg Sub Total ==> Infiltration Partition/Door Wall Cond Roof Cond Sub Total ==> Adjacent Floo Peaked at Time: Outside Air: 204.7 0.0 0.0 204.7 Total Capacity ton MBh 75AMES_TRACE.TRC 75 Ames Lab/Research Space Sens. + Lat. COOLING COIL PEAK 591,859 73,024 137,330 381,305 2,456.3 0.0 0.0 798,273 2,458.3 204,345 181,574 21,479 1,292 0 Btu/h 2,268 0 000 Plenum Sens. + Lat Sens Cap. MBh OADB/WB/HR: 88 / 74 / 105 COOLING COIL SELECTION 1,323.6 0.0 0.0 17,958 0 -7,441 ŗ, Btu/h 9,001 268 958 753 753 0 00 0 0000 Mo/Hr: 7 / 18 Coil Airflow 2,456,267 1,505,492 143,502 0 0 32,288 0 0 90,982 137,330 381,305 0 181,574 21,479 205,098 609,617 -7,441 2,045 0 Btu/h Net Total 00 0 00 0.0 0.0 Of Total Percent 100.00 Enter DB/WB/HR °F °F gr/lb (%) 20 23 4 8 6 œ 00000000 00 74.0 0.0 CLG SPACE PEAK 105.0 0.0 Space Sensible 71,943 68,304 381,305 521,552 206,488 7,419 739,013 215,253 Mo/Hr: 7 / 11 OADB: 82 1.348 0 Btu/h 0 00 0 00 0 System Checksums By ACADEMIC Percent Of Total 51.0 50.9 0.0 0.0 0.0 0.0 100.00 ' Grand Total ==> °F °F gr/lb 28 (%) 0 Exhaust Heat OA Preheat Diff. RA Preheat Diff. Additional Reheat 7 52 e 10 28 0 0 0 00 00 Adj Air Trans Hea Ventilation Load Ov/Undr Sizing Ceiling Load Supply Air Leakage Underfir Sup Ht Pkup Internal Loads Glass Solar Glass/Door Cond Skylite Solar Skylite Cond Roof Cond Lights People Sub Total ==: Sub Total ==> Misc Infiltration Floor Partition/Door Wall Cond Adjacent Floor 55.4 0.0 Int Door ExFlr Roof Wall Floor Part Ext Door Gross Total HEATING COIL PEAK Space Sens Space Peak 20,817 10,375 -120,092 -121,474 0 -112,788 -7,304 AREAS -1,382 0 0 Mo/Hr: Heating Design OADB: 9 0 0 Btu/h 0 0 00 00 00 0 5,984 Glass 0 0 16,708 -1,009,855 -1,900,709 -112,788 Coil Peak -783,564 Tot Sens -123,999 Variable Volume Reheat (30% Min Flow Default) (%) 0 8 0 Btu/h TRACE® 700 v6.2.8 calculated at 05:52 AM on 10/12/2012 00 0 0 0 c 00 Humidif Opt Vent Main Htg Aux Htg Preheat Reheat Alternative - 1 System Checksums Report Page 2 of 2 Total Of Total Percent 100.00 -0.88 53.13 0.00 0.00 41.22 0.00 0.00 0.00 6.52 0.00 0.00 0.59 0.00 0.00 (%) HEATING COIL SELECTION Btu/hr-ft² No. People Auxiliary Leakage Dwn Leakage Ups Exhaust Rm Exh Fn MtrTD Fn BldTD Fn Frict Ra Plenum Return Ret/OA ft²/ton Return cfm/ft² Terminal Main Fan SADB cfm/ton % 0A MinStop/Rh nfi AHU Vent Nom Vent Sec Fan Diffuser -1,534.3 -259.1 0.0 Capacity MBh -1,916.9 -382.6 0.0 ENGINEERING CKS 0.0 TEMPERATURES AIRFLOWS Coil Airflow Cooling 100.0 Cooling 55.0 32,761 11,199 0 0 11,199 0 1.57 160.05 101.70 117.99 275 Cooling 31.723 31.723 32,761 32,761 32,761 11,199 32,761 32,761 75.4 75.4 87.5 1,039 0.4 2.7 0 0 0 9.0 51.0 51.0 0.0 0.0 Heating 100.0 0.54 ۴Щ Heating 81.7 70.4 9.0 0.0 0.0 0.0 Heating -92.08 0 11,199 10,807 10,807 392 11,199 11,199 11,199 11,199 11,199 51.0 0.0 81.7 0.0 ŕ 0

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Nathaniel J. Mooney Mechanical Dr. William Bahnfleth Technical Report Two 10/12/12

2012