## The Palestra Building London, England



Architectural Renderings compliments of Alsop Architects

# **Technical Assignment 2**

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### I. Executive Summary

The purpose of this report is to take a closer look at the mechanical structures of the Palestra Building looking at the design's environmental consciousness according to the LEED program, power consumption densities according to ASHRAE Standard 90, lost rentable space due to mechanical systems, fuel utilization data, emissions, and load and energy analysis. A comprehensive analysis can then be completed with respect to 'the bottom line': money. And comparisons can be made with similar projects of scope and size to ensure efficiency on the project.

The Palestra Building was designed to qualify for a 'Very Good' rating on the BREEAM scale, which is the UK's equivalent to the US's LEED initiative. Palestra received 57% of the points on the BREEAM scale (57points of a possible 90 points), but only received 42% of the points (29 of 69 points) according to LEED. With 29 points the Palestra Building is certified as a LEED building, but it does not qualify for the Silver, Gold, or Platinum certifications.

The envelope was found to be compliant with ASHRAE Standard 90.1. The Palestra Building was found to have 44.3% glazing on its façade which is less than the 50% maximum as stated in Standard 90. The façade's shading coefficients were also calculated with the maximum values for the North façade being 0.36 and all other sides being 0.25. The glazing on all sides of Levels 0-8 (the 'Bottom Box') and the North side of the Levels 9-12 (the 'Top Box') complied with the Standard, while the South/East/West facing areas on Levels 9-12 did not pass with a value of 0.34 > 0.25.

The lighting consumption of Palestra was also calculated according to ASHRAE Standard 90. According to the 'Space by Space' method outlined in the Standard, only four of the six typical spaces divided by activity passed. This included the water closets, reception area, plant room, and corridors. The spaces that did not pass were the Office Space (15.75 W/m<sup>2</sup> > 11.83 W/m<sup>2</sup>) and below grade Car Park ( $3.5W/m^2 > 2.15W/m^2$ ). According to the 'Building Area Method' analysis, the power overall lighting power density for the building I 14.75 W/m<sup>2</sup> which is significantly greater than the 10.7 W/m<sup>2</sup> (1.0 W/ft<sup>2</sup>) maximum value outlined in Std. 90. The Palestra Building does not comply with ASHRAE Standard 90's lighting power density regulations.

The Palestra Building has a rooftop chiller plant, a basement boiler plant, and an additional major mechanical space on the ground level to service the lobby area. It was found that 10.56% (3450.11 square meters) of the building's gross internal area is lost due to these systems. The design team was aiming for a value between 6 and 11% for mechanical spaces, so while this is on the higher end of the range it is still considered 'good design.'



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The Palestra Building's mechanical systems contain 4 gas-fired boilers, where three run at full capacity and one is for redundancy. There are also 7 packaged chillers, with 6 running at full capacity. Each chiller has an electrical consumption of 186kW. The total gas intake for the Palestra Building is 212 m<sup>3</sup>/h. Through a full building simulation using Carrier's Hourly Analysis Program (HAP) version 4.20, it was found that the design tonnage and supply rate (cfm) per air handling unit were comparable with the HAP output. However the ventilation rates for the units serving the office spaces according to HAP were double the rate of the design flow. This suggests a difference between the American and British building assumptions and will be discussed further in the conclusion.

The design peak loads for the Palestra Building are 1796kW (heating), 3871kW (cooling), and 3051kW (electrical). The natural gas intake is sized at 212 m<sup>3</sup>/h, providing 6.64E+06 Therms per annum. Each of the seven chillers is also sized to provide 157 tons of air conditioning each. To accurately calculate the emissions for the electrical generation mix in the UK, the following percentages were used Coal: 34%, Oil: 2%, Natural Gas: 37%, Nuclear: 23%, Hydro/Wind: 4%. The final pollutant concentrations were found to be 3.49E+4 lbm of SOx, 1.64E+4 lbm of CO2, and 7.24E+6 of NOx.

Finally, the operational and first costs for the mechanical systems were calculated. The building's mechanical first costs came in at  $\pounds 9.9$  million which is 15% of the total project cost. According to the HAP cost analysis the annual operating costs will average  $\pounds 200,000$  annually. These values are based on the assumption that the building owners will choose to use British Gas as their electrical and gas supplier. With such a large commercial consumer, the nominal rate could improve.



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## II. Background

The mechanical systems in the Palestra Building include the following:

• Cooling

Cooling is provided through a chiller plant located on the roof and consisting of seven packaged air-cooled chiller units, six of which run at full load daily, while the seventh serves as a backup unit. These units run the building's chilled water system fed to the fan coil units and cooling coils in the air handling plant. The primary and secondary constant temperature pumps and circuits are located on the room next to the chiller units.

• Heating

Heating is provided through a gas-fired central boiler. The boiler room is located in the basement, and runs on four boilers, three of which run at 100% to met the daily demands while the fourth is a backup during times of maintenance or it can be used as a 'booster boiler' to generate the morning warm-up. These boilers service a low temperature hot water system fed to AHU ventilation systems, fan coil units, and heater batteries.

• Humidification

The Palestra Building is located in London, England, a location where humidity levels are not a critical concern for 60% of the year. However, during the winter months when the humidity drops down occupants can begin to experience dry eyes and throats, similar to the symptoms of Sick Building Syndrome (SBS). To maintain the humidity level between 35-65% there is a combination of chilled ceilings and the fan coil units with a VAV system.



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### III. LEED Analysis

The Leadership in Energy and Environmental Design standards for rating Green Building Design is the American document that sets the national standard for Green Buildings. The aim of the LEED program is to encourage an improvement in the occupant well-being, environmental performance, and the economic returns of buildings through innovative standards and technologies. Green design is also commonly known as Sustainable Design, where a strong emphasis is placed on the ability of the current design to be able to adapt to the future needs of the building and its occupants. This will increase the building's life span and thus the returns that the owner can expect on his investment.

The LEED rating system is a point system based characteristics in six main areas: sustainable sites, water efficiency, energy and atmosphere, materials and resources, and indoor environmental quality. Depending on your attention to these areas in the design a building can achieve up to 69 points.

### **LEED Rating System**

26-32 points: certified as a LEED Building33-38 points: Silver certification,39-51 points: Gold certification52-69 points: Platinum certification

The Palestra was not designed to meet the LEED standards; however it was designed to the UK equivalent for Non-Residential buildings, BRE's Environmental Assessment Method (BREEAM). Under the BREEAM Palestra received a 'Very Good' Rating. It is important to note that while a main design objective for this project was to obtain a 'Good' or 'Very Good' rating on the BREEAM scale. BREEAM places more emphasis on transportation to the site, and with the Palestra Building being 500m from a tube stop, many additional points were gained for BREEAM that do not apply to LEED.

Palestra is being scored under the LEED design standard as well as part of an ongoing study into the similarities and differences between the building design codes in the US and the UK.

Table 3.1 shows the results of the LEED analysis. The Palestra Building received 29 points out of a possible 69, gaining LEED certification.





Table3.1 LEED Certification Analysis						
Palestra Building						
		Possible	Points			
Credit No.	Category	Points	Received	Comments		
SUSTAIN	ABLE SITES	14				
Prereg 1	Erosion & Sediment Control	Required				
1	Site Selection	1	1	Located in Central London		
				The development has made efficient use of the site with a		
2	Urban Redevelopement	1	1	high density of people accommodated on the site.		
	· · · · · · · · · · · · · · · · · · ·			The development makes use of a large brown-field site		
3	Brownfield Redevelopement	1	1	which helps reduce pressure to use green-field sites.		
				Central location of the development near to public		
	Alt Transport: Public Transport			amenities such as shops transport links, local health		
4.1	Arrace	1	1	centres leisure facilities, communication services, bospitals and cultural facilities		
4.1	Alt Transport: Biovole Storage &	· ·		nospitais and cultural racilities.		
12	Changing Rooms	1	1	Secure, covered spaces for hisvales		
4.2	Alt Transnort: Alt Fuel Vehicles	1		Secure, covered spaces for bicycles.		
4.5	Alt Hansport. Alt I der Verificies			Secure covered spaces for bicycles and cars are		
4.4	Alt Transport: Parking Capacity	1	1	provided.		
	Reduced Site Disturbance:			1		
5.1	Protect/Restore Open Space	1	0			
	Reduced Site Disturbance:			Given the multi-storey nature of the development		
5.2	Development Footprint	1	1	schemes this objective is achieved.		
	Stormwater Management: Rate and			A Sustainable II than Drainage Sustam has been installed to		
6.1	Quantity	1	1	reduce storm-water run-off by more than 50%.		
				The primary role of the site drainage scheme will be to		
				ensure the quality of site runoff and the attenuation of		
				runoff on site in order to reduce peak flows and		
6.2	Stormwater Management: Treatment	1	1	suspended solids in runoff discharge.		
7.1	Heat Island Effect: Non-Roof	1				
7.2	Heat Island Effect: Roof	1				
				to reduce the amount of light spillage to comply with the		
				planning requirements, the amount of light being emitted		
				reduced which will require for some of the huminaires		
				adjacent to the south facade to be switched off at night		
				between 7pm and 7am. The effect of this will be to keep		
8	Light Pollution Reduction	1	1	the lights spillage on Rowland Hill house down to 1 hix		
WATER E	FFICIENCY	5				
	Water Efficient Landscaping: Reduce					
1.1	by 50%	1	0			
	Water Efficient Landscaping: No		_			
12	Potable Use or No Irrigation	1	n			
	· · · · · · · · · · · · · · · · · · ·		-	Rainwater collection scheme, harvesting rainwater from		
				the roof for flushing WCs. Waste generated during		
				building operation is being managed and reduced by		
_				waste-stream management, including: the separation,		
2	Innovative Wastewater Technologies	1	1	storage and recycling of waste.		
				The demand for water is being reduced through		
21	Water Lleo Reduction: 20% reduction	1	1	measures including: spray taps and a comprehensive leak		
<u> </u>	vvater Use Reduction: 20% reduction			detection system Water efficient appliances have the notential of metricing		
				the amount of water consumed by as much as 70% in		
3.2	Water Use Reduction: 30% reduction	1	1	comparison to standard fittings and appliances.		





ENERGY	& ATMOSPHERE	17		
Prereq 1	Fund. Bldg. Systems Commisioning	Required		
Prereq 2	Min. Energy Performance	Required		
	<b>.</b>			CFC-free materials For the areas where refrigerants are
				specified, these will be of zero ODP (Ozone Depleting
				Potential). Also, the intention will be for the GVVP (Global
	CFC Reduction in HVAC&R			Warming Potential) to be as low as possible, to minimise
Prereq 3	Equipment	Required		the impact on the environment.
				Measures for reducing energy demand during the
1	Ontimiza Energy Derformence	1 to 10		operation of the development include: centralised plant to
21	Denouveble Energy Ferformance	1 10 10	0	improve energy eniciency
2.1	Renewable Energy, 5%	1	0	
2.2	Renewable Energy, 10%	1	U	
2.3	Renewable Energy, 20%	1	U	
3	Additional Commissioning	1		
				The chillers used in the building contain refrigerants with
				an Ozone Depletion Potential of zero. • The bollers are
				uttra-low-INUX-emitting. Reducing the emission of NUX
				gases (various oxides of hitrogen) reduces the
4	Ozone Depletion	1	1	generation of acid rain and local air poliution and impact op climate chapge
				Refrigerant leak-detection system is installed to reduce
5	Measurement & Verification	1	1	the risk of pollution resulting from leaks
6	Green Power	1	n n	
MATERIA	IS & RESOURCES	13	0	
	ES a RESOURCES	15		<b>H</b>
Dravage 1	Storage and Collection of Decualables	Demuired		Ilrovision of storage space for recyclable materials (such
Frerey I	Storage and Collection of Recyclables	Required		as cans, cups, paper).
	Building Reuse: Maintain 75% of			
1.1	existing shell	.]	U	
	Building Reuse: Maintain 100% of		_	
1.2	existing shell	1	0	
	Building Reuse: Maintain 100%			
1.3	existing shell and 50% non-shell	1	0	
				Management of waste: waste segregation and disposal
				has been undertaken during the construction phase.
	Construction Monorament:			During operation, staff will be encouraged to recycle
2.4	Construction waste Management.	4	4	waste through the provision of appropriate collection
Z.1	Divert 50%		- 1	facilities on site.
	Construction vvaste Management:			
2.2	Divert 75%	1		
				Recycled aggregate (crushed concrete) has been used in
				ine pilling mailbisposal of waste will is in line with equivoprophetal good practice, and potential relies of
31	Resource Reuse: Snecify 5%	1	1	environmental good practice, and potential re-use of materials before disposing them is considered
3.1	Pecource Peuse: Specify 10%	1	-	materials before alsposing them is considered.
J.2	Tresource rreuse. Opecity 1070	1		All unwanted materials from the site during construction
				will be recycled or disposed of in a way that is
				environmental good practice and compliant with
4.1	Recycled Content: Specify 5%	1	1	regulations.
4.2	Recycled Content: Specify 10%	1		-
	Local/Regional Materials: 20%			Materials were calented for long life and low maintenance
5.1	Manufactuered locally	1	1	and where possible were sourced locally
0.1	Local/Regional Materials: of 20% in			and, make possible, wele sourced locally.
60	MPc5 1 50% Harvested Locally	1		
Ω	Panidly Danawahla Matariala	1		
0	rtapiury rtenewable Materials			All solid timber and timber namel products were obtained
7	Certified Wood	1	1	from sustainable, well-managed sources.





Prereq 1         Minimum IAQ Performance         Required           Prereq 2         Control         Required         0           1         Carbon Dioxide Monitoring         1         0           2         Vertilation Effectiveness         1         ASHRAE 129-1997           2         Construction IAQ Mgmt Plan: During         1         1         1           3.1         Construction IAQ Mgmt Plan: Before         0         0         1           3.2         Occupancy         1         1         1         1           0         Construction IAQ Mgmt Plan: Before         0         Early and comparation of the anytic material completion the design team will explain and demonstrate the practical completion the design team will explain and demonstrate there anytic on anytic on any service of the uniting of anytic on the design team will explain and demonstrate there anytic on the design team will explain and demonstrate there anytic on the design team will explain and demonstrate there anytic on the design team will explain and demonstrate there anytic on team anytic team will be anytic on any service of team anytic on team anyte team anytic on team anytic on team anytic on team any	INDOOR	15			
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gained the maximum REEAM credits available for use of low-environmental impact construction materials. The use of toxic and corone-depleting materials has been avoided.         4.1       and Sealants       1       1       embodied emargy, zero toxicity         4.2       Low-Emitting Materials: Paints       1       1       embodied emargy, zero toxicity         4.3       Low-Emitting Materials: Carpet       1       1       embodied emargy, zero toxicity         4.3       Low-Emitting Materials: Carpet       1       1       1         4.4       Wood       1       1       1         6.1       Controllability of Systems: Perimeter       1       1       Fully integrated Building Management System         6.2       Perimeter       1       1       Fully integrated Building Management System         7.1       ASHRAE 55-1992       1       1       Emergy-efficient lighting and controls. Local control of the internal zone control of gabe by means of internal blinds.         7.2       Monitoring System       1       1       Fully integrated Building Management System         7.2       Monitoring System       1       1       Fully integrated Building Management System         7.2       Monitoring System       1       1       Fully integrated Building Management System         8.1       spaces					Environmentally friendly and healthy materials: the building
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4.4       Wood       1       1         4.4       Wood       1         Indoor Chemical and Pollutant Source       1         5       Control       1         6.1       Controllability of Systems: Perimeter       1         7.1       Controllability of Systems: Non-       1         6.2       Perimeter       1         7.1       ASHRAE 55-1992       1         7.1       ASHRAE 55-1992       1         7.2       Monitoring System       1         1       Thermal Comfort: Permanent       1         7.2       Monitoring System       1         1       The façade would allow sufficient daylight to enter the space so that for a high percentage of the time the electric lighting in the perimeter areas could be switched off if, spaces         8.1       spaces       1       0         1.1       Innovation in Design       1       1         1.2       Innovation in Design       1       1         1.3       Innovation in Design       1       1         1.4       Innovation in Design       1       1         1.3       Innovation in Design       1       1         1.4       Innovation in Design       1       1 </td <td>4.2</td> <td>Low-Emitting Materials: Carnet</td> <td>1</td> <td>1</td> <td>construction a during occupation</td>	4.2	Low-Emitting Materials: Carnet	1	1	construction a during occupation
4.4       Wood       1         Indoor Chemical and Pollutant Source       1         5       Control       1         6.1       Controllability of Systems: Perimeter       1         6.1       Controllability of Systems: Non-       1         6.2       Perimeter       1         Thermal Comfort: Comply with       1       1         7.1       ASHRAE 55-1992       1         Thermal Comfort: Permanent       1       Energy-efficient lighting and controls. Local control of the internal environment has been provided for occupants wherever possible, including local control of glare by means of internal blinds.         7.2       Monitoring System       1         1       1       The façade would allow sufficient daylight to enter the space so that for a high percentage of the time the electric lighting in the perimeter areas could be switched off if, resulting to energy savings.         Daylight & Views: Views for 90% of 8.2       0       0         Staces       1       0         INNOVATION & DESIGN PROCESS       5       1         1.3       Innovation in Design       1         1.4       Innovation in Design       1         1.3       Innovation in Design       1         2       LEED Accredited Professional       1         2	4.5	Low-Emitting Materials: Carpet	I	1	
4.4       Wood       1         Indoor Chemical and Pollutant Source       1         5.1       Controllability of Systems: Perimeter       1         6.1       Controllability of Systems: Non-       1         6.2       Perimeter       1         Thermal Comfort: Comply with       1       Fully integrated Building Management System         7.1       ASHRAE 55-1992       1         Thermal Comfort: Permanent       1       Energy-efficient lighting and controls. Local control of the internal environment has been provided for occupants wherever possible, including local control of glare by means of internal blinds.         7.2       Monitoring System       1         Daylight & Views: Daylight 75% of 8.2       5       5         1       Innovation in Design       1       0         INNOVATION & DESIGN PROCESS       5       1       0         1.1       Innovation in Design       1       1         1.3       Innovation in Design       1       1         1.4       Innovation in Design       1       1         2       LEED Accredited Professional       1       1	4.4	Wood	1		
5       Control       1         6.1       Controllability of Systems: Perimeter       1       1         6.2       Perimeter       1       1         7.1       ASHRAE 55-1992       1       1         7.1       ASHRAE 55-1992       1       1         7.2       Monitoring System       1       1         8.1       spaces       1       1       1         8.1       spaces       1       1       1       1         INNOVATION & DESIGN PROCESS       5       1       1       1         1.1       Innovation in Design       1       1       1         1.2       Innovation in Design       1       1       1         1.2       LEED Accredited Professional       1       1       1         2       LEED Accredited Professional       1       1       1	4.4	Indeer Chemical and Pollutant Source	I		
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6.2       Perimeter       1       1       Fully integrated Building Management System         6.2       Perimeter       1       1       Fully integrated Building Management System         7.1       ASHRAE 55-1992       1       1       1         7.2       Monitoring System       1       1       1       1         7.2       Monitoring System       1       1       1       1       1         8.1       spaces       1	0.1	Controllability of Systems: Lenineter		-	i uliy integrated Duliung Management System
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1.11       Profile Cost       1         Image: Control Cost       1       Image: Control Cost	7 1	ASHRAE 55-1992	1		
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Thermal Comfort: Permanent       wherever possible, including local control of lighting, local thermal zone control, and control of glare by means of internal blinds.         7.2       Monitoring System       1         1       1       Internal blinds.         Daylight & Views: Daylight 75% of 8.1 spaces       1       1         Daylight & Views: Views for 90% of 8.2 spaces       1       1         INNOVATION & DESIGN PROCESS       5         1.1       Innovation in Design       1         1.2       Innovation in Design       1         1.3       Innovation in Design       1         1.4       Innovation in Design       1         2       LEED Accredited Professional       1					internal environment has been provided for occupants
Thermal Comfort: Permanent       1       thermal zone control, and control of glare by means of internal blinds.         7.2       Monitoring System       1       1         Daylight & Views: Daylight 75% of       The façade would allow sufficient daylight to enter the space so that for a high percentage of the time the electric lighting in the perimeter areas could be switched off if, resulting to energy savings.         Daylight & Views: Views for 90% of       1       1         Baylight & Views: Views for 90% of       1       0         INNOVATION & DESIGN PROCESS       5       1         1.1       Innovation in Design       1         1.2       Innovation in Design       1         1.3       Innovation in Design       1         1.4       Innovation in Design       1         2       LEED Accredited Professional       1					wherever possible, including local control of lighting, local
7.2       Monitoring System       1       1       internal blinds.         Daylight & Views: Daylight 75% of       The façade would allow sufficient daylight to enter the space so that for a high percentage of the time the electric lighting in the perimeter areas could be switched off if,         8.1       spaces       1       1         Daylight & Views: Views for 90% of       1       1       resulting to energy savings.         Daylight & Views: Views for 90% of       1       0       0         INNOVATION & DESIGN PROCESS       5       1       0         1.1       Innovation in Design       1       1         1.2       Innovation in Design       1       1         1.3       Innovation in Design       1       1         1.4       Innovation in Design       1       1         2       LEED Accredited Professional       1       1		Thermal Comfort: Permanent			thermal zone control, and control of glare by means of
Daylight & Views: Daylight 75% of       The façade would allow sufficient daylight to enter the space so that for a high percentage of the time the electric lighting in the perimeter areas could be switched off if,         B.1       spaces       1       1       resulting to energy savings.         Daylight & Views: Views for 90% of       1       0       1       1         B.2       spaces       1       0       1       1         INNOVATION & DESIGN PROCESS       5       1       0       1         1.1       Innovation in Design       1       1       1         1.2       Innovation in Design       1       1       1         1.3       Innovation in Design       1       1       1         1.4       Innovation in Design       1       1       1         2       LEED Accredited Professional       1       1       1         PROJECT TOTALS       69       29       LEED Contified	7.2	Monitoring System	1	1	internal blinds.
Daylight & Views: Daylight 75% of     so that for a high percentage of the time the electric lighting in the perimeter areas could be switched off if,       8.1     spaces     1     1       Daylight & Views: Views for 90% of     1     0       8.2     spaces     1     0       INNOVATION & DESIGN PROCESS     5       1.1     Innovation in Design     1       1.2     Innovation in Design     1       1.3     Innovation in Design     1       1.4     Innovation in Design     1       2     LEED Accredited Professional     1					The façade would allow sufficient daylight to enter the space
Barrier of views. Daylight of views. Daylight 73 vol     Inghting in the perimeter areas could be switched off if,       8.1     spaces     1     1       Daylight & Views: Views for 90% of     1     0       INNOVATION & DESIGN PROCESS     5       1.1     Innovation in Design     1       1.2     Innovation in Design     1       1.3     Innovation in Design     1       1.4     Innovation in Design     1       2     LEED Accredited Professional     1		Daylight & Views: Daylight 75% of			so that for a high percentage of the time the electric
Daylight & Views: Views for 90% of 8.2 spaces     1     1     Pesuting to energy savings.       INNOVATION & DESIGN PROCESS     1     0       1.1     Innovation in Design     1       1.2     Innovation in Design     1       1.3     Innovation in Design     1       1.4     Innovation in Design     1       2     LEED Accredited Professional     1	81	enarge	1	1	ignting in the perimeter areas could be switched off if,
8.2     spaces     1     0       INNOVATION & DESIGN PROCESS     5       1.1     Innovation in Design     1       1.2     Innovation in Design     1       1.3     Innovation in Design     1       1.4     Innovation in Design     1       2     LEED Accredited Professional     1	0.1	Davlight & Views: Views for 90% of	I		resulting to energy savings.
INNOVATION & DESIGN PROCESS     5       1.1     Innovation in Design     1       1.2     Innovation in Design     1       1.3     Innovation in Design     1       1.4     Innovation in Design     1       2     LEED Accredited Professional     1	82	shares	1	Π	
1.1     Innovation in Design     1       1.2     Innovation in Design     1       1.3     Innovation in Design     1       1.4     Innovation in Design     1       2     LEED Accredited Professional     1		ION & DESIGN PROCESS	5	0	
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1.2     Innovation in Design     1       1.3     Innovation in Design     1       1.4     Innovation in Design     1       2     LEED Accredited Professional     1	1.1	Innovation in Design	1		
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			69	29	LEED Cortified



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## IV. Envelope Compliance with AHSRAE Std 90.1

Section 5 of ASHRAE's Standard 90.1-2004 regulates the energy efficiency of a building's envelope by providing minimum requirements for the heat transfer and insulation values of the façade. There are two methods to determine a façade's compliance, one is a Prescriptive Method and the other is a Trade-Off Option. Only the prescriptive method will be used in this analysis.

The Palestra Building is located in London, England. According to Table B-3 and B-4 this puts the building in Zone 4A. Table D-3 gives the number of heating degree days (HDD@65F) to be 5015 and the number of cooling degree days (CDD@50F) to be 1894. These values fall just outside of the thermal criteria set in Table B-4: CDD shall be less than 4500 and HDD shall be less than 3600. However, because the difference is only 515 heating degree days, the values calculated according to Standard 90.1-2004 shall be permissible. A more detailed explanation of the Heat Loss values for each level can be found in Appendix A.

Table 4.1 details the areas of glazing on the façade of the Palestra Building. The glazing design did change somewhat since this breakdown, however the follow diagrams give a good idea of the intricacy of the building envelope.

by type.				
Area #	Description	Framing system	Glazing type (see 5)	Area (m <sup>2</sup> )
1	Ground Floor Glazing	Stick system	с	314
2a	Bottom Box glazing South facade	Unitised frame	A	2,050
26	Bottom box balustrade at terrace level	Unitised frame, custom bespoke units, shaped to meet upper edge of box.	В	505
2c	Bottom Box glazing South façade, void unoccupied areas behind	Unitised frame, custom bespoke units, shaped to meet lower edge of box.	A	684
2d	Bottom Box glazing North façade, acoustic glazing,	As 2a	D	2,050
2e	Bottom Box glazing West façade, acoustic glazing,	Unitised frame, edge detail to account for inward elevation slope	D	842
2f	Bottom Box glazing East facade	Unitised frame, edge detail to account for outward elevation slope	A	772
3	Terrace Glazing	Stick system	С	988
4	Top Box Glazing	As 2a	E	2,988
5	Roof plant enclosure	Proprietary screening system	-	506

Table 4.1



South Elevation



North Elevation



### West Elevation



East Elevation



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### Walls

Table 5.5-4 sets the minimum U-values needed for the envelope. Describing Palestra's design as a 'Metal Building' yields a maximum Uvalue of 0.124 W/m^2K. As shown in Figure 5.1 the Opaque Wall Assembly has a U-Value of 0.34 W/m^2K. The Palestra's design Uvalue is much greater than the maximum value required by Standard 90.1.



Figure 5.1 Typical Wall U-Values

### Roof

According to Table 5 found in Section 2 of Approved Document L, the design Uvalue for Palestra is 0.2W/m<sup>2</sup>K. However, 0.2W/m<sup>2</sup>K is still much greater than the U-Value required by ASHRAE for a 'Metal Building,' 0.065. The roof of the Palestra Building does not comply with ASHRAE Standard 90.1.

### Glazing

Section 5.5 of ASHRAE's Standard 90 concerns the compliance of glazing percentages. It limits the allowable vertical fenestration area to less than 50% of the gross façade area, and the skylight fenestration is limited to 5% of the roof's gross area. The Palestra Building has no roof lights. The façade breakdown is summarized in Table 4.2.

The Palestra Building has 44.3% glazing on its façade and therefore complies with ASHRAE's Standard 90.1. It is important to note that it was not designed to ASHRAE Standards, but rather Approved Document L as published by the Deputy Prime Minister of England. From the building's compliance with both codes, we can assume that the standards follow similar guidelines.

Table 4.2 Palestra Envelope							
Façade Areas							
Ground Floor	Area, m^2						
Insulation	100						
Glazing	314						
Total	414						
% Glazing	75.85%						
Lower Box' Levels 0-8							
Vertical Insulation Strips	1780.9						



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Floor Edge Insulation	
(firestop@200mm	
downstand)	309.3
Glazing	6903
South Facing	2050
North Facing	2050
West Facing	842
East Facing	772
balustrade at terrace level	505
glazing South façade, void unoccupied areas behind	684
Insulation	2090.2
Total	17986.4
% Glazing	38.38%
Top Box' Levels 9-11	
Insulated 700mm upstand	533
Floor Edge Insulation	
(firestop @900mm	
downstand)	895
Glazing	2988
Insulation	1428
Total	5844
% Glazing	51.13%
Terrace	
Glazing	988
Total	988
%Glazing	100.00%
TOTALS	
Total Glazing	11193
Total Insulation	14039.4
Total Area of Façade	25232.4
Total % Glazing	44.36%

### **Solar Heat Gain Coefficient**

Section 9 of ASHRAE Standard 90.1-2004 regards the allowable shading heat gain coefficient (SHGC) for a building façade. The typical U-value for the glazing on the Palestra Building is 1.75.

According to Table 5.5-4 of Standard 90.1-2004, the maximum allowable SHGC factor for the South, East, and West elevations is 0.25, while the maximum SHGC factor is 0.36 for the North Side. Due to the large percentage of glazing on the Palestra Building, it was important for the design team to maintain a SHGC Factor of 0.3 or better. Below are the calculated Shading Coefficients.



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## Table 4.3 Palestra EnvelopeShading Coefficients

Lower Box' Levels 0-8	Area, m^2	Shading Coefficient	All Elevations, 0.25 Max	North Elevation, 0.36 Max
Solid panel	2.4	0		
Blue body tint glazing	3.075	0.35		
Total	5.475	0.20	PASS	PASS
Top Box' Levels 9-12				
Solid panel	0.9	0		
solar control glazing	2.75	0.52		
fritted glazing	1.375	0.32		
total	5.475	0.34	FAIL	PASS

The terrace level has no shading coefficient for its glazing because 80% of its area is shaded by the overhang of 'top box.'

The results listed in Table 4.3 confirms that the SHGC Factor of the Palestra Building's 'Lower Box' of its façade design does meeting ASHRAE Standards on all elevations. However, the coefficient for the 'Top Box' is only acceptable on the North elevation. Therefore, there will be high solar gains on 'Top Box' on the East, West, and South elevations than suggested by the code. The Palestra Building does not meet ASHRAE Standard 90.1.



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## V. Lighting Compliance with ASHRAE Std 90

Section 9 of ASHRAE Standard 90-2004 concerns the lighting design and power consumption of a building. There are two methods of compliance described in this section: the Building Area Method and the Space-by-Space Method. The Space-by-Space Method is a more detailed calculation and designates the power density for each space's function and summing them for the Overall Power consumption, while the Building Area Method is more general and only determined by the Building's total power consumption divided by the area. Both methods will be used in this analysis.

Palestra's primary space function is for office space. However, the final tenants' fit outs have not yet been finalized and are based on an average of 15 W/m<sup>2</sup>. Lighting to the open plan office spaces will be provided using recessed modular fluorescent luminaries, fitted with high frequency control gear and providing brightness management to increase its efficiency. To meet the target power density an efficiency of 3.5 W/m<sup>2</sup>/100lux was maintained throughout the building.

### **Space-by-Space Method**

Table 5.1 summarizes the Space-by-Space lighting density calculations. As you can see only 4 of the 6 spaces passed. The lighting for the office spaces is 33% higher than ASHRAE's suggestion, while the lighting in the car park is 63% higher. Again, these discrepancies could be accounted for by the different codes used for the design. The design of Palestra was based strongly on standards for 'Good Design' outlined in Chartered Institution of Building Services Engineers (CIBSE). However, Palestra does not meet ASHRAE Standard 90 section 9 using the Space-by-Space analysis.

Space	Area, m <sup>2</sup>	Lighting, lux	Efficiency, W/m^2/100lux	Lighting/Area, W/m^2	Lighting, Watts	Std 90, W/ft^2	Std 90, W/m^2	
Office Space	31606	450	3.5	15.75	497794.5	1.1	11.83	Fail
Water Closets	1125	150	3.5	5.25	5906.25	1	10.75	Pass
Reception	772	300	3.5	10.5	8106	1.3	13.4	Pass
Plant Room	2578.31	150	3.5	5.25	13536.128	1.2	12.9	Pass
Car Park	4942	100	3.5	3.5	17297	0.2	2.15	Fail
Corridors	608	200	3.5	7	4256	0.7	7.53	Pass
TOTAL	41631.31				546895.88			

Table 6.1 Lighting Design Loads

Note: The total area calculated for Lighting Load (41,631.31 m<sup>2</sup>) is greater than the Building's office area (37,098 m<sup>2</sup>) because the area of the below grade car park was include for lighting purposes, but does not compute into the gross office area.



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### **Building Area Method**

Power Density = Total Lighting Power/Total Floor Area = 546895.88W/37098m^2 = 14. 74 W/m^2

Using the Building Area Method the Light Power density was found to be 14.74 W/m<sup>2</sup> which is very close to the target density at 15 W/m<sup>2</sup>. However for an office building ASHRAE says the target Lighting Density should be 10.75 W/m<sup>2</sup> (1.0 W/ft<sup>2</sup>). Therefore the Palestra Building Fails the Building Area Method and does not meet ASHRAE Standard 90 section 9.



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### VI. Mechanical Space Impact

### Lost Rentable Space

The Palestra Building is a large scale speculative office building therefore its design was strongly driven by maximizing the net rentable space so that the developers can maximize their return.

		pubb	
		% Area to	Area,
Level	Space	GIA	m^2
Basement	Plant Room	1.98	734.54
Roof	Plant Room	3.72	1380.05
All Floors	Riser		
	Miscillaneous	0.8	296.78
	Public Health	0.3	111.29
	Electrical	0.5	185.49
	Mechanical	2	741.96
All Floors	Core 1	0.31	115.00
	Core 2	0.45	167.30
	Core 3	0.50	183.75
Total		10.56	3450.11
GIA. m^2	37098		

### Table 6.1 Mechanical Space

As shown, 10.5 % of the Palestra Building's gross area is consumed by mechanical space. To ensure that Palestra was maximizing the use of its mechanical spaces in the minimal amount of space the design team compared it's percentage of mechanical space to those of similar projects with a similar size and scope. Analyzing 10 previous projects the mechanical spaces ranged from 6.17-11.98% of the gross area. That places the Palestra within that range, thus ensuring that good design standards were maximized.

### **First Costs**

Equipment	Quantity	Cost
HEATING SYSTEMS		
	37,394	
Gas Supply	m^3	£1,037,744.00
700kw Gas-Fired Boiler	4	£46,600.00
Boiler Flue System	1	£27,780.00
LTHW Pumps	1	£11,715.00

**Table 6.2 Mechanical Firsts Costs** 





	37 394	
Primary Distribution - Heating	m^2	£299.152.00
·····	26.904	
Secondary Distribution - Heating	m^2	£591.888.00
		,
COOLING SYSTEMS		
553kw Air-Colled Chiller Package	7	£359.240.00
CHW Pumps	1	£18,165.00
	37.394	2.0,.00.00
Primary Distribution - Cooling	m^2	£373,940.00
	26,904	,
Secondary Distribution - Cooling	m^2	£1,022,352.00
Fan Coil Units		
Size 15 - Perimeter Office Areas	343	£303,554.00
Size 9 - Internal Office Areas	394	£292,741.00
Size 6 – Lobbies	22	£16.346.00
Carrier 30RH - 39 heat pumps		
(Lobby)	1	£11,700.00
Fan Coils	6	£5,310.00
AIR SYSTEMS		
AHUs – Office	2	£170.000.00
	37,394	
Toilet Extract Fans	m^2	£74,788.00
	37,394	
Supply/Extract Ductwork	m^2	£373,940.00
Constant Volume Box	176	£80,960.00
	26,904	
Secondary Ductwork to Fan Coils	m^2	£1,022,352.00
	1,227	
Basement Car Park Ventilation	m^2	£50,307.00
	1,235	
Plant Room Ventilation	m^2	£56,810.00
1500x1000mm motorised damper		
and grille for smoke clearance	98	£171,500.00
CONTROLS		
Control Installation to Mech		
Systems with Interface	1	£603,860.00
TRANSPORTATION		
1600kg/21 Person passenger lift @		
1.6m/s serving 13 levels	6	£1,440,000.00
1600kg/21 Person passenger lift @		
1.6m/s serving 14 levels	1	£260,000.00
3000kg/40 person goods		
lift@1.6m/s serving 14 levels	1	£170,000.00



Mechanical first costs for this project are £9.9 million which is approximately 15% of the total project's cost of £68 million.



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### VII. Load and Energy Estimates

The system contains 4 gas-fired boilers, where three run at full capacity and one is for redundancy. There are also 7 packaged chillers, with 6 running at full capacity. Each chiller has an electrical consumption of 186kW. The total gas demand for the Palestra Building is estimated to be 212 m<sup>3</sup>/h (6644146 therms). This includes 10% for spare capacity and 32% for pre-heat capacity. The design calculations for the heating and cooling loads can be seen in Appendix B.

In this analysis three of the building's air handling units will tested using Carrier's Hourly Analysis Program version 4.20. The three units being tested are AHU-1 and AHU-2 which together service all of the office space, and AHU-7 which services the ground floor lobby. This decision was made because these areas account for 86% of the building floor area, and all of the exterior spaces. These results are also summarized in Appendix C.

### Assumptions

### **Outdoor temperature**

Winter	-4°C saturated
Summer	29°C db, 20°C wb

### **Internal temperature**

Offices: 22°C +/- 2 Toilets/Stairs (summer) Uncontrolled (winter) 18°C min, 22°C +/- 2

### Air Movement

Winter	0.25m/s max
Summer	0.25m/s max

### **Relative Humidity:**

Uncontrolled. Facility is to be built in to the office air handling units for the future addition of humidifiers.

No allowance to be provided for associated services (power or gas) in base building.

Table 7.1

### AHU-1 (Office Space + Corridors)

	Capacity (ton)	Supply (L/s)	Ventilation (L/s)
Design	157	38813.64	17616
HAP	136.1	38826.99	31858.9



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### Table 7.2

### AHU-2 (Office Space + Corridors)

	Capacity (ton)	Supply (L/s)	Ventilation (L/s)
Design	157	37726.66	17616
HAP	135.4	38590.09	31858.9

Table 7.3

AHU-7 (Reception)			
	Capacity (ton)	Supply (L/s)	Ventilation (L/s)
Design	31	3496.15	2064
HAP	11.3	2271.73	1964

The results of the HAP analysis are compared with the design values on the schedule in Tables 7.1, 7.2, and 7.3. For AHU-1 and AHU-2 the design ventilation is significantly less than what HAP calculated. The design calculations were based on the 'Good Practice' guidelines of 16 L/s/occupant and 12 m^2/occupant as published in the Chartered Institution of Building Services Engineers (CIBSE).



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### VIII. Fuel Utilization Data\ Building Emissions

The past two decades have seen a significant increase in environmentally friendly building designs. And with the predictions that the average temperature of the earth will rise 8 degrees due to Global Warming, great strides are being taken to lessen the effect we have on our environment. Therefore it is important that a building's pollution be analyzed before its construction in order to ensure good fuel utilization and low emissions. The results of this analysis are also instrumental in the determination of a 'Green Building' according to the LEED program. In this section the energy consumption, as well as the emissions from on-site electrical use will be determined.

The Palestra Building is currently under construction in London, therefore there are not any utility summaries or meter readings for the building. The estimated loads calculated by the design team will be used in this section and are summarized in Table 8.1.

	BH proposed Brief		
<b>Tenant Area Electrical Load</b>			
Lighting	15 W/m2	18 VA/m2	
Equipment	30 W/m2	35 VA/m2	
Fan Coil units	6 W/m2	10 VA/m2	
total – Internal	51 W/m2	63 VA/m2	
Total floor area	26677	26677	
Tenant area load	1,361 kW	1,679 kVA	2433 amp
Landlord areas Electrical loads			
Lighting (automatic control)	7 W/m2	8 VA/m2	
General small power	2 W/m2	3 VA/m2	
Ventilation	40 W/m2	50 VA/m2	
Total	49 W/m2	61 W/m2	
Area	10717	10717	$m^2$
Landlord area load	525 kW	651 kVA	943 amp
Mechanical Plant for tenant			
areas			
Chiller Cooling Capacity (each)	553 kW		
Coefficient of Performance	3.3		
Chiller electrical Load (each)	168 kW	186 kVA	270 amp
No. of Duty chillers	6		
Total chiller load	1,005 kW	1,117 kVA	

### Table 8.1 Breakdown of cooling loads

	Rebecca S. All Mechanical Option The Palestra Build London, England	en ling		
10 No. Lifts	120 kW	141 kVA		
Tenant Area Ventilation Flow rate	35.6	m <sup>3</sup> /s		
Tenant Supply & Extract fan load	40 kW	47 kVA		
Total	1,691 kW	1,956 kVA	2835 amp	
Total				
Total	3,051 kW	3,635 kVA	5268 amp	
4 x 1600amp supplies			6400 amp	
Spare capacity		21%	1132 amp	
(Includes 270 amp for additional chiller)			•	

### Total per annum

1113656.81

A full building simulation was performed using Carrier's Hourly Analysis Program, and the detailed results for each air handling unit are summarized in Appendix C.

The expected emissions for the Palestra Building due to electrical use are summarized in Table 6.2 and based on an annual consumption of 1.11E+06 kWh as calculated in Table 8.1. The percentages of fuel used to generate electricity in the UK taken from "National Statistics Online, Social Trend 34." The mass per kilowatt-hour of emissions are based on the average values found in the Electrical Generation mix in the US. Because the building is still under construction and there are no meter readings the data regarding the particulates for each fuel source could not be acquired for this analysis.



Table 8.2 "Electricity Generation: by Fuel used, EU Comparison 2001"

				lbm Pollutant/kWh			Total Ibm Pollut	ant		
Fuel	kWh	% Total	Particulates	SO2/kWh	NO2/kWh	CO2/kWh	Particulates	SO2	NO2	CO2
Coal	3.79E+05	34.00%		1.28E-02	7.41E-03	2.15E+00		4.85E+03	2.81E+03	8.14E+05
Oil	2.23E+04	2.00%		1.54E-02	2.83E-03	2.11E+00		3.43E+02	6.30E+01	4.70E+04
Nat. Gas	4.12E+05	37.00%		1.35E-05	2.54E-03	1.34E+00		5.56E+00	1.05E+03	5.52E+05
Nuclear	2.56E+05	23.00%		0.00E+00	0.00E+00	0.00E+00		0.00E+00	0.00E+00	0.00E+00
Hydro/Wind	4.45E+04	4.00%		0.00E+00	0.00E+00	0.00E+00		0.00E+00	0.00E+00	0.00E+00
Totals	1.11E+06	100.00%		2.82E-02	1.28E-02	5.60E+00		3.14E+04	1.42E+04	6.24E+06
		Taking	g into account	a transmissi	on efficiency	/ of 0.9, tota	I emissions =	3.49E+04	1.58E+04	6.93E+06

A request for the actual mechanical equipment that has been specified for the building has been made, and this analysis will be updated as that data becomes available. Many of the estimations in this analysis could be strongly affected by the efficiency of the boilers, chillers, and cooling towers. For these calculations it was assumed that three of the four boilers were sized to carry an equal amount of the design heating load of 1796 kW that accounted for 10% spare capacity and 32% for preheat capacity (1533 MBH). Based on the energy input and output the overall efficiency was found to be approximately 70% for the boiler.



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The chillers were simulated as W/C Centrifugal systems sized at 187 tons, which is one sixth of the total building cooling load with the seventh chiller sized equally for redundancy. The input power for each chiller was 168 kW as noted in the specifications.

There was very little information regarding the cooling towers. Therefore each cooling was simulated with a fan load at 0.1 kW/ton.

Table 8.3 summarizes the NOx, SOx, and CO2 emissions from the Palestra Building's use of natural gas. These values are based on a flow rate of 212 cubic meters per hour which is equivalent to 2.29E+5 kWh.

Table 8.3 Natural Gas Consumption Emissions

Natural Gas Consumption							
per annum (kW/b)		SO2 (lbm/k\//h)	CO2 (lbm/k\Wh)	NOx (lbm/k\//h)	SO2 (lbm)	CO2 (lbm)	NOx (lbm)
229108.48	(Design)	1.35E-05	2.54E-03	1.34E+00	3.09E+00	5.82E+02	3.07E+05

Table 8.4 summarizes the total building emissions for Electrical and Gas consumption for a year.

### **Table 8.4 Total Energy Consumption Emissions**

	SO2 (lbm)	CO2 (lbm)	NOx (lbm)
Natural Gas and Electricity per annum	3.49E+04	1.64E+04	7.24E+06



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## IX. Annual Building Operating Costs

The operating costs of a building play a very important role when selecting the mechanical system. The final system should have a nice balance between the first costs and the annual operating costs in order to maximize revenue and reduce the payback period. In addition, the environmental impacts of the building should also be analyzed as in section 8 to ensure that as the system gets older and less efficient it will not need to be replaced because it falls below the minimum EPA standards.

The utilities for the Palestra Building have not been finalized due to the fact that it is currently under construction. These utility estimates were found on the website for British Gas, which will most likely be the supplier to the Palestra Building due to their existing connection on the site.

### **British Gas**

Electric £0.1119/kWh (first 900 units) £0.05896/kWh Gas £0.0295/kWh

Dual Fuel Standing Charge: £66.00

The load profile for these calculations was assumed to follow that of a typical office building with occupied levels from 7am – 7pm Monday through Friday, 12pm-5pm on Saturdays, and 12pm-3pm on Sundays and Holidays.

Chart 9.1 shows the breakdown of where all the operating costs being used. As expected the lighting load is the largest at approximately 60% of the operating costs. Typically the cooling tower fans would consumer a bit larger percentage of the building's costs, however only three chillers are online in this analysis.











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Component	Palestra (£)
Air System Fans	2,649
Cooling	6,513
Heating	0
Pumps	0
Cooling Tower Fans	2,480
HVAC Sub-Total	11,642
Lights	121,122
Electric Equipment	75,036
Misc. Electric	0
Misc. Fuel Use	0
Non-HVAC Sub-Total	196,158
Grand Total	207,800

#### Table 9.2 Annual Costs

#### Table 9.3 Annual Costs

	Annual Cost		Percent of Total
Component	(£)	(£/ft²)	(%)
Air System Fans	2,649	0.009	1.3
Cooling	6,513	0.021	3.1
Heating	0	0.000	0.0
Pumps	0	0.000	0.0
Cooling Tower Fans	2,480	0.008	1.2
HVAC Sub-Total	11,642	0.038	5.6
Lights	121,122	0.393	58.3
Electric Equipment	75,036	0.244	36.1
Misc. Electric	0	0.000	0.0
Misc. Fuel Use	0	0.000	0.0
Non-HVAC Sub-Total	196,158	0.637	94.4
Grand Total	207,800	0.675	100.0

Note: Cost per unit floor area is based on the gross building floor area.

Note much of the tenant fit out has not been included in this cost estimate. The additions made by the tenants are expected to add a large energy and heating load to the base estimates here. The additional loads will be handled by Air Handling Units 3 and 4 which are currently serving only the water closets throughout the building.



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The Palestra Building's operating cost is roughly £200,000 which seems quite low for a 37,000 square meter building. However, again these numbers will increase with the additional loads and operation of all the chillers.



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### X. Conclusion

This report took a closer look at the mechanical structures of the Palestra Building looking at the design's environmental consciousness according to the LEED program, power consumption densities according to ASHRAE Standard 90, lost rentable space due to mechanical systems, fuel utilization data, emissions, and load and energy analysis. All of these issues will then be computed with respect to money, the bottom line for most projects, and compared for its efficiency with similar projects of scope and size.

The Palestra Building received 42% of the points (29 of 69 points) according to LEED. With 29 points the Palestra Building is certified as a LEED building, but it does not qualify for the Silver, Gold, or Platinum certifications.

The envelope was found to be compliant with ASHRAE Standard 90.1. The Palestra Building was found to have 44.3% glazing on its façade which is less than the 50% maximum as stated in Standard 90. The façade's shading coefficients for the South/East/West elevations on the Ground-8 floors also did not comply with a value of 0.34 > 0.25 as stated in the Standard. Therefore, Palestra does not meet the ASHRAE glazing requirements.

The lighting consumption of Palestra was also calculated according to ASHRAE Standard 90. Following the 'Space by Space' method outlined in the Standard, only four of the six typical spaces sorted by activity passed. This included the water closets, reception area, plant room, and corridors. The spaces that did not pass were the Office Space (15.75 W/m<sup>2</sup> > 11.83 W/m<sup>2</sup>) and below grade Car Park ( $3.5W/m^2 > 2.15W/m^2$ ). From the design documents it is known that 15 W/m<sup>2</sup> for lighting in office areas was considered to be 'Good Practice' according to CIBSE guides. Therefore, while the design approximately meets the design intent in the UK, it exceeds the maximum values in the US. The 'Building Area Method' confirms this assumption where the overall power density for this office building was found to be 14.7 W/m<sup>2</sup> versus the 10.7 W/m<sup>2</sup> suggested by ASHRAE for an office building.

The Palestra Building was found to have 10.56% of the Gross Internal Area reserved for mechanical systems and spaces. While 10% of the rentable space seems large, the design team went to great lengths to centralize the systems and streamline the cores in order to minimize this value. As stated before they were aiming to achieve a val;ue between 6 and 11%. Due to the fact that the Palestra Building is fully mechanically ventilated, which is unusual in London's moderate climate, it seems appropriate that it is at the higher end of that range.



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The Palestra Building is predicted to have a £200,000 annual operating cost according to the HAP analysis, with a capital cost of £9.9 million for the mechanical systems. However, please note that the Natural Gas price from British Gas of 5.9 pence/kWh does not appear to have been utilized in this HAP analysis. This is most likely due to a linking error in system design within HAP, however this error could not be located. The actual annual operating costs are expected to be much greater for several reasons in addition to the £65,000 natural gas cost per annum. This analysis only accounts for three of the seven air handling units. While the three here account for 86% of the building's floor area, the additional units will increase the operating costs. Brining more air handling units online will also increase the chiller loads which will also affect the costs.

Calculating the electrical generations according to the UK mix of Coal: 34%, Oil: 2%, Natural Gas: 37%, Nuclear: 23%, Hydro/Wind: 4% the Palestra Building was found to have a fairly significant impact on its surroundings. With 34900 lbm of SOx, 16400 lbm of CO2, and 7240000 lbm of NOx the building could take a second look at some emission efficient equipment that could reduce these values. If this design had fallen under the new 2005 Part L Energy Regulations in the UK, they would have to decrease the CO2 emissions by 28% (4952 lbm) which is a significant amount of pollutant.

Palestra was clearly designed with the emphasis on its iconic façade and design. Therefore it is interesting to see how the mechanical side of the design performs and impacts the environment due to the owners desire to keep capital costs low and running costs lower.



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## **XI.** References

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### APPENDIX A

Ground Level			
	Area	Actual U- Value	Rate of heat loss per degree
Element	(m²)	(W/m <sup>2</sup> K)	(W/K)
Exposed Walls	0	0.2	0
Semi – exposed walls and floors	193	0.2	38.6
Glazed Curtain Wall	323	2.1	678.5
Windows	0	3.3	0.0
Roof	0	0.2	0.0
Floor	0	0.2	0.0
Rooflights	0	2.6	0.0
Totals	516		717.10

Level 1			
	Area	Actual U- Value	Rate of heat loss per degree
Element	(m²)	(W/m <sup>2</sup> K)	(W/K)
Exposed walls	0	0.2	0
Glazed Curtain Wall	564	2.1	1183.8
Windows	0	3.3	0.0
Roof	0	0.2	0.0
Floor	0	0.2	0.0
Rooflights	0	2.6	0.0
Totals	564		1183.81

Level 2			
	Area	Actual U- Value	Rate of heat loss per degree
Element	(m²)	(W/m <sup>2</sup> K)	(W/K)
Exposed Walls	0	0.2	0
Semi – exposed walls amd floors	0	0.2	0
Glazed Curtain Wall	915	2.1	1922.4
Windows	0	3.3	0.0
Roof	0	0.2	0.0
Floor	328	0.2	65.6
Rooflights	0	2.6	0.0
Totals	1244		1988





Levels 3-5			
	Area	Actual U- Value	Rate of heat loss per degree
Element	(m²)	(W/m <sup>2</sup> K)	(W/K)
Wall Type 1	0	0.2	0
Wall Type 2	0	0.2	0
Glazed Curtain Wall	2746	2.1	5767.1
Windows	0	3.3	0.0
Roof	0	0.2	0.0
Floor	0	0.2	0.0
Rooflights	0	2.6	0.0
Totals	2746		5767.15

Level 6			
	Area	Actual U- Value	Rate of heat loss per degree
Element	(m <sup>2</sup> )	(W/m <sup>2</sup> K)	(W/K)
Wall Type 1	0	0.2	0
Wall Type 2	0	0.2	0
Glazed Curtain Wall	915	2.1	1922.4
Windows	0	3.3	0.0
Roof	562	0.2	112.4
Floor	0	0.2	0.0
Rooflights	0	2.6	0.0
Totals	1477		2034.8

Level 7			
	Area	Actual U- Value	Rate of heat loss per degree
Element	(m²)	(W/m <sup>2</sup> K)	(W/K)
Wall Type 1	0	0.2	0
Wall Type 2	0	0.2	0
Glazed Curtain Wall	921	2.1	1934.6
Windows	0	3.3	0.0
Roof	284	0.2	56.8
Floor	0	0.2	0.0
Rooflights	0	2.6	0.0
Totals	1205		1991.4





Level 8			
	Area	Actual U- Value	Rate of heat loss per degree
Element	(m²)	(W/m <sup>2</sup> K)	(W/K)
Wall Type 1	0	0.2	0
Glazed Curtain Wall	819	2.1	1720.0
Windows	0	3.3	0.0
Roof	0	0.2	0.0
Floor	0	0.2	0.0
Rooflights	0	2.6	0.0
Totals	819		1720.03

Level 9			
	Area	Actual U- Value	Rate of heat loss per degree
Element	(m²)	(W/m <sup>2</sup> K)	(W/K)
Wall Type 1	0	0.2	0
Wall Type 2	0	0.2	0
Glazed Curtain Wall	907	2.1	1903.9
Windows	0	3.3	0.0
Roof	0	0.2	0.0
Floor	238	0.2	47.6
Rooflights	0	2.6	0.0
Totals	1145		1951.5

Level 10			
	Area	Actual U- Value	Rate of heat loss per degree
Element	(m²)	(W/m <sup>2</sup> K)	(W/K)
Wall Type 1	0	0.2	0
Wall Type 2	0	0.6	0
Glazed Curtain Wall	2720	2.1	5712.0
Windows	0	3.3	0.0
Roof	0	0.45	0.0
Floor	0	0.45	0.0
Rooflights	0	2.6	0.0
Totals	2720		5712.00





Level 11			
	Area	Actual U- Value	Rate of heat loss per degree
Element	(m²)	(W/m <sup>2</sup> K)	(W/K)
Wall Type 1	0	0.2	0
Wall Type 2	0	0.2	0
Glazed Curtain Wall	2720	2.1	5712.0
Windows	0	3.3	0.0
Roof	2676	0.2	535.2
Floor	0	0.2	0.0
Rooflights	0	2.6	0.0
Totals	5396		6247.2



The Palestra Building London, England



Appendix B

Fabric Heating Load	17014	XX 7 /XZ		
fotal Fabric insulation	1/014	W/K		
(ITOIII Appendix H)	2	dag C		
Internal temperature	-5	deg.C		
(Assume identical throughout)	22	deg C		
Total Fabric load	425351	W		
	-20001			
Infiltration Heating Load				
Total Facade area	10800	$m^2$		
Infiltration rate	2.5	m <sup>3</sup> /hr/m2		
temperature difference (as above)	25	К	Indexes	
Volume of infiltration	7.5	$m^3/s$	Puilding Floor height	2.6
Thermal capacity of air	1200	I/m3 K	Air changes per hour	5.0 0.23
Total Infiltration load	225000	W	All changes per nour	0.23
Mechanical Ventilation Heating I	load			
Total floor area	26677	$m^2$		
Occupancy	12	m <sup>2</sup> /occupant		
Ventilation Flow rate	16	1/s/occupant		
Air tempered to	22	deg.C		
External air	-3	deg.C		
Thermal Efficiency of	50	%		
ventilation plant				
Temperature difference	12.5	K		
Ventilation Flow rate	35.6	m <sup>3</sup> /s		
Air thermal Capacity	1200.0	J/m <sup>3</sup> .K		
System losses	10%			
Ventilation heat load	586894	W		
Total Heating Load				
Total Heating Load	1,237	kW	Indexes	
Spare capacity	10%			
Pre-heat period	32%		Building Floor area	26677
Installed Heating Load	1,796	kW	Load per m2 (W/m <sup>2</sup> )	67.3
Breakdown of cooling				
loads				

BH proposed Brief			
Internal Cooling Load			
persons	10 W/m2	m <sup>2</sup> /occupant	
light	15 W/m2	$W/m^2$	

	Rebecca S. Allen Mechanical Option The Palestra Building London, England	
equip	30 W/m2	$W/m^2$
Fan Coil units	6 W/m2	$W/m^2$
total - Internal	61 W/m2	W/m <sup>2</sup>
Environmental Cooling Load		
Room Temperature	22	deg.C
Outdoor temperature	29	deg.C
Difference	7	deg.C
Solar cooling load	25	$W/m^2$ (estimate) *
Fabric cooling load	5	$W/m^2$ (estimate) *
Infiltration cooling load	1.9	$W/m^2$ (estimate) *
Total Environmental	32 W/m2	
Mechanical Ventilation Cooling	g Load	
Total floor area	26677	$m^2$
Occupancy	12	m <sup>2</sup> /occupant
Ventilation Flow rate	16	l/s/occupant
Air tempered to	22	deg.C
External air	29	deg.C
Thermal Efficiency of ventilation plant	50	% (estimate) *
Temperature difference	-3.5	K
Ventilation Flow rate	35.6	m <sup>3</sup> /s
Air thermal Capacity	1200.0	J/m <sup>3</sup> .K
Ventilation cooling load	149391	W (estimate) *
Ventilation cooling load	5.6	W/m <sup>2</sup> (estimate) *
Total		
total W/m2	99	$W/m^2$
Area	26416	$m^2$
Total Cooling Load	2602	W
Sensible Heat Ratio	15%	
System Losses	10%	
Total	3,291 kW	
Proposed chillers	Capacity	Spare
6 x 0.553 MW	3,318 kW	0.81%
7 x 0.553 MW	3,871 kW	17.61%



The Palestra Building London, England



Appendix C – HAP Results

### **Air System Information**

Air System Name	AHU-1
Equipment Class C	W AHU
Air System Type	VAV

## Sizing Calculation Information Zone and Space Sizing Method:

Zone CFM .	Peak zone sensible load
Space CFM	Individual peak space loads

### **Central Cooling Coil Sizing Data**

Total coil load 136.1	Tons
Total coil load 1633.1	MBH
Sensible coil load 1633.1	MBH
Coil CFM at Aug 1400 82278	CFM
Max block CFM at Aug 1400 107034	CFM
Sum of peak zone CFM 107265	CFM
Sensible heat ratio 1.000	
ft²/Ton 1101.4	
BTU/(hr-ft <sup>2</sup> ) 10.9	
Water flow @ 10.0 °F rise 326.79	gpm

### **Supply Fan Sizing Data**

Actual max CFM at Aug 1400 107034	CFM
Standard CFM 106733	CFM
Actual max CFM/ft <sup>2</sup> 0.71	CFM/ft <sup>2</sup>
Outdoor Ventilation Air Data	
Design airflow CEM 67512	CEM

	51312	CEIVI
CFM/ft <sup>2</sup>	. 0.45	CFM/ft <sup>2</sup>

Number of zones	12	
Floor Area	149886.8	ft²
Location London - Heathrow, United	Kingdom	

Calculation Months	Jan to Dec
Sizing Data	Calculated

Load occurs at Aug 1400	
OA DB / WB	°F
Entering DB / WB 79.9 / 65.7	°F
Leaving DB / WB 61.5 / 59.3	°F
Coil ADP	°F
Bypass Factor 0.100	
Resulting RH	%
Design supply temp 61.7	°F
Zone T-stat Check 12 of 12	OK
Max zone temperature deviation 0.0	°F

Fan motor BHP 10.00	BHP
Fan motor kW 7.46	kW
CFM/person 152.05	CFM/person

	DESIGN COOLING		DESIGN HEATING			
	COOLING DATA AT Aug 1400			HEATING DATA AT DES HTG		
	COOLING OA D	0B / WB 80.5 °F	/ 65.8 °F	HEATING OA D	B/WB 25.0 °F	/ 21.0 °F
		Sensible	Latent		Sensible	Latent
ZONE LOADS	Details	(BTU/hr)	(BTU/hr)	Details	(BTU/hr)	(BTU/hr)
Window & Skylight Solar Loads	29255 ft <sup>2</sup>	298809	-	29255 ft <sup>2</sup>	-	-
Wall Transmission	31536 ft <sup>2</sup>	43889	-	31536 ft <sup>2</sup>	86610	-
Roof Transmission	14359 ft <sup>2</sup>	30990	-	14359 ft <sup>2</sup>	28113	-
Window Transmission	29255 ft <sup>2</sup>	24754	-	29255 ft <sup>2</sup>	447602	-
Skylight Transmission	0 ft <sup>2</sup>	0	-	0 ft <sup>2</sup>	0	-
Door Loads	0 ft <sup>2</sup>	0	-	0 ft <sup>2</sup>	0	-
Floor Transmission	5267 ft <sup>2</sup>	0	-	5267 ft <sup>2</sup>	0	-
Partitions	0 ft <sup>2</sup>	0	-	0 ft <sup>2</sup>	0	-
Ceiling	149887 ft <sup>2</sup>	0	-	149887 ft <sup>2</sup>	0	-
Overhead Lighting	225010 W	618123	-	0	0	-
Task Lighting	0 W	0	-	0	0	-
Electric Equipment	139395 W	434250	-	0	0	-
People	444	82290	91020	0	0	0
Infiltration	-	0	0	-	0	0
Miscellaneous	-	0	0	-	0	0
Safety Factor	0% / 0%	0	0	0%	0	0
>> Total Zone Loads	-	1533105	91020	-	562325	0
Zone Conditioning	-	1371550	91020	-	368759	0
Plenum Wall Load	0%	0	-	0	0	-
Plenum Roof Load	0%	0	-	0	0	-
Plenum Lighting Load	0%	0	-	0	0	-
Return Fan Load	82278 CFM	0	-	1073 CFM	0	
Ventilation Load	67512 CFM	241638	-91020	1073 CFM	49460	0
Supply Fan Load	82278 CFM	19893	-	1073 CFM	-5496	-
Space Fan Coil Fans	-	0	-	-	0	-
Duct Heat Gain / Loss	0%	0	-	0%	0	-
>> Total System Loads	-	1633081	0	-	412723	0
Central Cooling Coil	-	1633082	0	-	0	0
Terminal Reheat Coils	-	0	-	-	0	-
Zone Heating Unit Coils	-	0	-	-	412723	-
>> Total Conditioning	-	1633082	0	-	412723	0
Key:	Positiv	ve values are clg	loads	Positiv	ve values are hto	j loads
	Negativ	ve values are hte	g loads	Negati	ve values are clo	g loads

#### **Air System Information**

Air System Name	AHU-2
Equipment Class	CW AHU
Air System Type	VAV

## Sizing Calculation Information Zone and Space Sizing Method:

Zone CFM .	Peak zone sensible load
Space CFM	Individual peak space loads

### **Central Cooling Coil Sizing Data**

Total coil load 135.4	Tons
Total coil load 1624.8	MBH
Sensible coil load 1624.8	MBH
Coil CFM at Jul 1400 81776	CFM
Max block CFM at Aug 1400 106214	CFM
Sum of peak zone CFM 106445	CFM
Sensible heat ratio 1.000	
ft²/Ton 1107.0	
BTU/(hr-ft <sup>2</sup> ) 10.8	
Water flow @ 10.0 °F rise 325.13	gpm

### **Supply Fan Sizing Data**

Actual max CFM at Aug 1400         106214           Standard CFM         105915           Actual max CFM/ft²         0.71	CFM CFM CFM/ft <sup>2</sup>
Outdoor Ventilation Air Data	CEM

Design almow CFIVI	0/512	CFIN
CFM/ft <sup>2</sup>	. 0.45	CFM/ft <sup>2</sup>

Number of zones	12	
Floor Area	149886.8	ft²
Location London - Heathrow, United	Kingdom	

Calculation Months	Jan to Dec
Sizing Data	Calculated

Load occurs at Jul 1400	
OA DB / WB	°F
Entering DB / WB 79.9 / 65.7	°F
Leaving DB / WB 61.5 / 59.3	°F
Coil ADP 59.4	°F
Bypass Factor 0.100	
Resulting RH	%
Design supply temp 61.7	°F
Zone T-stat Check 12 of 12	OK
Max zone temperature deviation 0.0	°F

Fan motor BHP 10.00	BHP
Fan motor kW 7.46	kW
CFM/person 152.05	CFM/person

	D	ESIGN COOLIN	G	C	ESIGN HEATING	G
	COOLING DATA AT Jul 1400			HEATING DATA AT DES HTG		
	COOLING OA D	)B/WB 80.5 °F	/ 65.8 °F	HEATING OA D	B/WB 25.0 °F	/ 21.0 °F
		Sensible	Latent		Sensible	Latent
ZONE LOADS	Details	(BTU/hr)	(BTU/hr)	Details	(BTU/hr)	(BTU/hr)
Window & Skylight Solar Loads	29255 ft <sup>2</sup>	280776	-	29255 ft <sup>2</sup>	-	-
Wall Transmission	31536 ft <sup>2</sup>	38991		31536 ft <sup>2</sup>	86610	-
Roof Transmission	14359 ft <sup>2</sup>	35740		14359 ft <sup>2</sup>	28113	-
Window Transmission	29255 ft <sup>2</sup>	24754	-	29255 ft <sup>2</sup>	447602	-
Skylight Transmission	0 ft <sup>2</sup>	0	-	0 ft <sup>2</sup>	0	-
Door Loads	0 ft <sup>2</sup>	0	-	0 ft <sup>2</sup>	0	-
Floor Transmission	5267 ft <sup>2</sup>	0	-	5267 ft <sup>2</sup>	0	-
Partitions	0 ft <sup>2</sup>	0	-	0 ft <sup>2</sup>	0	-
Ceiling	149887 ft <sup>2</sup>	0	-	149887 ft <sup>2</sup>	0	-
Overhead Lighting	225010 W	618123	-	0	0	-
Task Lighting	0 W	0	-	0	0	-
Electric Equipment	139395 W	434250	-	0	0	-
People	444	82290	91020	0	0	0
Infiltration	-	0	0	-	0	0
Miscellaneous	-	0	0	-	0	0
Safety Factor	0% / 0%	0	0	0%	0	0
>> Total Zone Loads	-	1514924	91020	-	562325	0
Zone Conditioning	-	1363529	91020	-	368882	0
Plenum Wall Load	0%	0	-	0	0	-
Plenum Roof Load	0%	0	-	0	0	-
Plenum Lighting Load	0%	0		0	0	-
Return Fan Load	81776 CFM	0	-	1064 CFM	0	-
Ventilation Load	67512 CFM	241354	-91020	1064 CFM	49083	0
Supply Fan Load	81776 CFM	19921	-	1064 CFM	-5496	-
Space Fan Coil Fans	-	0		-	0	-
Duct Heat Gain / Loss	0%	0	-	0%	0	-
>> Total System Loads	-	1624804	0	-	412470	0
Central Cooling Coil	-	1624803	0	-	0	0
Terminal Reheat Coils	-	0		-	0	-
Zone Heating Unit Coils	-	0		-	412470	-
>> Total Conditioning	-	1624803	0	-	412470	0
Кеу:	Positiv	ve values are clg	loads	Positiv	ve values are hto	J loads
	Negativ	ve values are hte	g loads	Negati	ve values are clo	y loads

#### **Air System Information**

Air System Name	AHU-7
Equipment Class	CW AHU
Air System Type	VAV

## Sizing Calculation Information Zone and Space Sizing Method:

Zone CFM .	Peak zone sensible load
Space CFM	Individual peak space loads

### **Central Cooling Coil Sizing Data**

Total coil load 11.3	Tons
Total coil load 135.2	MBH
Sensible coil load 116.4	MBH
Coil CFM at Aug 1400 4814	CFM
Max block CFM at Sep 1400 5859	CFM
Sum of peak zone CFM 5859	CFM
Sensible heat ratio 0.861	
ft²/Ton 737.3	
BTU/(hr-ft <sup>2</sup> ) 16.3	
Water flow @ 10.0 °F rise 27.06	gpm

### **Supply Fan Sizing Data**

Actual max CFM at Sep 1400         5859           Standard CFM         5843           Actual max CFM/ft²         0.71	CFM CFM CFM/ft <sup>2</sup>
Outdoor Ventilation Air Data Design airflow CFM	CFM

Number of zones	
Floor Area	′ ft²
Location London - Heathrow, United Kingdom	i i

Calculation Months	Jan to Dec
Sizing Data	Calculated

Load occurs at Aug 1400	
OA DB / WB	°F
Entering DB / WB	°F
Leaving DB / WB 57.6 / 56.3	°F
Coil ADP 55.1	°F
Bypass Factor 0.100	
Resulting RH 48	%
Design supply temp 61.7	°F
Zone T-stat Check 1 of 1	OK
Max zone temperature deviation 0.0	°F

Fan motor BHP 10.00	BHP
Fan motor kW 7.46	kW
CFM/person 112.48	CFM/person

	DESIGN COOLING		C	ESIGN HEATIN	G	
	COOLING DATA AT Aug 1400		HEATING DATA AT DES HTG			
	COOLING OA D	B/WB 80.5 °F	/ 65.8 °F	HEATING OA D	B/WB 25.0 °F	/ 21.0 °F
		Sensible	Latent		Sensible	Latent
ZONE LOADS	Details	(BTU/hr)	(BTU/hr)	Details	(BTU/hr)	(BTU/hr)
Window & Skylight Solar Loads	502 ft <sup>2</sup>	8657	-	502 ft <sup>2</sup>	-	-
Wall Transmission	3307 ft <sup>2</sup>	7632	-	3307 ft <sup>2</sup>	9082	-
Roof Transmission	0 ft <sup>2</sup>	0	-	0 ft <sup>2</sup>	0	-
Window Transmission	502 ft <sup>2</sup>	425	-	502 ft <sup>2</sup>	7684	-
Skylight Transmission	0 ft <sup>2</sup>	0	-	0 ft <sup>2</sup>	0	-
Door Loads	0 ft <sup>2</sup>	0	-	0 ft <sup>2</sup>	0	-
Floor Transmission	3809 ft <sup>2</sup>	0	-	3809 ft <sup>2</sup>	0	-
Partitions	0 ft <sup>2</sup>	0	-	0 ft <sup>2</sup>	0	-
Ceiling	3809 ft <sup>2</sup>	0	-	3809 ft <sup>2</sup>	0	-
Overhead Lighting	12470 W	34256	-	0	0	-
Task Lighting	0 W	0	-	0	0	-
Electric Equipment	7725 W	24066	-	0	0	-
People	37	6858	7585	0	0	0
Infiltration	-	0	0	-	0	0
Miscellaneous	-	0	0	-	0	0
Safety Factor	0% / 0%	0	0	0%	0	0
>> Total Zone Loads	-	81895	7585	-	16765	0
Zone Conditioning	-	81199	7585	-	11276	0
Plenum Wall Load	0%	0	-	0	0	-
Plenum Roof Load	0%	0	-	0	0	-
Plenum Lighting Load	0%	0	-	0	0	-
Return Fan Load	4814 CFM	0	-	59 CFM	0	-
Ventilation Load	4162 CFM	14068	11193	59 CFM	2708	-307
Supply Fan Load	4814 CFM	21158	-	59 CFM	-5496	-
Space Fan Coil Fans	-	0	-	-	0	-
Duct Heat Gain / Loss	0%	0	-	0%	0	-
>> Total System Loads	-	116425	18778	-	8488	-307
Central Cooling Coil	-	116425	18778	-	-3180	-307
Terminal Reheat Coils	-	0	-	-	0	-
Zone Heating Unit Coils	-	0	-	-	11668	-
>> Total Conditioning	-	116425	18778	-	8488	-307
Кеу:	Positiv	/e values are clg	loads	Positiv	ve values are htg	loads
	Negativ	ve values are hte	g loads	Negati	ve values are clo	g loads

#### 1. Plant Information:

Plant Name	Palestra
Plant Type	Chiller Plant
Design Weather	London - Heathrow, United Kingdom

### 2. Cooling Plant Sizing Data:

Maximum Plant Load 282.7	Tons
Load occurs at Aug 1400	
ft²/Ton 1089.8	ft²/Ton
Floor area served by plant 308080.3	ft²

#### 3. Coincident Air System Cooling Loads for Aug 1400

Air System Name	Mult.	System Cooling Coil Load ( Tons )
AHU-1	1	136.1
AHU-2	1	135.3
AHU-7	1	11.3

System loads are for coils whose cooling source is ' Chilled Water ' .

#### 1. Unmet Load Statistics

Month	Equipment Capacity is Sufficient (hrs)	Capacity Insufficient by 0%-5% (hrs)	Capacity Insufficient by 5%-10% (hrs)	Capacity Insufficient by >10% (hrs)	Total Hours with Unmet Loads	Total Hours with Equipment Loads
January	30	0	0	0	0	30
February	29	0	0	0	0	29
March	16	0	0	0	0	16
April	95	0	0	0	0	95
Мау	198	0	0	0	0	198
June	263	0	0	0	0	263
July	294	0	0	0	0	294
August	317	0	0	0	0	317
September	310	0	0	0	0	310
October	194	0	0	0	0	194
November	50	0	0	0	0	50
December	47	0	0	0	0	47
Total	1843	0	0	0	0	1843

### Annual Cost Summary

### Table 1. Annual Costs

-	Palestra
Component	(£)
Air System Fans	2,649
Cooling	6,513
Heating	0
Pumps	0
Cooling Tower Fans	2,480
HVAC Sub-Total	11,642
Lights	121,122
Electric Equipment	75,036
Misc. Electric	0
Misc. Fuel Use	0
Non-HVAC Sub-Total	196,158
Grand Total	207,800

#### Table 2. Annual Cost per Unit Floor Area

Component	Palestra (£/ft²)
Air System Fans	0.009
Cooling	0.021
Heating	0.000
Pumps	0.000
Cooling Tower Fans	0.008
HVAC Sub-Total	0.038
Lights	0.393
Electric Equipment	0.244
Misc. Electric	0.000
Misc. Fuel Use	0.000
Non-HVAC Sub-Total	0.637
Grand Total	0.675
Gross Floor Area (ft <sup>2</sup> )	308080.3
Conditioned Floor Area (ft <sup>2</sup> )	308080.3

Note: Values in this table are calculated using the Gross Floor Area.

### Table 3. Component Cost as a Percentage of Total Cost

Component	Palestra (%)
Air System Fans	1.3
Cooling	3.1
Heating	0.0
Pumps	0.0
Cooling Tower Fans	1.2
HVAC Sub-Total	5.6
Lights	58.3
Electric Equipment	36.1
Misc. Electric	0.0
Misc. Fuel Use	0.0
Non-HVAC Sub-Total	94.4
Grand Total	100.0

### Table 1. Annual Costs

Component	Palestra (£)
HVAC Components	
Electric	11,642
Natural Gas	0
Fuel Oil	0
Propane	0
Remote HW	0
Remote Steam	0
Remote CW	0
HVAC Sub-Total	11,642
Non-HVAC Components	
Electric	196,160
Natural Gas	0
Fuel Oil	0
Propane	0
Remote HW	0
Remote Steam	0
Non-HVAC Sub-Total	196,160
Grand Total	207,802

#### Table 2. Annual Energy Consumption

Component	Palestra
HVAC Components	
Electric (kWh)	149,670
Natural Gas (na)	0
Fuel Oil ()	1,246
Propane (na)	0
Remote HW (na)	0
Remote Steam (na)	0
Remote CW (na)	0
Non-HVAC Components	
Electric (kWh)	2,521,820
Natural Gas (na)	0
Fuel Oil ()	0
Propane (na)	0
Remote HW (na)	0
Remote Steam (na)	0
Totals	
Electric (kWh)	2,671,489
Natural Gas (na)	0
Fuel Oil ()	1,246
Propane (na)	0
Remote HW (na)	0
Remote Steam (na)	0
Remote CW (na)	0

### Table 3. Annual Emissions

Component	Palestra
CO2 (lb)	0
SO2 (kg)	0
NOx (kg)	0

### Table 4. Annual Cost per Unit Floor Area

Component	Palestra (£/ft²)
HVAC Components	
Electric	0.038
Natural Gas	0.000
Fuel Oil	0.000
Propane	0.000
Remote HW	0.000
Remote Steam	0.000
Remote CW	0.000
HVAC Sub-Total	0.038
Non-HVAC Components	
Electric	0.637
Natural Gas	0.000
Fuel Oil	0.000
Propane	0.000
Remote HW	0.000
Remote Steam	0.000
Non-HVAC Sub-Total	0.637
Grand Total	0.675
Gross Floor Area (ft <sup>2</sup> )	308080.3
Conditioned Floor Area (ft <sup>2</sup> )	308080.3

Note: Values in this table are calculated using the Gross Floor Area.

#### Table 5. Component Cost as a Percentage of Total Cost

Component	Palestra (%)
HVAC Components	
Electric	5.6
Natural Gas	0.0
Fuel Oil	0.0
Propane	0.0
Remote HW	0.0
Remote Steam	0.0
Remote CW	0.0
HVAC Sub-Total	5.6
Non-HVAC Components	
Electric	94.4
Natural Gas	0.0
Fuel Oil	0.0
Propane	0.0
Remote HW	0.0
Remote Steam	0.0
Non-HVAC Sub-Total	94.4
Grand Total	100.0



	Annual Cost		Percent of Total
Component	(£)	(£/ft²)	(%)
Air System Fans	2,649	0.009	1.3
Cooling	6,513	0.021	3.1
Heating	0	0.000	0.0
Pumps	0	0.000	0.0
Cooling Tower Fans	2,480	0.008	1.2
HVAC Sub-Total	11,642	0.038	5.6
Lights	121,122	0.393	58.3
Electric Equipment	75,036	0.244	36.1
Misc. Electric	0	0.000	0.0
Misc. Fuel Use	0	0.000	0.0
Non-HVAC Sub-Total	196,158	0.637	94.4
Grand Total	207,800	0.675	100.0

Note: Cost per unit floor area is based on the gross building floor area.

 Gross Floor Area
 308080.3
 ft²

 Conditioned Floor Area
 308080.3
 ft²



	Annual Cost		Percent of Total
Component	(£/yr)	(£/ft²)	(%)
HVAC Components			
Electric	11,642	0.038	5.6
Natural Gas	0	0.000	0.0
Fuel Oil	0	0.000	0.0
Propane	0	0.000	0.0
Remote Hot Water	0	0.000	0.0
Remote Steam	0	0.000	0.0
Remote Chilled Water	0	0.000	0.0
HVAC Sub-Total	11,642	0.038	5.6
Non-HVAC Components			
Electric	196,160	0.637	94.4
Natural Gas	0	0.000	0.0
Fuel Oil	0	0.000	0.0
Propane	0	0.000	0.0
Remote Hot Water	0	0.000	0.0
Remote Steam	0	0.000	0.0
Non-HVAC Sub-Total	196,160	0.637	94.4
Grand Total	207,802	0.675	100.0

Note: Cost per unit floor area is based on the gross building floor area

Gross Floor Area	308080.3	ft²
Conditioned Floor Area	308080.3	ft²



### 1. Annual Costs

	Annual Cost		Percent of Total
Component	(£/yr)	(£/ft²)	(%)
HVAC	11,642	0.038	5.6
Non-HVAC	196,158	0.637	94.4
Grand Total	207,800	0.675	100.0

Note: Cost per unit floor area is based on the gross building floor area.

Gross Floor Area	308080.3	ft²
Conditioned Floor Area	308080.3	ft²

#### 1. Annual Coil Loads

Component	Load (kBTU)	(kBTU/ft²)
Cooling Coil Loads	900,005	2.921
Heating Coil Loads	858	0.003
Grand Total	900,863	2.924

#### 2. Energy Consumption by System Component

Component	Site Energy (kBTU)	Site Energy (kBTU/ft <sup>2</sup> )	Source Energy (kBTU)	Source Energy (kBTU/ft <sup>2</sup> )
Air System Fans	116,212	0.377	415,044	1.347
Cooling	285,675	0.927	1,020,268	3.312
Heating	1,246	0.004	1,246	0.004
Pumps	0	0.000	0	0.000
Cooling Towers	108,786	0.353	388,521	1.261
HVAC Sub-Total	511,919	1.662	1,825,078	5.924
Lights	5,312,958	17.245	18,974,848	61.591
Electric Equipment	3,291,426	10.684	11,755,093	38.156
Misc. Electric	0	0.000	0	0.000
Misc. Fuel Use	0	0.000	0	0.000
Non-HVAC Sub-Total	8,604,383	27.929	30,729,941	99.747
Grand Total	9,116,302	29.591	32,555,019	105.671

#### Notes:

1. 'Cooling Coil Loads' is the sum of all air system cooling coil loads.

2. 'Heating Coil Loads' is the sum of all air system heating coil loads.

3. Site Energy is the actual energy consumed.

Source Energy is the site energy divided by the electric generating efficiency (28.0%).
 Source Energy for fuels equals the site energy value.

6. Energy per unit floor area is based on the gross building floor area.

Gross Floor Area	308080.3	ft²
Conditioned Floor Area	308080.3	ft²

#### 1. Annual Coil Loads

Component	Load (kBTU)	(kBTU/ft²)
Cooling Coil Loads	900,005	2.921
Heating Coil Loads	858	0.003
Grand Total	900,863	2.924

#### 2. Energy Consumption by Energy Source

Component	Site Energy (kBTU)	Site Energy (kBTU/ft <sup>2</sup> )	Source Energy (kBTU)	Source Energy (kBTU/ft <sup>2</sup> )
HVAC Components				
Electric	510,673	1.658	1,823,832	5.920
Natural Gas	0	0.000	0	0.000
Fuel Oil	1,246	0.004	1,246	0.004
Propane	0	0.000	0	0.000
Remote Hot Water	0	0.000	0	0.000
Remote Steam	0	0.000	0	0.000
Remote Chilled Water	0	0.000	0	0.000
HVAC Sub-Total	511,919	1.662	1,825,078	5.924
Non-HVAC Components				
Electric	8,604,448	27.929	30,730,172	99.747
Natural Gas	0	0.000	0	0.000
Fuel Oil	0	0.000	0	0.000
Propane	0	0.000	0	0.000
Remote Hot Water	0	0.000	0	0.000
Remote Steam	0	0.000	0	0.000
Non-HVAC Sub-Total	8,604,448	27.929	30,730,172	99.747
Grand Total	9,116,367	29.591	32,555,250	105.671

#### Notes:

1. 'Cooling Coil Loads' is the sum of all air system cooling coil loads.

Heating Coil Loads' is the sum of all air system heating coil loads.
 Site Energy is the actual energy consumed.

4. Source Energy is the site energy divided by the electric generating efficiency (28.0%).

5. Source Energy for fuels equals the site energy value.

6. Energy per unit floor area is based on the gross building floor area.

Gross Floor Area	308080.3	ft²
Conditioned Floor Area	308080.3	ft²