# Pearland Recreation Center and Natatorium Pearland, Texas



# **Technical Report #2**

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## **Section 1: Executive Summary**

This technical report contains a detailed project schedule and structural system cost estimate, general conditions estimate, and site layout plans for four key phases of construction for the Pearland Recreation Center and Natatorium. The report concludes with an overview of the PACE Roundtable Conference.

Pearland's 11 month project schedule begins with the Notice to Proceed on April 20, 2009 and concludes with Substantial Completion on May 12, 2010. The schedule breaks the building into two portions; the recreation center and the natatorium. These halves of the building have significantly different designs, making it reasonable to separate the construction of the building. The natatorium has a glulam structural system and houses a swimming pool while the recreation center uses a steel structural system and features a competitive gym among other athletic courts and rooms.

Structural system construction cost estimate for the building is \$4,427,368.67. This cost estimate was created by taking a typical bay in the recreation center and extrapolating this cost to obtain a cost for the entire building's structural system. Pricing for this estimate was obtained from RS Means 2009 Building Construction Cost Data and contractor quotes. A general conditions cost estimate of \$560,314.50 was also calculated. Project Management expenses were the majority (>60%) of the general conditions cost.

Site layout plans were created for the excavation, foundations, structural framing erection, and enclosures phases of construction. Construction generally progresses from the northwest corner to the southeast corner of the building. No critical logistical issues were apparent. The site is very open with ample space for material staging and storage. Temporary utilities are easily accessible off of Bailey Road on the south side of the site.

An overview of the PACE Roundtable Conference October 14-15, 2009 and some ongoing issues in the construction industry wrap up the report. PACE Roundtable provided an excellent opportunity to interact with industry members. The conference supplied some good potential thesis research topics, such as considering why the selected project delivery method was chosen by the owner and why no sustainable design was implemented into the project.

### Section 2: Detailed Project Schedule

Construction of the Pearland Recreation Center and Natatorium will begin with the Notice to Proceed on April 20, 2009 and conclude with Substantial Completion on May 12, 2010. The complete detailed schedule is available in Appendix 1. To create the construction schedule for the project the building was split into two portions: recreation center and natatorium. This was done because these two portions of the building are very different and will be constructed in a different manner due to the swimming pool and glulam structural system in the natatorium. Table 2.1 – Milestone Date Comparison compares some key construction milestone dates in the recreation center versus the natatorium.

Table 2.1 – Milestone Date Comparison

Milestone	Recreation Center	Natatorium
Notice to Proceed	4/20/2009	4/20/2009
Top Out	8/7/2009	8/30/2009
Dry-In	10/23/2009	12/9/2009
Substantial Completion	5/12/2010	4/28/2010

#### Structure and Enclosure:

Construction of the building's structural system and enclosure is sequenced as shown in Figure 2.2 - Structural and Enclosure Trade Construction Sequence

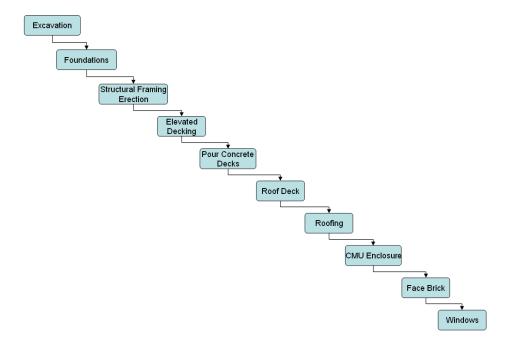


Figure 2.2 – Structural and Enclosure Trade Construction Sequence

### Interiors:

Following 'Dry-In,' a 'parade of trades' construction sequence is applied; that is only one trade works in each space at a time and each trade follows the previous. Figure 2.3 - Interior Trades Construction Sequence shows the order of the interior 'parade of trades'.

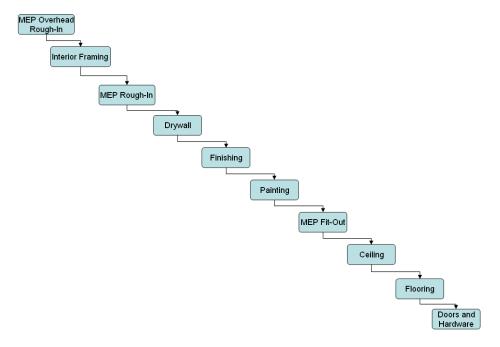


Figure 2.3 - Interior Trades Construction Sequence

Following the interior 'parade of trades' a number of specialty items are installed, such as casework, gym flooring, and gym equipment. See the detailed schedule in Appendix 1 for all activities.

### **Recreation Center:**

Construction of the recreation center progresses counterclockwise through the building in three phases. Figure 2.4 – Recreation Center Construction Phase Locations shows the locations of these three phases.

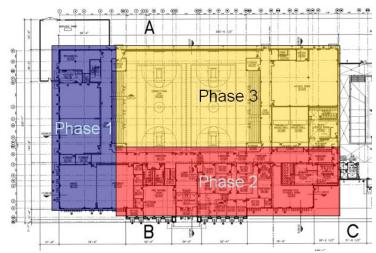


Figure 2.4 – Recreation Center Construction Phase Locations

Second floor activities only have two phases since the gym is double height and the small portion of phase three that has a second level is combined with phase 2 for the second floor.

#### Natatorium:

There is no phasing of construction in the natatorium as there was in the recreation center. Construction sequencing in the natatorium will revolve around the swimming pool construction. See Figure 2.5 – Swimming Pool Construction Sequence for the sequence of swimming pool construction activities.

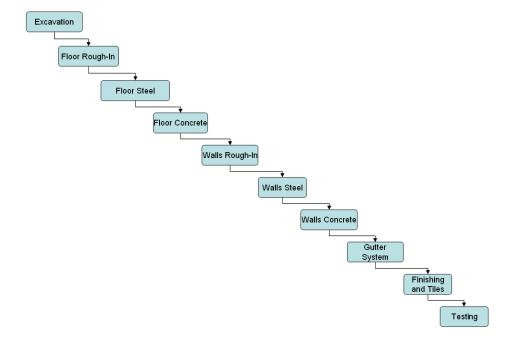


Figure 2.5 – Swimming Pool Construction Sequence

Construction of other portions of the natatorium will be occurring throughout the pool construction; however it is critical that the finishing and tiles in the swimming pool are the last activity to occur in the swimming pool area in order to protect the work. Immediately after this is completed, the pool will be filled with water and testing and chemical balancing will begin.

## Section 3: Site Layout Planning

Site layout for the Pearland Recreation Center and Natatorium is greatly simplified due to a large site. Consistent across all phases of the project are the dumpsters in the northeast corner of the site with a dedicated entrance off of Bailey road for access to empty them, porta-potties in the northeast corner of the parking lot, the construction offices on the east side of the site, the temporary transformer in the southeast corner of the building, temporary utilities running to the southeast corner of the building from Bailey Rd, contractor parking on the south side of the site, and the site entrance off of Bailey road on the south side of the site.

Site layout for the excavation phase of construction is shown in Figure 3.1 – Excavation Phase Site Plan. Excavation will begin from the northwest corner of the building and proceed towards the southeast corner of the building as shown. Dump trucks will arrive and circulate through the site to remove soil as shown.

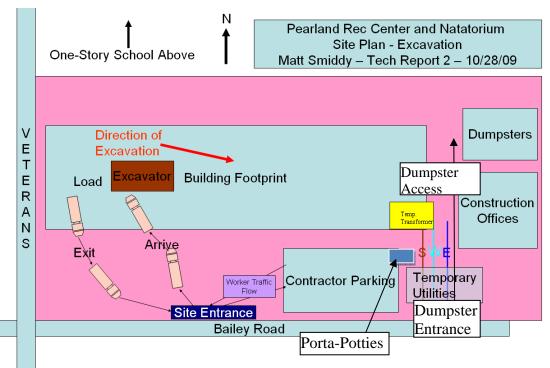


Figure 3.1 – Excavation Phase Site Plan

Figure 3.2 – Foundations Phase Site Plan shows the site layout for the foundations phase of construction. Foundations work will again progress from the northwest corner to the southeast corner of the building. A rebar yard, with access provided for flatbed rebar truck deliveries, is provided in the southwest corner of the site. The pump truck and concrete trucks will circulate as shown. They will only be present on site during concrete pours. The location of the pump truck will move eastward on the site as work progresses. A contractor material storage area is also provided in the southeast corner of the site.

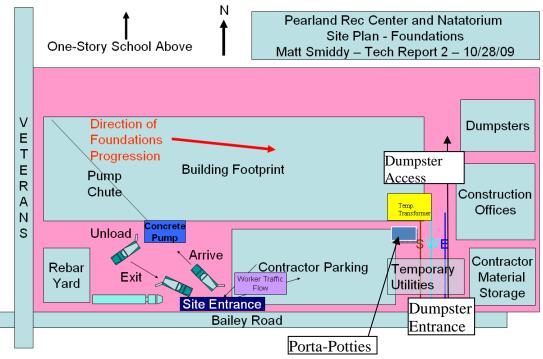


Figure 3.2 – Foundations Phase Site Plan

The project site begins to become more congested as the structural framing erection phase of construction begins. Site layout for this phase is shown in Figure 3.3 – Structural Framing Erection Phase Site Plan. Erection of the steel and glulam will proceed from the west end of the building to the east end. Steel and glulam members will be delivered and unloaded in the shake-out area in the southwest corner of the site. Two cranes will be erecting the steel and glulam on site, one on the north side and one on the south side of the building as shown. Steel joists will be delivered to this shake-out area as well, but will then be moved to the joist shake-out area on the north side of the site to be prepared for final erection. There will be an access point for stocking material to the building located at the southwest corner of the building. This will be done using front loaders.

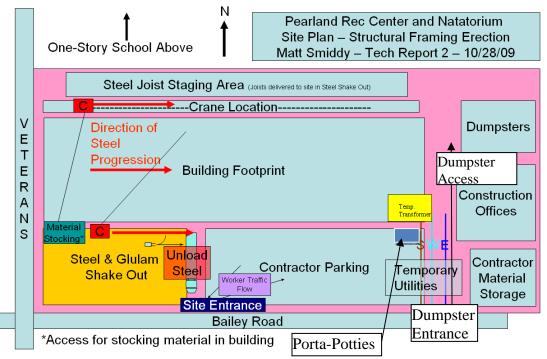
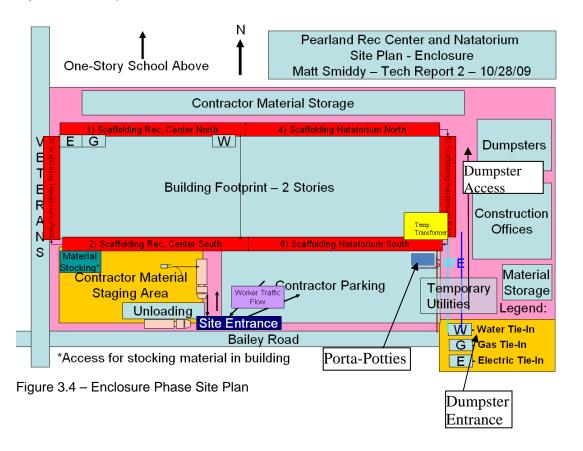


Figure 3.3 – Structural Framing Erection Phase Site Plan

Enclosures is the final phase of construction. Work in this phase will progress in a clockwise direction, first around the recreation center than proceeding to go around the natatorium. There will be a contractor material staging area in the southwest corner of the site. This area will be used by contractors to unload materials from trucks as shown. There are also material storage areas on the north side and in the southeast corner of the site. Materials will again be stocked to the building through the access point at the southwest corner of the building using front loaders. Figure 3.4 – Enclosure Phase Site Plan shows the site layout for this phase of construction.



## **Section 4: Detailed Structural Systems Estimate**

A detailed structural system construction cost estimate for the Pearland Recreation Center and Natatorium project yielded just over \$4,425,000, or about \$42/SF. This cost includes all labor, equipment, and material required for construction of the caissons, concrete, structural steel, steel decking, joists, trusses, wood decking, and glulam structural framing. A break-down of the cost estimate is shown in Table 4.1 – Detailed Structural System Estimate Summary. The complete estimate is available in Appendix 2.

Table 4.1 – Detailed Structural System Estimate Summary

Cost Breakdown Summary						
Dev.	Item	<b>Total Cost</b>				
02465	Caissons	\$526,841.25				
03220	Rebar	\$60,681.51				
03221	WWF	\$18,041.18				
03310	3000 psi concrete	\$145,747.62				
03311	3500 psi concrete	\$36,687.77				
03312	Concrete Finishing	\$15,161.58				
03313	Concrete Forming	\$471,115.84				
03314	Vapor Barrier	\$123,562.53				
03315	5" Concrete Edge Form	\$2,729.14				
03316	3" Pour Stop	\$821.42				
03500	Roof Deck	\$626,272.50				
05100	Structural Steel	\$702,167.12				
05200	Steel Floor Joists	\$390,755.16				
05300	Metal Deck	\$66,784.03				
06100	Wood Trusses	\$170,000.00				
06110	Glulam (Decking, Purlins, and Columns)	\$1,070,000.00				
	Total Cost	\$4,427,368.67				

Pricing for the estimate was obtained using RS Means 2009 Building Construction Cost Data and contractor information. RM Rodgers provided the glulam pricing and Tectum Inc. provided pricing for the Tectum E roof decking system over the recreation center. All other pricing information came from RS Means.

The estimate was created by doing a detailed take-off of a typical bay of the building and extrapolating. Figure 4.2 – Location of Typical Bay Used for Estimate shows the 2520 SF (both levels) area, between gridlines G-J and 1-2, which was used.

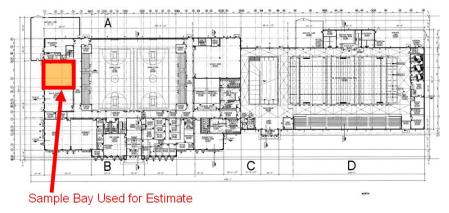


Figure 4.2 – Location of Typical Bay Used for Estimate

#### **Recreation Center:**

Using the total cost estimate obtained from this bay, a cost/SF value was calculated and multiplied by the square footage of the recreation center. This cost/SF did not include the Tectum 'E' roof decking or roof trusses. The cost of these two items were estimated for the entire recreation center then added to the extrapolated cost estimate. See Appendix 2 for the complete detailed cost estimate and Appendix 3 for the hand take-off quantities used to develop this detailed estimate.

### Natatorium:

Modifications had to be made to the cost/SF value to estimate the natatorium's structural system cost since the structural system is glulam instead of steel, like the recreation center. Additionally, there are no elevated slabs in the natatorium. To account for these differences the structural steel and elevated deck costs were subtracted from the recreation center's cost/SF. This new cost/SF was then multiplied by the total square footage of the natatorium. This extrapolated value was added to the glulam columns, purlins, and decking value provided by RM Rodgers for the total natatorium structural system construction cost. See Appendix 2 for the complete detailed cost estimate and Appendix 3 for the hand take-off quantities used to develop this detailed estimate.

Pricing sheets for all RS Means values are available in Appendix 4. These costs include all waste factors.

### **Section 5: General Conditions Estimate**

A general conditions cost of just over under \$2 million was estimated for the Pearland Recreation Center and Natatorium project. This estimate was obtained using pricing from RS Means and EMJ Corporation. See Appendix 5 for the complete estimate.

The general conditions estimate contains 5 portions: project management, temporary facilities, temporary utilities, cleaning, and miscellaneous. Project management and insurance, bond, and O&P are the primary costs in the general conditions, totaling almost \$1.9 million. Temporary facilities includes items such as job office trailers, temporary sanitary facilities, and barricades. All material hoisting (lifts, cranes etc.) and heavy equipment are to be provided by the contractors so it was not necessary to include these items. Temporary utilities consists of costs for temporary electric, water, and telephone during construction. The cleaning section will pay for weekly site clean-up and final building clean-up. A miscellaneous section with items such as hand tools, safety, and blue prints is also included. A 2% bond, 3% insurance, and 10% overhead and profit are also included in the estimate. These percentages are of the total project cost (\$16,786,542 as per Tech #1 estimate).

Appendix 4 contains RS Means cost data that was used for the estimate.

## **Section 6: Critical Industry Issues**

PACE Roundtable 2010 was a great opportunity to hear what is happening in the construction industry. Some of the key topics that were discussed during the conference were energy efficiency in buildings, building information modeling (BIM), and business and networking. There were also panel discussions with industry members regarding some interesting developments in the construction market and with students about communication opportunities in emerging technology. I was unfortunately only able to attend the morning session of the conference on Thursday due to another commitment.

PACE Roundtable 2010 kicked off with a networking reception and dinner on Wednesday, October 14, 2009. The reception was a great opportunity to catch up with the industry members. I was able to have a lengthy conversation with Keith Mondock from Turner Construction, who I will be having a second interview with in a few weeks. We discussed my thesis project and how it was progressing. It was a great conversation to lead into my interview.

At dinner I sat beside John Bechtel, of Pennsylvania State University Office of the Physical Plant. Our dinner conversation included a discussion about the construction of the Millennium Science Complex and some upcoming projects at Penn State. Following dinner, Dr. Riley wrapped up the evening with a brief preview of Thursday's schedule.

Thursday morning began with an industry panel discussion of current construction industry issues. Some interesting topics that were discussed during this session included active market sectors, BIM developments, and strategies contractors were using to cope with the economic conditions. The entire industry is seeing far less work than a year ago and backlog is shrinking. The few projects that are being put out for bid are seeing many more bidders. This large influx of bidders on projects has driven down bid amounts. It was pointed out that these low bidders are frequently small firms getting in over their heads and there will likely be a significant increase in failure among construction companies. Some of the active industry sectors include healthcare, senior living, and energy retrofits. Residential projects were cited as being the most inactive due to the tightened credit markets.

During this panel discussion there was also an interesting discussion about how companies are coping with the downturn in available work. The larger companies stated that the reduction in work has allowed them to spend more resources on research, particularly in BIM. On the contrary, the small firms said they have reduced their progressions in BIM implementation due to shrinking resources and an increased need to focus on marketing and obtaining work. Employee training has also been more active. Firms are seizing the opportunity to educate their employees during the lull. Most importantly, companies have ramped up their marketing efforts. They have not only been marketing to past

and current clients, but also have started seeking out potential clients that they have never worked with before.

Following the industry panel there were three break-out groups with different focus topics: energy and the construction industry, business and networking, and BIM executive planning. I attended the business and networking session facilitated by Chris Magent because I have already been exposed to BIM and energy in buildings in academic classes, however business and networking is a topic I have not had much exposure to.

In the business and networking session the need for diversity in market sectors was emphasized. I found it interesting that one of the methods being used to achieve this was joint-ventures. Joint-ventures have allowed companies that haven't worked in a certain sector to team up with a firm that is established in that sector and obtain experience in the new type of project. At the same time, these joint-ventures have been created to increase bonding capacity and other project requirements such as minority company involvement in project teams. A question was posed regarding the difficulty in obtaining cooperation from both firms in a joint-venture; however from experience it has been noted that as long as both companies have similar values there are no problems because both project teams can focus on the same goal: providing the owner with a quality project.

Another topic that was brought up in the business and networking session was trends in project delivery methods. The industry members all reported that they were seeing a rise in the number of lump sum bids coming in. It was acknowledged that this increase can be primarily attributed to repeat clients no longer having projects, resulting in a shift of the types of clients. It was also mentioned, primarily by Balfour Beatty, that there has been an increase in Design-Build projects due to the increased government work that has been created by the stimulus act. Integrated Project Delivery (IPD) was also discussed during this time. Rob Leicht from DPR Construction joined our discussion at this time to act as an 'expert' in this area since he has done significant research on the topic and DPR is a leader in this delivery method. There was confusion surrounding the definition of IPD. Rob defined this as an 'integrated design-bid-build' contract that is signed by the owner, designer, construction manager, and subcontractor and allocated risk between all parties. The best definition was from Southland Industries: 'A Design-Build project done right.'

Attending the PACE Roundtable gave me some ideas of potential thesis topics. The first idea I may want to pursue would be regarding LEED/Sustainability. My project is completely state funded; however there are no sustainable aspects in the building. I may want to speak with the owner and first determine if there was a reason for this and if not, possibly analyze the implementation of some sustainable aspects into the design as well as the construction. I want to also try

to apply some BIM applications, such as 3-D coordination, into my research; however this may be very difficult since I still have not been able to obtain the 2-D CAD drawings for the project.

Two other issues I may want to investigate involve the project delivery method. It is currently being delivered via a Design-Bid-Build method. I may want to look at what an adjustment in the delivery method may do to the project. The project is also being funded by 3 different sources, however only one of the parties are overseeing the construction of the project. There may be some interesting issues to look at with this 'joint-venture' as well.

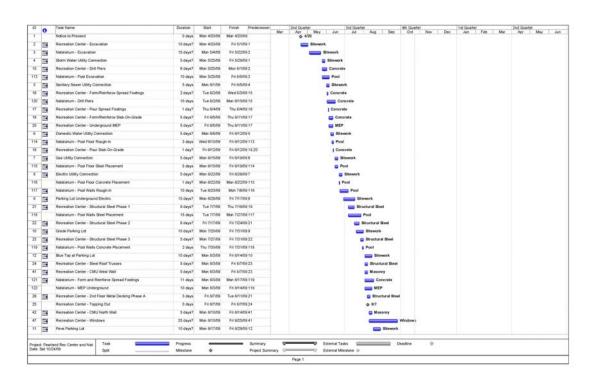
The PACE Roundtable was a great opportunity for me to not only interact on an interpersonal level with key industry members, but also learn first hand about important developing issues in the construction industry. Without this conference, coming up with ideas for my thesis research would have been much more difficult.

### **Key Contacts:**

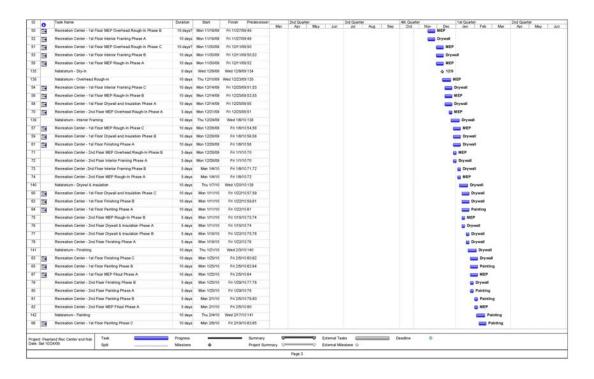
Robert Leicht – DPR Construction – Integrated Project Delivery John Bechtel – Penn State OPP – Integrated Project Delivery/Owner's Perspective of Delivery Method

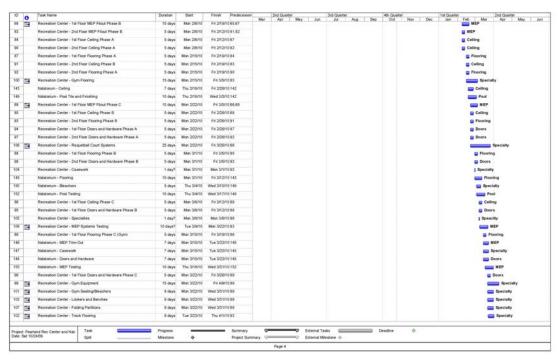
# Appendix 1 Detailed Project Schedule

# **Detailed Project Schedule**









## Pearland Recreation Center and Natatorium – Tech Report #2



# Appendix 2 Detailed Structural System Estimate

# **Detailed Structural System Estimate**

ltem	Units	Quantity	Labor (\$/unit)	Material (\$/unit)	Equipment (\$/unit)	Total (\$/unit)	Labor	Material	Equipment	Total	RS Means
					Caissons	CONTRACTOR ASSESSED.					
8 Bell diameter, 48" shaft	EA	5.00	\$975.00	\$450.00		\$1,430.00	\$4,875.00	\$2,250.00	\$5,500.00	\$12,625.00	Page 592
					Footings						
Concrete - 3000 psi	CYD	1,48					\$49.58	\$149.48		\$381.32	Page 64, 65
Concrete Forming	SFCA	80.00		\$0.70				\$56.00			Page 46
Reinforcing Steel	TON	0.04	\$690.00			\$2,280.15	\$27.20	\$59.00	\$5.01	\$91.21	Page 59
	100000		S 1888 S S		Grade Beams	100000		1000000			See to be to be
Concrete - 3000 psi	CYD	6.00		\$101.00				\$606,00			Page 64, 65
Concrete Forming	SFCA	294.00		\$0.70				\$205.80			
Reinforcing Steel	TON	0.40	\$890,00			\$3,330.00	\$358.67	\$983,32	\$0.00	\$1,341.99	Page 58
					Slab-On-Grade		,	,			
Concrete - 3000 psi	CYD	19.44	\$16.70					\$1,963,44			Page 64, 65
Concrete Finishing	SF	1260.00	\$0.18	\$0.00				\$0.00			Page 66
"Concrete Edge Form	LF.	27.25	\$2.02	\$0.36				\$10.36			Page 47
/apor Barrier	SF	1260.00						\$1,512.00			Page 192
Reinforcing Steel	TON	0.01	\$620.00	\$1,475.00		\$2,095.00	\$6.20	\$14.75	\$0.00	\$20.95	Page 59
					Elevated Slab						
Concrete - 3500 psi	CYD	11.67	\$15.50					\$1,213.68			Page 64
Concrete Finishing	CYD	1260.00						\$0.00			Page 66
5" Pour Stop	SF	6.81	\$3,33	\$1.47				\$10.01			Page 44
X 6 WWF Reinforcing	CSF	12.60		\$32.50				\$409.50			Page 60
1/16* Metal Decking	SF	1260.00	\$0.36			\$2.11	\$453.60	\$2,167.20	\$37.80	\$2,658.60	Page 124
					Steel Columns						
S 10x10x3/8"x16"	LF	6.75					\$344.25	\$10,968.75			Page 110
S 8x8x3/8"x14"	LF	1.93	\$49.00			\$964.00	\$94.50	\$1,697.14	\$67.50	\$1,859,14	Page 110
					Steel Beams	S 7.55(0/3)	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -		Q 30 PR 80	6 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	SE SE
V 27x84	LF	54.50	\$2.96	\$139.00	\$1.58	\$143.54	\$161.32	\$7,575.50	\$86.11	\$7,822.93	Page 114
V 16x26	LF	45.50		\$43.00	\$1,74	\$47,18	\$111.02	\$1,956.50	\$79,17	\$2,146.69	Page 114
V 30x90	LF	27.25	\$2.94	\$163.00		\$167.50	\$80.12	\$4,441.75	\$42.51	\$4,564.38	Page 114
					Floor Joists						
8LH12	LF	500.50	\$1.96	\$28.00	\$1.12	31.08	980.98	14.014.00	560.56	\$15,555.54	Page 121
			Tot	al Structural System	Cost	100-100	ol more	THE RESERVE		\$80,719.45	9000000
			- 100	Total Cost/SF1:	0.000					\$32.03	-

tructural System	SF	63300	\$32.03					\$2,027,499.00 NA
	359,011		200000	Roof De	ock			
7 1/4* Tectum E Roof Deck	SF	59645.00	\$3.50	\$7.00	\$0.00	\$10.50 \$208,757.50 \$417,515.00	\$0.00	\$626,272.50 NA
				Wood Tru	reses			
130' LHSP Wood Joist Trusses	EA	68	\$500.00	\$1,500.00	\$500.00	\$2,500.00 \$34,000.00 \$102,000.00	\$34,000.00	\$170,000.00 NA
	300	30	Total Recreation	Center Structural System	n Cost:	10 12 St		\$2,823,771.50

'Note: This cost does not include the Roof Deck and Wood Trusses

	11.11	To	I		E	T	4 - 4			W-100	Inc. st
tem	Units	Quantity	Labor (\$/unit)	Material (\$/unit)	Equipment (\$/unit)	Total (\$/unit)	Labor	Material	Equipment	Total	RS Means
					Caissons						
Pell diameter, 48" shaft	EA	5.00	\$975.00	\$450.00	\$1,100.00	\$1,430.00	\$4,875.00	\$2,250.00	\$5,500.00	\$12,625.00	Page 592
	1930	18			Footings		2		TO THE REAL PROPERTY.		Contraction of the
Concrete - 3000 psi	CYD	1.48	\$33.50	\$101.00	\$123.15	\$257.65	\$49.58			\$381.32	Page 64, 65
Concrete Forming	SFCA	80.00	\$2.93	\$0.70	\$124.15	\$127.78	\$234,40	\$56.00	\$9,932.00	\$10,222,40	Page 46
Reinforcing Steel	TON	0.04	\$680.00	\$1,475.00	\$125.15	\$2,280.15	\$27.20	\$59.00	\$5.01	\$91.21	Page 59
	0	121	25		Grade Beams		Contract of	200000000	1	(i)	Nation of the last
Concrete - 3000 psi	CYD	6.00	\$12.05	\$101.00	\$4.39	\$117.44	\$72.30	\$606.00	\$26.34	\$704.64	Page 64, 65
Concrete Forming	SFCA	294.00	\$2.93	\$0.70	\$0.00	\$3.63	\$861.42	\$205.80	\$0.00		
Reinforcing Steel	TON	0.40	\$890.00	\$2,440.00	\$0.00	\$3,330.00	\$358.67	\$983.32	\$0.00		
	A	_		5	lab-On-Grade						
Concrete - 3000 psi	CYD	19.44	\$16.70	\$101.00	\$6.10	\$123.80	\$324.65	\$1,963,44	\$118.58	\$2,406.67	Page 64, 65
Concrete Finishing	SF	1260.00				\$0.18	\$226.80	\$0.00			Page 66
5" Concrete Edge Form	LF	27.25			\$0.00	\$2.40	\$55.05	\$10.36	\$0.00		Page 47
Vapor Barrier	SF	1260.00					\$1,449.00				Page 192
Reinforcing Steel	TON	0.01	\$620.00	\$1,475.00	\$0.00	\$2,095.00			\$0.00		Page 59
	1			tal Structural System		32,000.00				\$32,114.60	
				Total Cost/SF1:	2222					\$12.74	

AND DESCRIPTION OF THE PARTY OF	to find	Tel 200000000	Natate	rium Structural Costs (E	xcept Glulam Materi	als				TARRESTA MARRIADA	-2000
Structural System	SF	41817	\$12.74							\$532,911.20	NA
				Glutam							*******
Glulam Framing	SF	41230.00	57.14	\$15.90	\$0.00	60E 0E	£100 405 00	\$655,725.00	\$0.00	£1 070 000 00	NA.
Vood Deck	SF	41230.00	\$1.34	\$2.71	\$0.00	\$20,90	\$302,485,00	\$111,790.00	\$0.00	\$1,070,000.00	NA.
		110	Total Matabasis	on Chanchard Contact Co.	de la		6 10			\$1 602 011 20	

'Note: This cost does not include Glulam Products

Total Structural Con	its
Natatorium Structural Cost	\$1,602,911.2
Recreation Center Structural Cost	\$2,823,771.5
Total Structural Cost	\$4,427,368.6
Total Structural ContiSE	C424

# **Appendix 3**

# Detailed Structural System Cost Estimate Hand Take-Offs

# Detailed Structural System Cost Estimate Hand Take-Offs

	Becreation Center, 1054
	Structural System Hand Talke-Off
	From Gridlines G-5/1-4
1)	Carissons: (2) @ 48"dia, (2) @ 42"dia and (2)@ 30"dia. All R' length
	Concrete: 2x5.58 CYD
	7x5.58 CYD 2x4.27 CYD 2x2.18 CYD 2x2.18 CYD 2x2.18 CYD 3000ps;
Reins.	Steel Vertical All 6: 8-#10
1	6x8x12'=576lf+ of #10
	Ties: 2- #3@18" => 8 ties (12')
	(2) - 12.56' = 7(2)(8)(12.56) = 201'
	(7) - 10.99' = 7(7)(8)(10.99) = 176'
	(2) - 7.85' = 7(2)(8)(7.85') = 126'
	So: #3: 0.37651 #10: 4.303451
	503'x0.376'b/st _ 0.1 Ton
^_	576'x 4,303'95+ - 1.24 Ton of Rebace

	284
2)	Factings: (5) 2'x2'x2' FJ6s
	Concrete: 40 = 1.48 CYDs -3000psi
	Farming: 16 SFCA X5= 805FCA
	Steel: 2-#7 T+B
	5x(4)(2) = 40-lst 05#7
	#7: 2.044 1/57
1	Grade Beam : 0.04 Ton
3)	Grade Beam:
	Total Length: 73.5'
	Concrete: 2'x 1.1' x 73.5' = 161.7 CF
	Forming: 4'x 73.5'= 294 SFCA
	Steel: 2-#7 T+B
	473.5' = 2945+ 547 #3 Sticings @10"ox. = 88: Sticings
5	6.2'x88 = 546' of #3
	0.376×546+294×2.044 = 0.403Tons

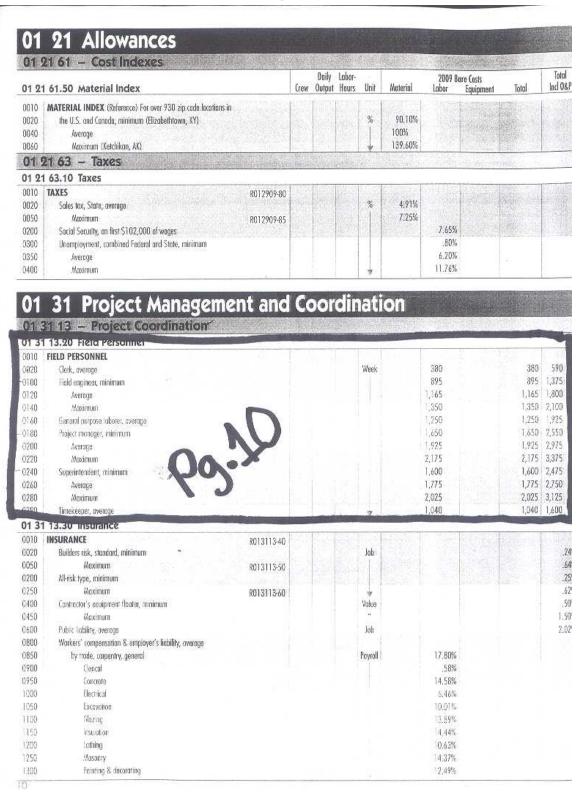
		3054
4)	Slab-on Grade: Area = 27.25'x 46.25' = 1	260 SF
	Concrete: 1260 SF x 5/12 = 525 = 19	.44 CYD
	Vapor Barrier: 1260SF 27	-3000psi
	5" Edge Form: 27.251	
	Steel: #3 @ 14" a.c. EW	if.
	27.25 + 46.25 = 24 +40 = 64lft of	#3
~.	0.376×64 = 0.01 Ton	
	Finishing: 1260 SF	
5)	Elevated Slab: 1260 SF	
	Concrete: 1260 x3/12= 11.67CYD-3	Bopsi
	9/16 Deck: 1260 SF	04
	3" Paur Stap: 27, 25.15	
_	Finishing: 1260SF	
/ Y	Reinforcing: 1260SFOF 6×6 WW	

	*Note: These are forcentire bldg. (Reclinited)
*6)	Roof Deck: 319×181=57,739 SFx103=59,645SF  74" Tectum E Roof Deck: 59,645SF
*7)	Wood Trusses: 68 LHSP@ 5'o.c
8)	Steel:
	Columns: (4) T\$ 10×10×36" - 27'  Beams: (2) W 27×84 - 27.25'  (1) W 16×26 - 45.5'  (1) W 30×90 - 27.25'  Floor Joists: (11) 28 LH 12 - 45.5'

# **Appendix 4**

# RS Means 2009 Building Construction Cost Data Sheets

# RS Means 2009 Building Construction Cost Data Sheets



The same of	11 13 - Structural Cast-In-Place Concrete	13011111	1000	7.		12.4				William I
2 44	13.25 Forms in Place, Columns	Crew	Daily Output	Labor- Hours	Unit	Hatavial		rre Costs	7.41	Total incl O&P
300	48" diameter		50	.640	L.F.	Material 68	Labor 24	Equipment	Total 92	113
350	60" diameter		45	.711	No.	42	27		69	88
	For second and succeeding months, deduct	£1: Y	40	5000		50%	24		670	1,000
00		(4)	165	194	SECA	2.4	12.98		0.75	14.0
CC	Job-built alywood, P" x 8" columns, T use	- 61		.164	SECA		7,35		9.76	11.1
50	2 050		195		- 1	1,37	6.20		7.57	10
00	3.use		210	.152	4 16	.96	5.75	20027	6.71	
50	4 use		215	149		.79	5.65		6.44	9.6
00	12" x 12" columns, 1 use		180	.178	300	2.27	6.75		9.02	12.9
50	2.050		210	.152	138	1.25	5.75		7	10.3
00	3 use	4.7	220	.145		.91	5.50		6.41	9.5
50	4 use		225	.142		.74	5.40		6.14	9.1
00	16" x 16" columns, 1 use		185	.173	l fil	2.24	6,55		8.79	12.6
50	2 use	1.7	215	.149		1.19	5.65		6.84	10.0
00	3 use		230	139	RE	.90	5.25		6.15	9.1
50	4 use		235	.136		.73	5.15	1175	5.88	8.8
00	24" x 24" columns, 1 use		190	.168		2.49	6.40		8.89	12.6
50	2 use		216	.148		1.37	5.60		6.97	10.2
00	3 1190		230	.139		.99	5.25		6.24	9.2
50	4 use		238	.134		.81	5.10		5.93	8.8
00	36" x 36" columns, 1 use		200	.160		1.81	6.05		7.86	11.4
50	Z use		230	.139	100	1.03	5.25	1	6.28	9.3
00	3 496		245	.131		.73	4.94		5.67	8.4
50	4 458		250	128	100	.59	4.85		5.44	8.1
00	Steel framed plywood, based on 50 uses of purchased		250	3120	1.5	RESIDENT	4.03		2013	0.1
	forms, and 4 uses of bracing lumber	1								
20	The state of the s	(-1	340	.094	SECA	4.53	3.56	SHEMIN	8.09	10.5
00	8" x 8" calumn	(2)		.091	SELEN	3.99	3.46		7.45	9.7
50	10° x 10"	3.1	350 370	.086		3.38	3.27		6.65	8.8
00	12" x 12"	11.7								7.6
50	16" x 16"	-	400	.080		2.63	3.03		5.66	
00	20" x 20"		420	.076	140	2.35	2,88	1.05	5.23	7.0
50	24"x24"		440	.073		1.67	2.75		4.42	8.1
55	30" x 30"		440	.073		2.14	2.75	<b>32465</b>	4,89	6.6
60	.36" x 36"	V	460	.070	7	1.90	2.63		4.53	6.1
3 1	1 13.30 Forms in Place, Culvert									9.
10	FORMS IN PLACE, CULVERT R031113	40	dine.			Bright of		HALLERS		
115	5' to 8' square or rectangular, 1 use	(-1	170	.188	SECA	6.10	7.15		13.25	17.7
50	Z use R031113-	60	180	.178		3.90	6.75		10.65	14.7
00	3 use		190	168		3.16	6.40		9.56	13.4
50	4 050	W	200	.160		2.79	6.05		8.84	12.4
	13.35 Forms in Place, Elevated Slabs	1	-							
-		10	Herene S	Males	CURRE		Manager H		NEETWO.	Laws a
			470	.102	c.r	4.53	3,97	-0-36	8.50	11.1
000	Flat plate, job-built plywood, to 15' high, 1 use R031113-	60 G2	470		S.F.	2.49	3.59		6.08	8.3
50	2 use		520	.092	3	1.47	0.37		0.00	7.2
50		THE REAL PROPERTY.	540			47	3.33		4.80	6.7
50	4 use		560	,086						
00	15-10 ZO migir tenings, 4 Use		450	1077		1.67	3.77	12.00	4.70	9.2
00	21' to 35' high ceilings, 4 use		450	.107		2.55	4.15		6.70	
000	Flot slob, drap panels, jab-built plywood, to 15" high, 1 use	100	449	.107	GE 181	4.77	4.16	1065.00759	8,93	11,7
50.	2 use	el or a	509	.094		2,62	3.67	max.	6.29	8.6
00	3 use		532	.090		1.91	3,51		5.42	7.5
150	4 use		544	.088		1.55	3.43	CONTRACT.	4.98	7
250	15' to 20' high ceilings, 4 use		480	.100	1000-003	5.10	3.89	100000000000000000000000000000000000000	8.99	11.6

20	11 13 - Structural Cast-In-Place Concre	te fo	ormii	ng					HIPET.		
12 4	1 13.45 Forms in Place, Footings		(rev:	Daily Outabl	Labor	Unit	Material		are Costs	4.1	Total incl O&P
500	Keywoy, 4 use, tapered wood, 2" x 4"		Lon		Hours .015	Li	Material . 16	Labor .60	Equipment	Total	1,10
550	2" x 6"		Culp	500	.016	No.	.26			,76 .90	1.28
2000	Tapered plastic			530	.015		.53			1.13	1,51
2250	For keyway hung from supports, add		200	150	.053		.65			2.78	4.02
3000	Pile cap, square or rectangular, job-huilt plywood, 1 use		(-1	290	.110	SFCA	2.46		1021: E1H	6.64	9.20
3050	2 use		***	346	.092	3190	1.35	3,50		4.85	6.95
3100	3 use			371	.086		.99			4.26	6.15
3150	4 use			383	.084		.80			3.96	5.80
4000	Triangular or hexagonal, 1 use			225	.142		2.86	5.40		B.26	11.50
4050	2 use 2 use			280	.114		1.58	4.33	SC TO HENCHO	5.91	8.45
4100	3 use			305	.105		1.15	3.97		5.12	7,40
4150	4 use		He	315	.102		.93	3.85		4.78	6.95
5000	Spread factings, job-built lumber, 1 use		146	305	.105		2.16	3.97		6.13	8.55
5050	2 use		1	371	.086		1.20	3.27		4,47	6.35
100	3150			40I	080		- 0/	0.00		7.00	5.65
5150	4 use			414	077	v	.70	2.93		3.63	5.30
0000	Supports the bowers, plantas or tempores, 2, in 2, 100 mg.	-	100	9	1.200	Circles Co.	5.40	90.90		90%	- 19 C
6050	4' x 4' footing			22	1.455		10.80	55	A Lawrence	65.80	.97.50
6100	8' x 8' footing			20	1.600		21.50	40.50		82	118
6150	12' x 12' footing			17	1,882	w	- 26	71.50		97.50	140
7000	Plinths, job-built plywood, 7 use			250	.128	SECA	2.73	4,85		7.58	10.50
7100	4 use			270	.119	"	.90	4.49		5.39	7.95
050 000 050 500 550	30" diameter, 13" high Island forms, 10" long, 9" high, 3'- 6" wide 4" vide 20" long, 9" high, 4" wide 5" vide	G G G	(-) ∀	8 10 9 6 5	3.200 3.556 5.333 6.400	v	157 440 455 730 760	40 121 135 202 242		197 561 590 932 1,002	235 675 710 1,125 1,200
	1 13.50 Forms In Place, Grade Beam	The second									
2010		113-40									
0020	Job-built plywood, 1 use		C-2	530	.091	SECA	3.25	3.52		6.77	9.05
0050	2 use RC31	113-60		580	.083		1.79	3.22		5.01	6.95
0150			1 1 1		070		1.06	3.09			5.95
STATE OF THE PARTY.	4 use		4	605	.079	Ψ.	1,90	3,07		4.15	3.73
-	1 13.55 Forms in Place, Mat Foundation	no Lora	District of	DIVEST.	Partico	te de la constante de la const		PER CONTRACT		WATER CO.	
0010		113-40	00	000		CFCA	0.04	4.45		0.70	10.05
0020	Job-built plyword, 1 use		C-2	290	166	SFCA	2.94	6.45		9.39	13.25
0050		113-60		310	.155		1.19	6		7,19	10.65
0100	3.058		200	330 350	.145		.75 .70	5.65 10 1	W-24/07/08/10	6.40	9.60 9
0120	4 usa		*	930	.10/	Ψ.	7.0	5.35		0.03	- 7
1	1 13.65 Forms In Place, Slab On Grade							P. 100 CO. 100			
0010		11340		in.					100		
1000	Bulkhead forms w/keyway, wood, 6" high, 1 use		(-)	510	.063	Lf.	.84		8 +	3.22	4.60
1050		113-60			€.080		.46	3.03	400.0	3.49	5.20
1100	4 usas		Sin	350	.091	833	.27	3.46		3.73	5.65
1400	Bulkhead form for slab, 4-1/2" high, exp metal, incl keywey & stokes	G		1200	.027		2.78	1.01		3.79	4.63
1410	5-1/2" trigh	G		1100	.029		3.23	1.10	1	4.33	5.25
1420	7-1/2" high	G		960	.033		4.26	1.26		5.52	6.65
1430	9-1/2" high	G		840	.038		4.84	1.44		6.28	7.55

								201	29.	47
03	11 Concrete Forming		1400			S I				
	11 13 - Structural Cast-In-Place Co	ncrete Fo	emi	ng					THE YEAR	
3 1	1 13.65 Forms In Place, Slab On Grade		Crew	Daily Output	Labor- Hours	Unit	Material	2009 Bare Costs Labor Equipment	Total	Total Ind 08
000	Curb farms, wood, 6" to 12" high, on grade, 1 use		C-T	215	.149	SFCA	2.83	5.65	8.48	- 11
050	2 use		iels.	250	.128		1.57	4.85	6.42	9
100	3 use			265	.121		1.13	4.57	5.70	8
i.ca			WW (SE	275	114		97	4.41	5 33.	
000	Edge forms, wood. 4 use, an grade, to 6" high			600	.053	LF.	.38	2.02	2.40	3
050	7" to 12" high		3		E CONTRACT			Will a second		5.045
500	For depressed slabs, 4 use, to 12" high			300	.107	LF.	.56	4.04	4.60	δ
550	To 24" high			175	.183		.76	6.90	7.66	11
000	For slab blockouts, to 12" high, 1 use		1018	200	,160		.63	6.05	6.68	10
050	To 24" high, 1 use	A	10	120	.267		.80	10.10	10.90	16
100	Plastic (extruded), to 6" high, multiple use, on grade	<b>48)</b> 7 min	V 1	k 2800	.040	7	5.50	1.51	7.01	8
000	Screed, 24 ga. metal key joint, see Div. 03 15 05:25	<b>房 国</b>		0 0	FI SULAN		meye vil			
020	Wood, incl. wood stakes, 1" x 3"	10	(-)	900	.036	L.F.	.68	1.35	2.03	2
050	2" x 4"			900	.036	#	.63	1.35	1,98	2
000	Trench forms in floor, wood, 1 use		1	160	.200	SECA	1.48	7.55	9.03	13
050	2 usa		and the same	175	.183		,81	6.90	7,71	11
100	3 use			180.	.178		.59	6.75	7.34	. 11
150	4 use			185	.173	4	.48	6.55	7.03	10
760	Void farm, carrugated fiberbaard, 6" x 12", 10" long	G	7	240	,133	S.F.	,84	5.05	5.89	8
3 1	1 13.85 Forms In Place, Walls									
010	FORMS IN PLACE, WALLS	R031113-10								
100	Box out for wall openings, to 16" thick, to 10 S.F.		C-2	24	2	Ea.	21.50	78	99,50	145
150	Over 10 S.F. (use perimeter)	R031113-40	"	280	.171	L.F.	1,78	6.65	8,43	12
250	Brick shelf, 4" w, and to wall forms, use wall area aby shelf									
260	1 use	8031113-60	(-2	240	.200	SECA	1.87	7.80	9.67	14
300	2 use			275	.175		1.03	6.80	7.83	11
350	4 use			300	.160	7	.75	6.20	5.95	10
500	Bulkhead, wood with keyway, Tuse, 2 piece 🛴 🥒		7	265	.181	L.F.	1.68	7.05	8.73	12
600	Bulkhead forms with keyway, 1 piece expanded metal, 8" wall	G	C)	1000	.032	0.5	4.26	1.21	5.47	6
610	10" wall	G		800	.040		4.84	1.51	6.35	7
520	12" wall	G		525	.061	4	5.80	2.31	8.11	10
700	Buttress, to B' high, 1 use	. 6	02	350	.137	SECA	7.05	5.35	12.40	16
750	2 use			430	.112		3.89	4.34	8.23	91
300	3 use		11	460	.104		2.83	4.06	6.89	9
350	4 use		М	480	.100	4	2.33	3.89	6,22	8
000	Corbel or hounch, to 12" wide, add to wall forms, 1 use			150	.320	L.F.	1.95	12.45	14.40	21
)50	2 use			170	.282	100	1.07	-11	12.07	18
00	3 use 3 use		100	175	.274		.78	10.65	11.43	17
50	4 use			180	.267	4	.63	10.35	10.98	16
000	Wall, job-built plywood, to 8' high, 1 use		2	370	.130	SECA	2.62	5,05	7.67	10
)50	2 056			435	.110		1.61	4.29	5.90	å
00	3 456			495	.097		1.17	3,77	4,94	7
50	4 use			505	.095		95	3.70	4.65	á
100	Over B' to 16' high, I use			280	.171		9.40	6.65	16.05	20
150	2 use			345	.139		1.34	5.40	6.74	9.
00	3 use			375	.128		.96	4.98	5.94	8
550	4 use			395	.122		78	4.73	5.51	8
00	Over 16' high, I use			235	.204		2.71	7.95	10.66	15.
50	Zuse			290	166		1.49	6.45	7.94	11.
300	3 tsa			315	.152		1.08	5.95	7,93	0.
50	4 tse			330	145		.88	5.65	6,53	9
	2.00				22.020			557.710	10775707	

3 2	105 - Reinforcing Steel Accessorie	.5		Daily	Labor-	_	_	2009 Ba	es fact		Total
011	05.75 Splicing Reinforcing Bars		Crew	Output	Hours	Unil	Moterial	Labor	Equipment	Total	ind 0&P
50	#10.9	G	(-5	95	.589	Ea.	27	25.50	8.30	55.80	74
60	<b>*9-8</b>	G	(-25	105	.305		21	10.65		31.65	40.50
30	#R-7	G		115	.278		19.55	9,75		29,30	37.50
20	#76	G		130	.246		19.05	8.60		27.65	35
10	Position coupler for curved bors, toper forecided, ₹4 burs	G		160	.200		22	7		29	35,50
10	₹5 bars	G		145	.223		23	7.70		30.70	35
20	é6 bars	G		130	246		26	93.8		34.60	43
3C	∮7 bars	G		110	.291		38.50	10.15		48.65	59.50
40	#8 bars	G	w	100	.320	148	40	11.20		51,20	62.50
50	≱9 bars	G	C-5	90	.622		43.50	27	8.75	79.25	101
60	#10 bars	G		80	.700		47	30.50	9.85	87.35	111
70	#11 bars	G		70	.800		49	35	11.30	95.30	122
80	#14 bars	G		55	1.018		61	44	14.35	119.35	154
90	#18 bnrs	G	H	40	1.400		88	61	19.75	168.75	216
00	Transition position coupler for curved bars, taper threaded, #18-14	G		40	1.400		- 111	61	19.75	191,75	241
10	₹18-11	G		40	1.400		112	61	19.75	192.75	242
20	<b>#14·11</b>	G	LIBE	. 55	1.018		95	44	- 14.35	153.35	191
30	#11-10	G		70	.800		54.50	35	11.30	100.80	128
40	#10-9	G		80	.700		52	30,50	9.85	92.35	116
50	#9-8	G	C-25	90	.356	1	48	12.45		60.45	73.50
60	#87	G		100	.320		44	11,20		55.20	67
70	£7-4	G		110	.291		42.50	10.15		52.65	64
00	Sleeve type w/ grout filler, for precast concrete, #6 bars	G		72	.444		23.50	15.55		39.05	51.50
02	#7 bars	G		64	.500		25.50	17,50		43	57
05	₹8 bars	G		56	.571		29	19.95		48,95	65
07	#9 bots	G	+	48	.667		31.50	23.50		55	73.50
10	#10 bors	G	0.5	40	1.400		41	61	19,75	121,75	165
00	₩11 bars	G	131	32	1.750		49	76	24.50	149.50	203
20	₹14 bnrs	G	W	24	2,333		79,50	101	33	213.50	285
00	Sleeve type w / ferrous filler, for critical structures, ₹6 bars	G	C-25	72	.444		41	15.55		56.55	71
10	₹7 bors	G		64	.500		42	17.50		59.50	75
20	#8 bors	G	V	56	.571		44	19,95		63.95	81.50
30	#9.bars	G	C-5	48	1.167		45	50.50	16.45	111.95	149
40	#10 bars	G	14	40	1,400		48	61	19.75	128.75	172
50	#11 bors	G		32	1.750		58	76	24.50	158,50	213
60	₽14 bors	G	lah.	24	2.333		73	101	33	207	278
70	#1B hors	G	v	16	3.500		106	152	49.50	307.50	415
000	Weldable half coupler, taper threaded, #4 bars	G	E-16	120	.133		7.10	6.10	1.12	14.32	19.95
00	#5 bors	G		112	.143		8.40	6.55	1.20	16.15	22
00	#6 bors	G		104	.154		13.35	7.05	1,29	21.69	28.50
100	\$7 bars	G	188	96	.167		15.50	7.60	1.40	24.50	32
100	#8 bars	G		88	,182		16.15	8.30	1.53	25.98	34.50
00	#9 bars	G	15	80	.200		17.80	9.15	1.68	28.63	37.50
000	#10 bors	G	1518	72	.222		18.20	10.15	1.86	30.21	40
700	#11 liors	G		64	.250		19.45	11.45	2,10	33	44.50
300	#14 bors	G		56	.286		22.50	13.05	2.40	37.95	50.50
900	#18 bars	G	W	-48	.333	V	36.50	15,25	2.80	54.55	70
3 2	1 10 - Uncoated Reinforcing Steel							work			3.5
and a proper	10.60 Reinforcing In Place		-								
contractor (	REINFORCING IN PLACE A615 Grade 60, incl. access. labor	R032110-10				West West		mgravy t	allegra job	Mar.	
100	Bearns & Girders, #3 to #7	[C]	(.n)	m 1.60	20	Ton	1,550	890	Of the last of the	2,440	3,150

	21 Reinforcing Steel 1 10 - Uncoated Reinforcing Steel						No.				
	10.60 Reinforcing In Place		Crew	Daily Output	Labor- Hours	Unit	Material	2009 Bar Lebor	e Costs Equipment	Total	Total Incl 0&
150		G	4 Rodm			Ton	1,550	530		2,080	2,575
200	Calumns, #3 to #7	G		1.50	21.333	T	1,550	950		2,500	3,250
250		G		2.30	13.913		1,550	620		2,170	2,725
300	Spirals, hot rolled, 8" to 15" diameter	G		2.20	14.545	9 4	2,000	650		2,650	3,250
320		G	i li i	2.20	14.545		1,925	650	-	2,575	3,150
330	24" to 36" diameter	G		2.30	13.913		1,825	620		2,445	3,025
340	36" to 48" diameter R032110-50	G		2.40	13.333		1,725	595		2,320	2,875
360		G		2.50	12.800		1,925	570		2,495	3,025
380	64" to 84" diameter R032110-70 -	G		2.60	12.308		2,000	550		2,550	3,100
390		G		2.70	11.852		2,100	530		2,630	3,175
100		G		2.90	11.034		1.650	490		2 140	2,000
500	Footings, #4 to #7	G		2.10	15.238		1,475	680		2,155	2,729
600	Slob on grade, #3 to #7	G	Swill I	Z.5U	13.913	365	1,475	620		1,775 Z <sub>2</sub> 073	بادائرة
700	W0.6, #3.10 #7	-1	CONTRACTOR OF THE PERSON NAMED IN		TAKE T			- USUS		77.50	
750	#8 to #18	G	7	4	8	4	1,475	355		1,830	2,200
900	Use the fallowing for a rough estimate guide									7.16	
000	Typical in place, average, under 10 ton job, #3 to #7	G	4 Rodm	1,80	17.778	Ton	1,600	790	+	2,390	3,075
010	#8 to #18	G		2.70	11.852		1,625	530		2,155	2,57
050	10 = 50 ton job, #3 to #7	G		2.10	15.238		1,575	680		2,255	2,825
060	#8 to #18	G		3	10.667		1,600	475		2,075	2,550
100	50 – 100 ton jcb, #3 - #7	G		2.20	14.545		1,525	650		2,175	2,750
110	#8 to #18	G		3,10	10.323		1,575	460		2,035	2,47
150	Over 100 ton jab, #3 - #7	G		2.30	13.913		1,525	620		2,145	2,700
160	#8-#18	G	7	3.20	10		1,550	445		1,995	2,425
200	High strength steel, Grade 75, ₹14 bars only, add	G					153			153	160
2000	Unloading & sorting, add to above		0-5	100	.560			24.50	7.90	32.40	47
200	Crane cost for handling, add to above, minimum			135	,415			18	5.85	23,85	35
210	Average			92	.609			26,50	8.60	35.10	52
220	Moximum		7	35	1.600	· W		69.50	22.50	92	138
400	Dowels, 2 feet long, deformed, #3	G	2 Rodm	520	.031	Eo.	.64	1.37		2.01	
410	ALCOHOLOGICA CONTRACTOR OF THE STREET	G		480	.033		1.14	1.48		2.62	
420	#5	G		435	.037		1.78	1.64		3.42	
430	\$6	G		360	.044	¥	2.56	1.98		4.54	
450	Longer and heavier dowels, add -	G		725	.022	Lb.	.85	.98		1.83	3
500	Smooth dawels, 12" long, 1/4" or 3/8" diameter	G		140	.114	Ea.	1.21	5.10		6.31	
520	5/8" diameter	G		125	.128		2.11	5.70		7.81	1
530	3/4" diameter	G		110	.145	w	2.62	6.50		9.12	13
600	Dowel sleeves for CIP concrete, 2-point system										
610	Sleeve base, plastic, for 5/8" smooth dowel sleeve, fosten to edge form		1 Rodm	200	.040	Ea.	.52	1.78		2.30	
615	Sleeve, plastic, 12" lang, for 5/8" smooth dowel, snap onto bas	9	100	400	.020		1.03	.89		1.92	
620.	Sleeve base, for 3/4" smooth dowel sleeve			175	.046		.49	2.04		2.53	3
625	Sleeve, 12" long, for 3/4" smooth dewel			350	.023		1.08	1.02		2.10	1
630	Sleeve base, for 1" smooth dawel sleeve			150	.053		.64	2.38		3.02	
635	Sleeve, 12" long, for 1" smooth dowel		7	300	.027		1.84	1.19		3.03	1
700	Dowel caps, visual warning only, plastic, #3 to #8		2 Rodm	800	.020		.51	.89		1.40	
720	₹8 to ₹18			750	.021	e fi i	1.08	.95		2.03	
750	Impolement protective, plastic, #4 to #9		7	800	.020	7	1.95	.89		2.84	
-	10.70 Glass Fiber Reinforced Polymer Bars										
010	GLASS FIBER REINFORCED POLYMER BARS					LE	35			.35	
050	#2 bar, .043 lbs/ ft.					1.1.	.48			.48	

	teel							-		
03 21 10.70 Glass Fiber Reinforced Polymer Ba	arc	Crew	Duity	Labor Haum	H-si	Massalal	2009 8	Bare Costs	9.7	Total
0150 #4 hrs., 160 hrs/ H	115	riew	Outpu	пооп	Unit LE.	Materini .70	Laber	Equipment	Total .70	Incl 0&P
0200 #5 np. 258 ips/ft.					hale.	98			.70	1.0
9250						1,35			1.85	1.4
0300 #7 bm, 497 lbs/fc						1.70			1.70	1,8
0350						2,25			2.25	2.4
0400 #9 liar, ,800 lbs/ ft.						2.90			2.90	3.1
0450 #10 bar, 1.08 lbs/ ft,					v	3.45			3.45	3.8
0500 For Bends, add per bend =			100	0,10	Ea.				1	1.1
03 21 13 - Galvanized Reinforcing	Steel							WHEN	11	
3 21 13.10 Galvanized Reinforcing										
0010 GALVANIZED REINFORCING		107			713	Name of		Sheater.		311
0150 Add to uncoated reinforcing price for galvanizing		185			Ton	1,150			1,150	1,250
03 21 16 - Epoxy-Coated Reinforcia	ng Steel					1		344		
03 21 16.10 Epoxy-Coated Reinforcing	The state of the s		and the Vision					THE STATE OF		
0010 EPOXY-COATED REINFORCING		1676						5.700		Zai E.
0100 Add to uncoated reinferring price for coaling with epoxy		FR			Ton	865			865	950
	CN G	2 Rodm			C.S.F.	18.05	20.50		38.55	53.50
300 6 x 6 · W2.9 x W2.9 (6 x 6) 42 lb, per ( S F	CN G	2 Rodm	35 21 29	.457 537 .552	C.S.F.	18.05 54.50 32.50	20.50 25 24.50		38.55 49.50 57	53.50 - // 50 76
1300 6 x 5 · W2.9 x W2.9 (6 x 6) 42 lb, nec C S F 1400 9x 0 · W4 x W4 (4 x 4) 58 lb, per C.S.F.	<u> </u>	2 Radm	21 29 27	.552 .573	C.S.F.	32.50 46.50	24.50 24.50 24.50		40,50 57	76
1800 6 x 6 - W2.9 x W2.9 (6 x 6) 42 lb, per C.S.F. 400 6 x 6 - W2.9 x W2.9 (6 x 6) 42 lb, per C.S.F. 400 4 x 4 x W1.4 x W1.4 (10 x 10) 31 lb, per C.S.F.	C G	2 Rodin	21 29 27 31	.552 .573 .516	CSE	32.50 46.50 26.50	24.50 24.50 24.50 23	SEA X THOSA OF	49.50 57 70 49.50	76 67
1300 6 x 6 - W2.9 x W2.9 (6 x 6) 42 lb, ner C S F 1400 4 x 4 - W1.4 x W1.4 (10 x 10) 31 lb, per C.S.F. 1600 4 x 4 - W2.1 x W2.1 (8 x 8) 44 lb, per C.S.F.		2 Rodin	29 27 31 29	.552 .573 .516 .552	CS.F	32.50 46.50 26.50 38	24.50 24.50 23 24.50		49.50 57 ,0 49.50 62.50	76 76 67 81,50
1500 6 x 6 - W2.9 x W2.9 (6 x 6) 42 lb, per C.S.F. 400 4x 4 - W1.4 x W1.4 (10 x 10) 31 lb, per C.S.F. 1500 4x 4 - W1.4 x W1.4 (10 x 10) 31 lb, per C.S.F. 1600 4x 4 - W2.1 x W2.1 (8 x 8) 44 lb, per C.S.F. 1650 4x 4 - W2.9 x W2.9 (6 x 6) 61 lb, per C.S.F.		2 Radm	29 27 31 29 27	.552 .573 .516 .552 .593	C.S.F.	32.50 46.50 26.50 38 50.50	24.50 20.50 23 24.50 26.50		49.50 57 49.50 62.50 77	76 67 81.50 98.50
1300 6 x 6 - W2.9 x W2.9 (6 x 6) 42 lb, ner C S E 1400 4 x 4 - W1.4 x W1.4 (10 x 10) 31 lb, per C.S.E. 1600 4 x 4 - W2.1 x W2.1 (8 x 8) 44 lb, per C.S.E. 1650 4 x 4 - W2.9 x W2.9 (6 x 6) 61 lb, per C.S.E. 1650 4 x 4 - W2.9 x W2.9 (6 x 6) 61 lb, per C.S.E.		2 Rodm	29 27 31 29	.552 .573 .516 .552	C.S.F. ▼	32.50 46.50 26.50 38	24.50 24.50 23 24.50		49.50 57 ,0 49.50 62.50	76 76 67 81,50
\$00		2 Rodm	29 27 31 29 27	.552 .573 .516 .552 .593	€S.E.	32.50 46.50 26.50 38 50.50	24.50 20.50 23 24.50 26.50		49.50 57 49.50 62.50 77	76 67 81.50 98.50
1300 6 x 6 - W2.9 x W2.9 (6 x 6) 42 lb, per C.S.F. 1400 4 x 4 - W1.4 x W1.4 (10 x 10) 31 lb, per C.S.F. 1600 4 x 4 - W2.1 x W2.1 (8 x 8) 44 lb, per C.S.F. 1650 4 x 4 - W2.9 x W2.9 (6 x 6) 61 lb, per C.S.F. 1750 Rolls		2 Rodm	29 27 31 29 27	.552 .573 .516 .552 .593	CS.F.	32.50 46.50 26.50 38 50.50	24.50 20.50 23 24.50 26.50		49.50 57 49.50 62.50 77	
1300 6 x 6 - W2.9 x W2.9 (6 x 6) 42 lb, ner C S E 1400 74 x W4 (4 x 4) 58 lb, per C.S.E. 1500 4 x 4 - W1.4 x W1.4 (10 x 10) 31 lb, per C.S.E. 1600 4 x 4 - W2.1 x W2.1 (8 x 8) 44 lb, per C.S.E. 1650 4 x 4 - W2.9 x W2.9 (6 x 6) 61 lb, per C.S.E. 1700 4 x 4 - W4 x W4 (4 x 4) 85 lb, per C.S.E.			21 29 27 31 29 27 25 6.50	.557 .576 .516 .552 .593 .640	v	32.50 46.50 26.50 38 50.50 65.50	24.50 20.70 23 24.50 26.50 28.50		40.50 57 49.50 49.50 62.50 77 94	76 67 81.5 98.5 139
1300			21 29 27 31 29 27 25 6.50	.552 .573 .516 .552 .593 .640 2.462	v	32.50 46.50 26.50 38 50.50 65.50	24.50 23 24.50 26.50 28.50		40.50 57 49.50 62.50 77 94	76 67 81.50 98.50 119
\$00		2 Rodm	21 29 27 31 29 27 25 6.50	.552 .573 .516 .552 .593 .640 2.462	v	32.50 46.50 26.50 38 50.50 65.50	24.50 23 24.50 26.50 28.50		40.50 57 49.50 62.50 77 94	76 67 81,50 98,50 119
300 6 x 6 - W2.9 x W2.9 (6 x 6) 42 lb, per C.S.F. 400 4 x 4 - W1.4 x W1.4 (10 x 10) 31 lb, per C.S.F. 4 x 4 - W1.4 x W1.4 (10 x 10) 31 lb, per C.S.F. 4 x 4 - W2.1 x W2.1 (8 x 8) 44 lb, per C.S.F. 650 4 x 4 - W2.9 x W2.9 (6 x 6) 61 lb, per C.S.F. 700 4 x 4 - W4 x W4 (4 x 4) 85 lb, per C.S.F. 880 2 x 2 - \$14 galw, 21 lb/C.S.F., acom & column wrap 900 2 x 2 - \$12 galw, for gunthe reinforcing  3 23 Stressing Tendons 3 23 05.50 Prestressing Steel  101 PRESTRESSING STEEL	G G G G G G G G G G G G G G G G G G G	2 Rodm	29 27 31 29 27 27 25 6.50 6.50	.552 .578 .576 .552 .593 .640 2.462 2.462	CS.F.	32.50 46.56 26.50 38 50.50 65.50	24.50 23 24.50 26.50 28.50 110 110	09	49.50 57 49.50 62.50 77 94 176 175.50	76 67 81,50 98,50 139 252 252
\$300	G G G G G G G G G G G G G G G G G G G	2 Rodm	29 27 31 29 27 27 25 6.50 6.50	.512 .552 .516 .552 .593 .640 2.462 2.462	v	32.50 46.56 26.50 38 50.50 65.50 66 45.50	24.50 24.50 23 24.50 26.50 28.50 110 110	.09	49.50 57 49.50 62.50 77 94 175.50	76 67 81.50 98.50 119 252 252
\$00	G G G G G G G G G G G G G G G G G G G	2 Rodm	29 27 31 29 27 27 25 6.50 6.50	.552 .578 .576 .552 .593 .640 2.462 2.462	CS.F.	32.50 46.56 26.50 38 50.50 65.50	24.50 23 24.50 26.50 28.50 110 110	.09 .04 .06	49.50 57 49.50 62.50 77 94 176 175.50	76 67 81.50 98.50 119 252 252 252
\$00	C C C C C C C C C C C C C C C C C C C	2 Rodm	29 29 31 29 27 27 25 6.50 6.50	514 .552 .573 .516 .552 .593 .640 2.462 2.462	CS.F.	32.50 46.56 26.50 38 50.50 65.50 66 65.50	24.50 24.50 24.50 26.50 28.50 110 110	.04	49.50 62.50 77 94 176 175.50	76 67 81.50 98.50 119 252 252
1800	R034136-90	2 Rodm	29 29 31 29 27 27 25 6.50 6.50	514 .552 .573 .516 .552 .593 .640 2.462 2.462 2.462 0.053 .024 .038	CS.F.	32.50 46.56 26.50 38 50.50 65.50 66 65.50	24,50 24,50 24,50 26,50 28,50 110 110	.04 .06	49.50 62.50 77 94 176 175.50	76 67 81.50 98.50 119 252 252 252 4.15 2.75 5.10
1300  6 x 6 · W2.9 x W2.9 (6 x 6) 42 lb, ner C.S.F.  1400  4 x 4 · W1.4 x W1.4 (10 x 10) 31 lb, per C.S.F.  1600  4 x 4 · W2.1 x W2.1 (8 x 8) 44 lb, per C.S.F.  1700  4 x 4 · W2.1 x W2.9 (6 x 6) 61 lb, per C.S.F.  1700  4 x 4 · W4 x W4 (4 x 4) 85 lb, per C.S.F.  1700  2 x 2 · #14 galv., 21 lb/C.S.F., becam & column wrap  2 x 2 · #12 galv. for gunite reinforcing  13 23 05.50 Prestressing Tendons  13 23 05.50 Prestressing Steel  1010  102  103  100' span, 100 kip  100' span, 100 kip  300 kip  200' span, 100 kip  300 kip  200' span, 100 kip  300 kip	R034136-90	2 Rodm	29 27 31 29 27 27 25 6.50 6.50 1200 2700 1700 3200	514 .552 .573 .516 .552 .593 .640 2.462 2.462 2.462	CS.F.	32.50 46.56 26.50 38 50.50 65.50 66 65.50	24.50 24.50 24.50 26.50 28.50 110 110 2.18 .97 1.54 .82	.04 .06 .03	49.50 62.50 77 94 176 175.50 4.60 2.06 3.93 2.87	76 67 81.50 98.50 119 252 252 252 6.15 2.75 5.10 3.57
1300	R034136-90 G G G G G G G G G G G G G G G G G G G	w 2 Radm	29 27 31 29 27 27 25 6.50 6.50 1200 2700 1700 3200 2700 2700	514 .552 .573 .516 .552 .593 .640 2.462 2.462 2.462 .053 .024 .038 .020 .024	CS.F.	32.50 46.56 26.50 38 50.50 65.50 66 65.50	24,50 23,24,50 26,50 28,50 110 110 2.18 .97 1.54 .82 .97	.04 .06 .03 .04	46.50 57 49.50 62.50 77 94 176 175.50 4.60 2.06 3.93 2.87 3.33	76 67 81.50 98.50 119 252 252 252 6.15 2.75 5.10 3.57 4.15
1300  6 x 6 · W2.9 x W2.9 (6 x 6) 42 lb, ner C.S.F.  1400  4 x 4 · W1.4 x W1.4 (10 x 10) 31 lb, per C.S.F.  1600  4 x 4 · W2.1 x W2.1 (8 x 8) 44 lb, per C.S.F.  1700  4 x 4 · W2.1 x W2.9 (6 x 6) 61 lb, per C.S.F.  1700  4 x 4 · W4 x W4 (4 x 4) 85 lb, per C.S.F.  1700  2 x 2 · #14 galv., 21 lb/C.S.F., becam & column wrap  2 x 2 · #12 galv. for gunite reinforcing  13 23 05.50 Prestressing Tendons  13 23 05.50 Prestressing Steel  1010  102  103  100' span, 100 kip  100' span, 100 kip  300 kip  200' span, 100 kip  300 kip  200' span, 100 kip  300 kip	R034136-90	w 2 Rodm	29 27 31 29 27 27 25 6.50 6.50 1200 2700 1700 3200 2700 3500 2600 3200 3200	514 .552 .573 .516 .552 .593 .640 2.462 2.462 2.462 .053 .024 .038 .020 .024 .018	CS.F.	32.50 46.56 26.50 38 50.50 65.50 66 65.50	24,50 23,24,50 26,50 28,50 110 110 2,18 97 1,54 82 97 7,75	.04 .06 .03 .04 .03	46.50 57 49.50 62.50 77 94 176 175.50 4.60 2.06 3.93 2.87 3.33 2.79	76 67 81.50 98.50 139 252 252 252 6.15 5.10 3.57 4.15 3.44

	11 05 - Normal Weight Structural	Contract		Daily	Labor		SAME INC.	2009 Bar	n facts		Total
3 31	05.30 Concrete, Field Mix		(rew	Output		Unit	Material	Labor	Equipment	Total	ind 0&P
010	CONCRETE, FIELD MIX	R033105-65				C.Y.	90	1000	SHEET -	90	99
)15 )20	FOB forms 2250 psi 3000 psi					n .	94			94	103
and the later of	05.35 Normal Weight Concrete, Ready Mix	(		_					SHEED HOLL		
010	NORMAL WEIGHT CONCRETE, READY MIX, delivered	R033105-10	.40					172376	(carrier)	V851	
012	Includes local aggregate, sand, portland cement, and water						and the same				
015	Excludes all additives and treatments	R033105-20	in i						90000		107
020	2000 psi		(CAN)			C.Y.	97			97	107
150	3000 psi	P033105-30		-	1230	Sec.	101			101	111
200	3500 psi	R033105-40					104			104	114
300	19000 JISI	11000105 10		-	B.S					100	
350	4500 psi	R033105-50					109			109	120
400	5000 psi	CN					411			111	122
411	6000 psi						127			127	139
412	8000 psi		130	T.LISS		RH2	206			206	227
413	10,000 psi						293			293 355	320 390
414	12,000 psi						355			222	370
000	For high early strength coment, add						10%			- 4	
010	For structural lightweight with regular sand, util					-1-	25% 5.25			5.25	5.8
300	For winter concrete (hot water), add						7.20			7.20	7.9
400	For hot wenther concrete (ice), add						3:95			3.95	4.3
410	For mid-range water reducer, add For high-range water reducer/superplasticizer, add						5.85			5.85	6.4
420 430	For retarder, add					100	2			2	2.2
440	For non-Chlorice accelerator, add						4.75			4.75	5.2
450	For Chloride accelerator, per 1%, add						2.75			2.75	3.0
460	For fiber reinforcing, synthetic (T Lb./C.Y.), add						é			6.	6.6
500	For Schurday delivery, add		Batt				5.50		Single	5.50	6.0
510	For truck holding/wairing time past 1st hour per load, add					Hr.	92			92	_ 101
520	For short load (less than 4 C.Y.), add per load		Tive S			.Eo.	100			100	110
000	For all lightweight aggregate, add			11.		C.Y.	45%				A SHIP AND A
3 3	1 05.70 Placing Concrete										
010	PLACING CONCRETE	R033105-70									
020	Includes labor and equipment to place and vibrate				51272					40.75	
050	Beams, elevated, small beams, pumped		C-20	60	1.067	C.Y.		36	13.15	49.15 81.50	7.0 113
100	With crane and bucket		(-7	45	1.600 .711			55 24	26.50 8.80	32.80	46.5
200	Large beams, pumped		C-20	90 65	1.108			38	18,40	56.40	78.5
250	With crane and bucket Columns, square or round, 12" thick, pumped		C-20	60	1.067			36	13.15	49.15	70
400 visn	With cone and bucket		C-7	40	1.800			61.50	30	91.50	127
450 4600	18" thick, pumped	ASSET VALUE OF	C-20	90	.711	THE ST		24	8,80	32.80	46.5
650	With crone and bucket		G7	55	1,309			45	.22	67	92.5
800	24" thick, pumped		C-20	92	.696			23.50	8,60	32.10	45.5
850	With crane and bucket		C7	70	1.029			35	17,10	52.10	73
000	36" thick, pumped		C-20	140	.457			15.50	. 5.65	21,15	29.5
050 400	Elevated slabs, less than 6" thick, pumped		C-20	140	.457			15.50	5.65	21.15	29.5
900	With Years and action		-4/	75	1/30		complements	O Mary Punch		STATE OF THE PARTY.	90.0
500	6" to 10" thick, pumped		C-20	160	400			13.55	4.94	18.49	26.5
1550	With crane and bucket		C-7	110	.655			22,50	10,90	33.40 16.44	46 23.5

00	24 61 -1 -1 -1			0	271	140	00			
	31 Structural Concrete		Y.							
03 3	1 05 - Normal Weight Structural Concre	te								
			Daily	Labor-	11:50	meer f	2009 Ba		Total	Total Incl 08
	05.70 Placing Concrete	Crew	Output	Hours .554	Unit C.Y.	Material	Labor 18.95	Equipment 9.20	Total 28.15	39
1650	With crone and bucket	G7.	130	400		SECTION.	13.20	.43	13.63	21
1900	Footings, continuous, shallow, direct chute	C-6 C-20	120	.400			14.45	5.25	19.70	28
1950	Pumped	(-7	90	.800			27.50	13.30	40.80	56.
2000	With craise and bucket	(-6	140	343			11.35	.37	11.72	17.
2100	Footings, continuous, deep, direct chute	6.20	160	400	NU DE	makuman	13.55	4.94	18.49	26.
2150	Pumped With crone and bucket	GZ.	110	655			22.50	10.90	33.40	46
2200			110	,033			29	10.30	00,10	-
2400	Footings, spread under 1 C.Y./ direct chute. Pumped	C-20	65	985		Name and Address of the Owner, where the Owner, which is the Owner, where the Owner, which is the Owner, whic	33.50	12.15	45.65	64.
7450	Tonipes	1020	-	100			Control of the last	20.30	89///8	
2600	Over 5 C.Y., direct chute	6-5	120	400			13.20	.43	- 13.63	21
2650	Pumped	C-20	150	427			14.45	5.25	19,70	28
2700	With crone and bucket	07	100	720			24.50	11.95	36.45	50.
2900	Foundation mats, over 20 C.Y., direct chate	C-6	350	.137	B IT	Will Street	4.53	.15	4.68	1.
2950	Pumped	C-20	400	.160			5,45	1.97	7.42	10.
3000	With crane and bucket	G7	300	240	134 171		8.20	3:99	12.19	16.
	Grode heams, Seart chute	on or	150	220	-		10.40	35	10.95	- IA
3250	Pumped	C-20	180	.356			12.05	4.39	16.44	23.
0.00	WIRKBUGSHARUSWA	E X 72	499	-180	SEC	SHOW SHAPE	THE PERSON	- BIRDS	STREET, SQUARE,	
3500	High rise, for more than 5 stories, pumped, add per story	C-20	2100	030			1.03	.38	1.41	1.
3510	With crone and bucket, add per story	(-7	2100	.034			1.17	.57	1.74	2.
3700	Pile caps, under 5 C.Y., direct chute	C-6	90	.533			17.65	.58	18.23	27.
3750	Pumped	C-20	110	.582			19.75	7.20	26.95	38
3800	With crone and bucket	67	80	.900			31	14.95	45.95	.63.
3850	Pile cop, 5 C.Y. to 10 C.Y., direct chute	C-6	175	.274			9.05	.30	9.35	14.
3900	Pumped	C-20	200	320			10.85	3.95	14.80	21
3950	With crane and backet	(-7	150	480			16.45	8	24.45	34
4000	Over 10 C.Y., direct chute	(-6	215	723			7,40	.24	7.64	11.
4100	Pumped	6.20	240	.267			9.05	3.29	12.34	27.
4100	With come and burlet	(7	185	.389	me la	ENDAR.	13.30	6.45	14.87	27
4350	Alab on grade, up to 6" that direct chute	C201	130		10100	DESCRIPTION.	16.70	6.10	22.80	32
1900	Pumped  Wair come with operate	C-Z0.	130	.472	100		102/0	0.10	22.00	J.L.
4600	Over 6" thick, direct chute	(-6	165	.291			9,60	.31	9.91	15.
4650	Pumped	C-20	185	346			11.75	4.27	16.02	22.
4700	With crone and bucket	67	145	497			17	8.25	25.25	35
4900	Walls, 3" thick, direct chute	(-6	90	533			17.65	.58	18.23	27.
4950	Pumped	C-20	100	.640		Talig of	21.50	7.90	29.40	41
5000	With crane and bucket	67	80	.900			31	14.95	45.95	63.
5050	12" thick, direct chate	C-6	100	.480	1		15.85	.52	16.37	25
5100	Pumped	C-20	110	.582			19.75	7.20	26.95	38
5200 5300	With crane and bucket	Ç-7	90	.300			27.50	13.30	40.80	56.
5350	15" thick, direct thute	(4	105	457			15.10	.49	15.59	23,
\$400	Pumped	C-70	120	.533			15.10	5.60	24.70	35
5600	With crone and bucket	(7	95	.758	7		26	12.60	38.60	53.
5610	Wheeled concrete dumping, odd to placing costs above									
5620	Wolking cort, 50" houl, udd	C-18	32	281	C.Y.		8.95	1,72	10.67	15.
5700	150' houl, odd		24	375			11.95	2.30	14.25	21
5800	250° houl, add	7	18	500			15.90	3,07	18.97	28
5810	Riding con, 50° houl, odd	0-19	80	113			3.58	1.08	4.66	Ď.
5900	150° houl, odd		50	150			4.77	1.44	9.21	.9.
10000	250' haul, and	7	45	200			4.35	1.92	1.27	11

2 2	E OC 20 Finishing Fig.	12	Daily	Labor	wes	5005 2055	2009 Ba	re Costs	SIZ	Total
	5 29.30 Finishing Floors	Crew	Output	Hours	Unit	Marerial	Lobor	Equipment	Total	Ind 0&
020	Manual screed finish	G10	4800	.005	S.F.		.18		,18	
125	Manual screed, bull floar, manual float		2000	.012			.43		.43	
150	Manual science, bull float, manual float & broom finish		1850	.013			.47		47	
200	Manual screet, but finat, manual floot, manual steel frewel		1265	.019			.68		.68	E.
250	Manual street, bull floot, machine floot & trawel (walk-behind)	C-10C	1715	.014			.50	.02	.52	
300	Power screed, bull float, machine float & trowel (walk-behind)	(-10D	2400	.010			.36	.05	.41	
350	Power screed, bull float, machine float & trowel (ride-on)	C-10E	4000	.006	DE L		.22	.03	.28	
400	Integral topping and finish, using 1:1:2 mix, 3/16" thick	C-108	1000	.040		.10	1.37	.24	1.71	2
450	1/2" thick		950	.042		.26	1.44	.25	1.95	2
500	3/4" thick		850	.047		.39	1.61	.28	2.28	3
600	1" thick	CITATION IN	750	.053		.52	1.83	11075-756	2.67	3.
300	Granolithic topping, laid after, 3:3:3-1/2 mix, 1/2" thick	1	590	.068		.29	2.32	.32	3.02	4.
120	3/4" thick		580	.069		43		.41		
350	1" thick		575	.070			2.36	.41	3.20	- 4
150	2" fikk	155-104-7-1-7-1	State of the last		Jan	.57	2.38	.42	3.37	4.
200	Heavy daty, 1:1:2, 3/4" thick, preshrunk, gray, 20:MSF		500	.080		1.15	2.74	.48	4.37	5
	100 MSF		320	.125		.73	4.29	.75	5.77	8
000			380	.105		.39	3.61	.63	4.63	6
00	Exposed local aggregate finish, minitruum	1 Cefi	625	.013		.22	.49	A STIESTIC	.71	
50	Maximum	- 17 10	465	.017		.66	.66		1.32	1
00	Floor obrasives, .25 psl, atominum axide		850	.009		.44	.36		_80	1.
50	Shicon corbide		850	.009		.61	.36		.97	1.
00	Flaor hardeness, metallic, light service, 150 psf, odd	46	850	.009		.51	.36		.87	1.
50	Medium service, .75 psf		750	.011		.76	.41		1.17	1.
00	Heavy service, 1.0 psf		650	.012	960	1,01	.47		1.48	1.
50	Extra heavy, 1.5 pst		575	,014		1.52	.53		2.05	2.
00	Non-matallic, light service, .50 psf		850	.009		.23	_36		.59	
350	Medium service, .75 psf		750	.011		.34	.41		.75	
00	Heavy service, 1.00 psf		650	.012		.45	.47		.92	1
50	Extra heavy, 1,50 psf	-	575	.014		.88.	.53		1.21	1,
00	Trap rack wearing surface for monolithic floors		36.00		v	.00	150		1,21	15
10	2.0 psf	C-10B	1250	.032	S.E.	.03	1.10	061.19	1.92	- 00
00	Floor coloring, dusted on, minimum (0.6 psf), add to above	1 Cefi	1300	.006		1100	1,10	.17	1,32	1.
50	Maximum (1.0.psf), add to above	i Cell	625			.43	.24		.67	
00	Colored powder only		02.3	.013	Y	71	.49		1.20	45
00		5.100	500	010	lb.				71	
	1/2" topping using 0.6 psf powdered color	C-108	590	.068	S.F.	4.86	2.32	.41	7,59	9.
50	1/2" topping using 1.0 psf powdered color		590	880.		5.15	2.32	.41	7.88	9.
00	Dustpraoling, solvent-based, 1 coat	1 Cefi	1900	.004		.17	.16		.33	
50	2 conts		1300	.006		.61	.24		.85	1.
00	Epoxy-based, 1 coat		1500	.005		.15	.20		.35	OHIV
50	2 coals		1500	.005	10	.29	.20	September 1	.49	
00	Stuir finish, floot		275	.029			137		1.11	1.
00	Steel trowel finish		200	.040	4		1.53		1.53	2.2
00	Silicon carbide finish, .25 psf		150	.053	W	.44	2.04		2.48	3.4
35	29.35 Control Joints, Saw Cut									
10	CONTROL JOINTS, SAW CUT	A to make	Sen I						W 15	. 20
00	Sowout in green concrete		1	312	0.00					
20	1" depth	C-27	2000	.008	LF.	.07	.31	.07	.45	
40	1-1/2" depth			.009		.10	.34	.08	.52	.7
60	2" death			.010		.13	.38	.09	.60	.8
00	Clean out centre/joint of debris	C-28		.001		.10	.05	.07	.05	.0

5 1	2 23 - Structural Steel for Buildings			0.4	takar			2009 Bar	a Carta		Total
			(rev		Labor- Hours	Unit	Materia	Labor	Equipmen!	Total	ind Q&P
	23.05 Canopy Framing CANOPY FRAMING							137.1	1000		0.00
20	6" and B" inembers, shop tobricated G		H	3000	.011	Lb.	1,80	:48	.04	2.32	2.89
	23.10 Ceiling Supports										
	The state of the s								0.00	64.00	78.50
00	Entrance door /folding partition supports, shop fabricated [G		H	60	.533	LF.	30	24	2.23	56.23 249.60	345
00	Linear perelerator done supports			14	2.286		137	103	9.60	26.40	32.50
00	Lintais or shalf angles, hung, exterior hat dipped galv.		181	267	120		20.50	5.40	.50 .50	23.65	29.50
50	Two costs primer point instead of galv.			267	.120	7	17.75	5.40	33.50	868.50	1,200
00	Monitor support, ceiling hung, expension boilted			4	8	Eu.	475 510	360 241	22.50	773.50	1,025
150	Hung from pre-set inserts			6	5.333		242	360	33.50	635.50	950
500	Mater supports for everhead doors			4	8	UE:	68.50	60.50	5:60	134.60	188
700	Portition support for heavy folding partitions, without pocket			24	1,333	LIF.	137	121	11:15	269.15	375
750	Supports at pocket only G			34	1941	+	58.50	42.50	3.94	104.94	145
000	Kalling dungs of the apot subbouss			8	4	fo.	195	181	16.75	392.75	555
100	Shight-ed light subhous, exhausion remort to coming was	교사	12/11	12	2.667		210	127	11.15	342.15	460
150	und use breze recers		l l	36	.889	LF.		40	3.72	112.22	151
100	toter parinter suppor	7		12	2.667	-	234	121	11.15	366.15	485
500	X-ray travel gality, supposi	-		14	4.79747			1/10/2		300	
5 1	2 23.15 Columns, Lightweight	-	1000					Serior	DIRECTOR !		Tables!
010	COLUMNS, LIGHTWEIGHT		ra.	780	.072	LE	6.10	3.13	2.23	11.46	14.50
000	Lightweight units (Ially), 3-1/2" diameter		E-2	900	:062	- W	8.95	2.71	1.93	13.59	16.5
050	4" diamete: Adjurtable jack past 8" maximum height 2-374" diameter	51		700	.002	Ea				33	36.5
800	Molingianic large boot, or attorney and a fine and a fine	3					53			53	56
850	4" Digitioner	-									
15 1	2 23.17 Columns, Structural		1-	-	-	-	1.				
010		, IV							194		
015	Made from recycled materials										
1020	Shop fris'd for 100-ten, 1-2 story project, behad connections		F-2	660	.085	LF	49.50	3.70	2.64	55.84	63.5
0800				780	.072		55	3,13	2.23	60.36	68.5
1830				1020		Н	65.50	2.39	1.71	69,60	78.5
0890	7 1 ANS. W			1200		Н	87	2.03	1.45	90.48	101
0930				1100			87	2.22	1.58	90.80	102
0940			1000	1998		U				.40	
1100			1 Ssw	k 945	.008	16	1,50		CHIEF THE BUILDING TO FE	1.88	2.3
1300		G	E2	1600	0 .004		1,50	.13		1.76	21
1500 1600		G		1400	0 .004		1.50		Charles and the same	1.79	2.
1700	Steel nine extra strong no concrete, 3" diameter x 12"-0"	G		60	.933	E	-1755	40.50	39600	254.50	305
1750	o 4" dicroster x 12'-0"	G		58	.966		270	42	30	342	400 680
180	6" diameter x 12"-0"	G	5	54	1.03		515	45	32	592	1,125
185		G		50	1.12		910	49	35	994 1,412.50	
190	A STATE OF THE STA	G		48	1.16	1965-75	1,325	51	36.50	1,867.50	2,075
195	0 12" dipmeter x 18"-9"	G		45			1,775	54	38.50	1.87	2,013
330	A Structural tribinal country A500GrR 4" to 4" sountry light section	G			0 .00				THE RESERVE OF THE PARTY OF THE	1.63	
360		G	. 4	3200	00 .007	-	1.50	-	0 .03	4.04	4
400	10 Concrete Filled, add			100	0.0		.F. 4.0		30	320	375
450	O Structural tubing, sq. 4" x 4" x 1/4" x 12'-0"	G					1 248	42	30	193	575
455	10 M M 17/0"	G	ALC: NO	54		100	THE PERSON NAMED IN	49	35	964	1,075
-		G		50			880	51	36.50	1,712.50	A LINE WATER
460	50 10" x 10" x 1/2" x 16'-0"	G	113	48	1,16		1,023	All Property lies	00.30	100	-
460	10 x 10 x 1/1 x 10 0										

500 520 560 580 700 740 900 100 300 320 940	.75 Structural Steel Members	6	Crew E-2	Output	Hours	Unit	Material	Labor	Equipment 1	Total	Ind 0&P
520 560 580 700 740 900 100 320 340	x 35 x 50 x 58 x 72	G	tex				100	and the second s	1.98	47,75	54
560 580 700 740 700 700 100 300 320 340	x 50 x 58 x 72	G		880	.064	L.E.	43	2.77	2.15	63.16	71
580 700 740 900 100 300 320 340	x 58 x 72			810	.069		58	3.07		88.07	99
700 740 900 100 300 320 340	x 72			750	.075		82.50	3.25	2.32		113
740 900 100 300 320 340		G	1	750	.075		95.50	3.25	2,32	101.07	
960 100 300 320 340	6.7	G		640	.088		119	3.81	2.72	125.53	140
100 300 320 340 360	x 87	G	N.	640	.088		144	3.81	2.72	150.53	167
300 320 340 360	W 14 x 26	G		990	.057		43	2.46	1.76	47.22	53
320 340 360	x 30	G		900	.062		49.50	2,71	1.93	54.14	61.
340 360	x 34	G		810	.069		56	3,01	2.15	61.16	69
360	x 43	G		810	.069		71	3.01	2,15	76.16	85.
	x 53	G		800	.070		87.50	3.05	2.18	92.73	304
	x 74	G	DE S	760	.074		122	3.21	2.29	127.50	142
380	x90	G	GIE	740	.076	Wis	149	3.30	2.35	154.65	171
100	of the supply of	(A)		720	079			0.00	2.42	203.81	226
700	W 16 x 26	G		1000	.056		43	2.44	1.74	47.18	33
900	X31	G		800	.070		66	3,05	2.18	71.23	80
100	x 40 x 50	G		800	.070		82.50	3.05	2.18	87.73	98.
120		G	Octo	760	.074	17103	111	3.21	2.29	116.50	130
140	x 67	G	E-5	960	.083		58	3.67	1.95	63.62	72
300	W 18 x 35	G	-1	960	.083		66	3.67	1.95	71.62	81
500	x 40	G	1		.083		76	3,67	1.95	81.62	92
520	x 46	G	O#K	960		1212	82.50	3.87	2.06	88.43	100
700	x 50			912	.088	ľ k.			2.06	96.93	109
900	x 55	G		912	880.		91	3.87	2.08	113	127
920	x 65	G		900	.089		107	3.92		131	147
940	x 76	G		900	.089	- 1	125	3.92	2.08	2500000	165
960	x 86	G		900	.089		142	3.92	2.08	148	
980	x 106	G	- 1	900	.089	80 3	175	3.92	2.08	181	201 87.
100	W 21 x 44	G		1064	.075	100	72.50	3.32	1.76	77.58	
300	x 50	G	SH	1064	.075	198	82.50	3.32	1.76	87.58	98.
500	х 62	G		1036	.077		102	3.41	1.81	107.22	121
700	x 68	G		1036	.077		112	3.41	1.81	117.22	131
720	x 83	G		1000	.080		137	3.53	1,88	142.41	159
740	x 93	G		1000	.080		153	3.53	1.88	158.41	177
760	x101	G		1000	.080		167	3,53	1.88	172.41	191
780	x122	G	H	1000	.080		201	3.53	1,88	206.41	229
900	W 24 x 55	G		1110	.072	1515	91	3.18	1.69	95.87	1107
100	x 62	G		1110	.072		102	3.18	1.69	106.87	120
300	x 68	G		1110	.072		112	3.18	1.69	116.87	130
500	x 76	G	1	1110	.072		125	3.18	1.69	129.87	145
700	x 84	G	1	1080	.074		139	3.27	1.74	144.01	160
720	x 94	G		1080	.074		155	3.27	1,74	160.01	179
740	x 104	G	lane.	1050		M 33	172	3.36	1.79	177.15	197
760	x 117	G	1616	1050	Florida Construction		193	3.36	1.79	198.15	220
780	1//	G		1050		1012	241	3.36	1.79	246,15	273
800	W 27 x 84	G		1190	.067	100	139	2.96	1258	143,54	159
700	# 114	G		1150	.070	A SAME	188	3.07	1.63	192.70	214
920	x 114	G		1150	2000000		241	3.07	1.63	245.70	272
940	x 146			1150			266	3.07	1.63	270.70	299
100	W 30 x 99	o en se per una relativida	1		.067		163	2.94	1.56	167.50	18/
1000	x 108 x 116			TZ-00	.069		191	3.04	1,62	195.66	218

-	121 16 – Longspan Steel Joist Frami	COLUMN SAN SAN SAN SAN SAN SAN SAN SAN SAN SA					Action of the second				
05 2	1 16.50 Longspan Joists	1 3 10	Crev	Daily v Qutpu	Labor- t Hours		Material	2009 Bi Labor	ore Costs Equipment	Total	Total Incl 08
2340	28LH11, 25 Lb/LF	G		1800	.044		28	1.96	1.12	31.08	35.
Z36U	320100, 17 W/D			1000			10.00		392	180	- SE/3
2380	32LH13, 30 Lb/LF 36LH09, 21 Lb/LF	G		1800	and the same	latio de la	34	1.96	1,12	37.08	42
2400	36LH14, 36 Lb/LF	G		1800	MARK SWIS		23.50	1.96	1.12	26.58	30
2420 2440	40UH10, 21 Ub/UF	G		1800			40.50	1.96	1.12	43.58	49
	40th15, 36 tb/tF			2200			23.50	1.60	.91	26,01	30
2460	The same of the sa	G	100	2200	.036	M) ke	40.50	1.60	.91	43,01	48
480	44LH11, 22 Lb/LF	G		2200			25	1.60	.91	27.51	31
500	44LH16, 42 Lb/LF	G		2200	.036		47,50	1,60	.91	50.01	56
520	48LH11, 22 Lb/LF	G		2200	.036		25	1.60	.91	27.51	31
540	48LH16, 42 Lb/LF	G	4	2200	.036	¥	47.50	1.60	.91	50.01	56
600	For less than 40-tan job lats										
602	For 30 to 39 tons, add						10%				
604	20 to 29 tons, add						20%				
506	10 to 19 tans, add				1000		30%				
507	5 to 9 tans, add	200 May 10 M 10 M 10 M 10			100000000000000000000000000000000000000		50%	25%	HINDERSON.	1000000	Carry Land
80	1 to 4 tons, add						75%	50%		46	
09	Less than I ton, add						100%	100%			
00	For welded cross bridging, add			8 1			140000	30%			
60	12K3, 5.7 lb/lF 14K3, 6.0 lb/lF	G G		1200 1500 1500	.053		5.10 5.80 6.10 6.40	2.94 2.35 2.35 1.96	1.57 1.34 1.34 1.12	9,71 9,49 9,79 9,48 11,33 10,61	12. 11. 12. 11. 13.;
000   000	16K3, 6.3 Lb/LF 16K6, 8.1 Lb/LF 18K5, 7.7 Lb/LF 18K9, 10.2 Lb/LF Span 30' to 50', minimum Average  Maximum 20K5, 8.2 Lb/LF 20K9, 10.8 Lb/LF 22K5, 8.8 Lb/LF			17 10 2000 2000	.044 .040 .040 .040 4.706 4.706 8 .040 .040	Ton V.F.	8.25 7.85 10.40 1,775 2,000 2,125 8.20 10.80 8.80	1.96 1.76 1.76 208 208 355 1.76 1.76	1 1 118 118 201 1	13.16 2,101 2,326 2,681 10.96 13.56	15.6 2,450 2,700 3,150 13.1 16.0
000000000000000000000000000000000000000	16K6, 8.1 Lb/LF 18K5, 7.7 Lb/LF 18K9, 10.2 Lb/LF Span 30' to 50', minimum Average CN Maximum 20K5, 8.2 Lb/LF			1800 2000 2000 17 17 10 2000 2000 2000 200	.044 .040 .040 4.706 4.706 8 .040 .040	1	7.85 10.40 1,775 2,000 2,125 8.20 10.80 8.80	1.76 1.76 208 208 355 1.76 1.76	1 118 118 201 1	2,101 2,326 2,681 10.96 13.56 11.56	2,450 2,700 3,150 13:1 16:0 13.8
00 00 00 00 00 00 00 00 00 00 00 00 00	16K6, 8.1 Lb/LF 18K5, 7.7 Lb/LF 18K9, 10.2 Lb/LF Span 30* to 50*, minimum Average  Average  Maximum 20K5, 8.2 Lb/LF 20K9, 10.8 Lb/LF 22K5, 8.8 Lb/LF	6 6 6 6		1800 2000 2000 17 17 10 2000 2000 2000 200	.044 .040 .040 4.706 4.706 8 .040 .040 .040	1	7.85 10.40 1,775 2,000 2,125 8.20 10.80 8.80 11.30	1.76 1.76 208 208 355 1.76 1.76 1.76	1 118 118 201 1	2,101 2,326 2,681 10.96 13.56 11.56 14.06	2,450 2,700 3,150 13:1 16:0 13.8 16:6
00 20 10 60 0 10 10 0 0 0	16K6, 8.1 Lb/LF 18K5, 7.7 Lb/LF 18K9, 10.2 Lb/LF Span 30* to 50*, minimum Average  Maximum 20K5, 8.2 Lb/LF 20K9, 10.8 Lb/LF 22K5, 8.8 Lb/LF 22K9, 11.3 Lb/LF	6 6 6 6 6		1800 2000 2000 17 17 10 2000 2000 2000 200	.044 .040 .040 4.706 4.706 8 .040 .040 .040 .040 .040	1	7.85 10.40 1,775 2,000 2,125 8.20 10.80 8.80 11.30 9.70	1.76 1.76 208 208 355 1.76 1.76 1.76 1.76	1 118 118 201 1 1 1 1 1	2,101 2,326 2,681 10.96 13.56 11.56 14.06 12.21	2,450 2,700 3,150 13:1 16:0 13:8 16:6 14.4
000 000 000 000 000 000 000 000	16K6, 8.1 Lb/LF 18K5, 7.7 Lb/LF 18K9, 10.2 Lb/LF Span 30* to 50*, minimum Average  Maximum 20K5, 8.2 Lb/LF 20K9, 10.8 Lb/LF 22K5, 8.8 Lb/LF 22K9, 11.3 Lb/LF 24K6, 9.7 Lb/LF			1800 2000 2000 17 17 10 2000 2000 2000 200	.044 .040 .040 4.706 8 .040 .040 .040 .040 .036 .036	1	7.85 10.40 1,775 2,000 2,125 8.20 10.80 8.80 11.30 9.70	1.76 1.76 208 208 355 1.76 1.76 1.76 1.76 1.76 1.60	1 118 118 201 -1 -1 -1 -1 -31 -31	2,101 2,326 2,681 10,96 13.56 11.56 14.06 12.21 15.61	2,450 2,700 3,150 13:1 16:0 13:8 16:6 14.4 18.2
000 000 000 000 000 000 000 000 000	16K6, 8.1 Lb/LF 18K5, 7.7 Lb/LF 18K9, 10.2 Lb/LF Span 30* to 50*, minimum Average  Maximum 20K5, 8.2 Lb/LF 20K9, 10.8 Lb/LF 22K5, 8.8 Lb/LF 22K9, 11.3 Lb/LF 24K5, 9.7 Lb/LF 24K10, 13.1 Lb/LF	6 6 6 6 6		1800 2000 2000 17 17 10 2000 2000 2000 200	.044 .040 .040 4.706 8 .040 .040 .040 .036 .036 .036	1	7.85 10.40 1,775 2,000 2,125 8.20 10.80 8.80 11.30 9.70 13.10 10.60	1.76 1.76 208 208 355 1.76 1.76 1.76 1.60 1.60	1 118 119 201 1 1 1 1 21 21 21 21	2,101 2,326 2,681 10.96 13.56 11.56 14.06 (2.21 15.61 13.11	2,450 2,700 3,150 13:1 16:0 13:8 16:6 14.4 18.2(
000000000000000000000000000000000000000	16K6, 8.1 tb/LF 18K5, 7.7 tb/LF 18K9, 10.2 tb/LF Spon 30' to 50', minimum Average CN Maximum 20K5, 8.2 tb/LF 20K9, 10.8 tb/LF 22K5, 8.8 tb/LF 22K9, 11.3 tb/LF 24K6, 9.7 tb/LF 24K10, 13.1 tb/LF 26K6, 10.6 tb/LF			1800 2000 2000 17 17 10 2000 2000 2000 200	.044 .040 .040 4.706 8 .040 .040 .040 .040 .036 .036 .036	1	7.85 10.40 1,775 2,000 2,125 8.20 10.80 8.80 11.30 9,70 13.10 10.60 13.80	1.76 1.76 208 208 355 1.76 1.76 1.76 1.60 1.60 1.60	1 118 118 201 -1 1 1 1 -2 1 -3 1 -9 1 -9 1 -9 1 -9 1	2,101 2,326 2,681 10.96 13.56 11.56 14.06 12.21 15.61 13.11 16.31	2,450 2,700 3,150 13:1 16:0 13:8 16:6 14.4 18.2 15:4 19
00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	16K6, 8.1 tb/LF 18K5, 7.7 tb/LF 18K9, 10.2 tb/LF Span 30° to 50°, minimum Average Maximum 20K5, 8.2 tb/LF 20K9, 10.8 tb/LF 22K5, 8.8 tb/LF 22K9, 11.3 tb/LF 24K5, 9.7 tb/LF 24K10, 13.1 tb/LF 26K6, 10.6 tb/LF 26K10, 13.8 tb/LF			1800 2000 2000 17 17 10 2000 2000 2000 200	.044 .040 .040 4.706 8 .040 .040 .040 .036 .036 .036 .036 .036 .036	1	7.85 10.40 1,775 2,000 2,125 8.20 10.80 8.80 11.30 9.70 13.10 10.60 13.80 12.70	1.76 1.76 208 208 355 1.76 1.76 1.76 1.60 1.60 1.60 1.60	1 118 118 201 1 1 1 1 91 91 91 91 91	2,101 2,326 2,681 10.96 13.56 11.56 14.06 12.21 15.61 13.11 16.31 15.91	2,450 2,700 3,150 13:1 16:0 13:8 16:6 14.4 18.2 15.4 19
00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	16K6, 8.1 tb/LF 18K5, 7.7 tb/LF 18K9, 10.2 tb/LF Spoil 30° to 50°, minimum Average Maximum 20K5, 8.2 tb/LF 20K9, 10.8 tb/LF 22K5, 8.8 tb/LF 22K9, 11.3 tb/LF 24K6, 9.7 tb/LF 24K10, 13.1 tb/LF 26K6, 10.6 tb/LF 26K10, 13.8 tb/LF 26K8, 12.7 tb/LF			1800 2000 2000 17 17 10 2000 2000 2000 200	.044 .040 .040 4.706 4.706 8 .040 .040 .040 .036 .036 .036 .036 .033 .033	1	7.85 10.40 1,775 2,000 2,125 8.20 10.80 8.80 11.30 9.70 13.10 10.60 13.80 12.70 17.10	1.76 1.76 208 208 355 1.76 1.76 1.76 1.60 1.60 1.60 1.40 1.47	1 118 118 201 1 1 1 1 1 2 91 91 91 91 34 84	2,101 2,326 2,681 10,96 13.56 11.56 14.06 12.21 15.61 13.11 6.31 15.01 19.41	2,450 2,700 3,150 13:3 16:0 13:8 16:6 14.4 18.2 15:4 19 17.4 122.50
00   20   40   50   10   60   70	16K6, 8.1 tb/LF 18K5, 7.7 tb/LF 18K9, 10.2 tb/LF Span 30* to 50*, minimum Average  Mosimum 20K5, 8.2 tb/LF 20K9, 10.8 tb/LF 22K5, 8.8 tb/LF 22K9, 11.3 tb/LF 24K5, 9.7 tb/LF 24K10, 13.1 tb/LF 26K6, 10.6 tb/LF 26K10, 3.8 tb/LF 28K12, 1tb/LF 28K12, 17.1 tb/LF 28K12, 17.1 tb/LF			1800 2000 2000 17 17 10 2000 2000 2000 200	.044   .040   .040   .040   .040   .040   .040   .040   .040   .040   .040   .040   .036   .036   .036   .033   .0	1	7.85 10.40 1,775 2,000 2,125 8.20 10.80 8.80 11.30 9.70 13.10 10.60 13.80 12.70 17.10 13.20	1.76 1.76 208 208 355 1.76 1.76 1.76 1.60 1.60 1.60 1.47 1.47	1 118 118 201 1 1 1 1 1 2 91 91 91 91 91 91 84 84	2,101 2,326 2,681 10,96 13,56 11,56 14,06 12,21 15,61 13,11 6,31 15,01 19,41 15,51	2,450 2,700 3,150 13:1 16:0 13.8 16:6 14.4 18.2 15:4 19 17,4 122.5 17.95
DD 200 140 160 160 160 160 160 160 160 160 160 16	16K6, 8.1 tb/LF 18K5, 7.7 tb/LF 18K9, 10.2 tb/LF Span 30° to 50°, minimum Average Maximum 20K5, 8.2 tb/LF 20K9, 10.8 tb/LF 22K5, 8.8 tb/LF 22K9, 11.3 tb/LF 24K6, 9.7 tb/LF 24K10, 13.1 tb/LF 26K6, 10.6 tb/LF 26K10, 13.8 tb/LF 28K12, 17.1 tb/LF 28K12, 17.1 tb/LF		*	1800 2000 2000 17 17 10 2000 2000 2000 200	.044 .040 .040 4.706 4.706 8 .040 .040 .040 .036 .036 .036 .036 .033 .033	1	7.85 10.40 1,775 2,000 2,125 8.20 10.80 8.80 11.30 9.70 13.10 10.60 13.80 12.70 17.10	1.76 1.76 208 208 355 1.76 1.76 1.76 1.60 1.60 1.60 1.40 1.47	1 118 118 201 1 1 1 1 1 2 91 91 91 91 34 84	2,101 2,326 2,681 10,96 13.56 11.56 14.06 12.21 15.61 13.11 6.31 15.01 19.41	2,450 2,700 3,150 13:1 16:0 13:8 16:6 14:4 18:2 15:4 19 17:40 22:50

	31 23 - Steel Roof Decking	SERVICE:	12000	Daily	Labor	military.	SHUUTE	2009 Ba	re Costs	54078	Total
15 3 2200	1 23.50 Roof Decking 50-500 soupres	G	Erew F-4	100000		Unit	Material	Labor	Equipment	Total	Incl O&
400	50-500 squares CN Over 500 squares	G	L-e	5160		S.F.	2	.30 .28	.03	2.33	2.
2600	20 gauge, under 50 squares	G		3865			3.03	.37	.03	3,43	2. 4.
650	50-500 squares	G		4170			2.42	.35	.03	2.80	3.
700	Over 500 squares	G		4300			2.18	.34	.03	2.55	3.0
900	18 gauge, under 50 squares	G		3800			3.91	.38	.04	4.33	51
950	50-500 squares	G		4100	11220		3.13	.35	.03	3.51	4.
000	Over 500 squares	G		4300	THE LABORY OF		2.82	.34	.03	3.19	3.
050	16 gauge, under 50 squares	G		3700	.009		5,25	.39	.04	5.68	6.
060	50-500 squares	G	1	4000	.008	1	4.21	.36	.03	4.60	5.3
100	Over 500 squares	G		4200	.008		3.79	.34	.03	4.16	4,1
150	For intermediate rib instead of wide rib, deduct	G	1	9000			.04		5387	.04	
160	For narrow rib instead of wide rib, add	G					.79			.79	
15	31 38 - Steel Form Decking	FRE VENT			J.W.				Ser.	Test.	1 B2
-	1 33.50 Form Decking						-112-Lan Wit				
010	FORM DECKING							Market 1			
100	Slab form, steel, 28 gauge, 9/16" deep, uncoated	G	E-4	4000	,008	5.E.	1.72	.36	.03	2,11	2.
220	24 gauge, 1" deep, uncoated	G		3900	800.		1,32	.36	.03	2.27	2.3
240	Galynnized	G		3900	.008		2.20	.37	.03	2.60	3.
300	24 gauge, 1-5/16" deep, uncoated	G		3800	.008		1.99	.35	.04	2.41	2.9
400	Galennized	G		3800	.008		2.34	.38	.04	2.76	3.5
500	27 gauge, 1-5/16" deep, uncoated	G		3700	.009		2.50	.39	.04	2.93	3,
600	Galvanized	G		3700	.009		2.55	.39	.04	2.98	3.5
700	22 gauge, 2" deep uncoated	G		3600	.009		3.28	.40	.04	3.72	4.3
800	Golvanized	G	+	3600	.009	w	3.22	.40	.04	3.66	4.3
000	Sheet metal edge clasure form, 12" wide with 2 bends, galv									-	Till Order
100	18 gauge	G	E-14	360	.022	1.7.	5.30	1.04	.37	6.71	8.1
200	16 gauge	G	02	360	.022	20	7.20	1.04	.37	8.61	10.1
A STATE OF	35 13 - Steel Cellular Decking 5 13.50 Cellular Decking	ssem	olie	25							
010	CELLULAR DECKING		eve jii			NEW T					
115	Made from recycled materials										
50	Cellular units, galv, 2" deep, 20-20 gauge, over 15 squares	G	E4	1460	.022	S.F.	10.20	.99	.09	11,28	18,7
300	18-20 gauge 18-18 gauge	G	3266	1420	.023		11.60	1.02	.09	12.71	14.7
20	16-16 gauge	G		1390	.023		11.95	1.04	.10	13.09	15.1
40	16-16 gauge	G		1360	.024		14.20	1.06	.10	15.36	17.6
100	3" deep, golvenized, 20-20 gouge	G		1330 1375	.024		15.85	1.09	.10	17.04	19.4
00	18-20 gruge	G	55/00	1350	.024	PS SING	11.25 13.60	1.05	.10	12.40	14.3
000	18-18 gauge	G		1290	.025		13.55	1.12	.10 .10	14.77	17.0
00	16-18 gauge	G		1230	.025		15.25	1.12	.10	16.54	17.0
00	16-16 gauge	G		1150	.028		16.65	1.26	.12	18.03	20.5
	4-1/2" deep, galvanized, 20-18 gauge	G	-	1100	.029	-500	15.70	1.31	.12	17.13	19.7
	18-18 gauge	G		1040	.031		15.60	1.39	.13	17.12	19.7
00					.033		17.55	1.48	.14	19.17	22
00 00 00	16-18 gauge	G		980	.000			(24D )	14	17.17	11

	2 13 - Built-Up Asphalt Waterproofing		Daily	Lobor-	Title	Material	2009 Bar Labor	Costs Equipment	Total	Total Incl Q&P
	13.20 Membrane Waterproofing MEMBRANE WATERPROOFING	(rew	Output	Hours	Unit	AVGIETIG:	Land	Edolbuseu	10101	mer gog
12	On slabs, 1 ply, felt, mopped	61	3000	.019	S.E.	.34	.60	.15	1.09	1.5
00	On slabs, 1 ply, glass finer Tabric, mapped		2100	.027		.36	.85	.21	1.42	2.0
00	On slabs, Z ply, felt, mapped		2500	.022		.69	.72	.18	1.59	2.1
00	On slobs, 2 ply, gloss fiber fabric, mopped		1650	.034		79	1.09	.27	2.15	2.9
00	On slobs, 3 ply, felt, mopped		2100	.027		1.03	.85	.21	2.09	2.8
00	On slabs, 3 ply, glass fiber fabric, mopped		1550	.036		1.07	1.16	.28	2.51	3.4
10	Asphaltic hardboard protection board, 1/8" thick	2 Kate	500	.032		.40	1.10		1.50	2.2
100	1/4" EPS membrane protection board		3500	.005		.21	16		.37	A
150	3/8" thick	3.00	3500	.005		23	.16	3,000	.39	5
080	1/2" thick		3500	.005		.26	.16		.42	5
70	Fiberglass fabric, black, 20/10 mesh		116	.138	Sq.	18	4.72		22.72	28
180	White, 20/10 mesh		116	.138		18	4,72		22.72	28
7	13 Sheet Waterproofing									
	3 53 - Elastomeric Sheet Waterproofi		8677	3/1/63	1181	A THE REAL PROPERTY.	OCTO, -			
-	53.10 Elastomeric Sheet Waterproofing and Acco	ess.	-		_					- 3
110	ELASTOMERIC SHEET WATERPROOFING AND ACCESS.	001	700	nac	20.0	1.70	30		2.14	2.9
)9()	EPDAN, plain, 45 mis thick.	2 Rafa		.028	S.F.	1.19	.95 .96		2.21	2.9
00	60 mils thick		570	.028		1.25	.95		2.11	2.8
00	Nylon reinforced sheets, 45 mils thick		580	.028		1.16	.73		2.43	3.2
100	60 mils thick	4:	570	.028	1	1,47	76		43.50	47,5
600	Vulcanizing splicing tupe for above, 2" wide				CLE	43.50			99.50	109
700	4" wide					99.50			16.50	18.1
900	Adhesive, bonding, 60 SF per go				Goi.	16.50				35
000	Splicing, 75 SF per gol					-32			32	3.4
200	Neoprene sheets, plain, 45 mils thick	2 Refe		.028	S.E.	1.68	.95		2.63	4.7
300	60 mils thick		570	.028		2.86	.96		3.82	3.5
500	Nylon reinforced, 45 mils thick		580	.028	1311	1.75	.95			4.3
600	60 mils thick		570	.028		2.46	.96		3.42	6.2
800	120 mils filiok	v	500	.032	w	4	1.10		5.10	19.2
900	Adhesive, splicing, 150 S.F. per gal, per coat				Gai.	17.50			17.50	3.9
100	Fiberglass reinforced, fluid applied, 1/8" thick	2 Rot		.032	S.F.	1.88	1.10	consists/contra	2.98	
200	Polyethylene and rubberized asphalt sheets, 1/8" thick	10	550	.029	100	.73	1		1.73	2.9
210	Asphaltic hardboard protection board, 1/8" thick		500	.032		.40	1.10	1000	1.50	2.5
220	1/4" thick		450	.036		.68	1.22		1,90	23
400	Polyvinyl chloride sheets, plain, 10 mils thick		580	.028	791	.17	.95		1,12	and Ha
500	20 mis thick		570	,028		.28	.96		1.24	1.5
700	30 mils thick	v	560	.029	w	.39	.98		1.37	2.0
	Adhesives, trowel grade, 40-100 SF per gal				Gal	27			27	29.5
000	Brush grade, 100-250 SF per gal.			those	"	27			27	29.
000 100	para different programme fluid analysis S5 mile think	9 Pn		.034	100	1.20	1.15	WE'CVE S	2,35	3.

	63 26 - Drilled Caissons									
4	3 26.13 Fixed End Cassion Piles	Ten	Daily		1000	Hereit !		are Costs	1601	Toto
10	FIXED END CASSION PILES R316326-60	£rew.	ouipt	Hour:	Unit	Materia	Lobor	Equipment	lote	incl O&P
15	Including excavation, concrete, 50 lbs reinforcing									
20	per C.Y., not incl. mobilization, boulder removal, disposal									
00	Open style, machine drilled, to 50° deep, in stable ground, no									
10	cusings or ground water, 18" diam., 0.065 C.Y./L.F.	B-43	200	.240	VLE	9.05	8.30	12.65	30	36,50
00	24" diometer, 0.116 C.Y./L.F.		190			16.20		13.35	38.30	46
00	30" diameter, 0.182 C.Y. /L.F.		150	.320		25.50	11.10	16.90	53,50	63.50
00	36" diameter, 0.262 C.Y./L.F.		125	.384		36.50	13.30	20.50	70.30	83
00	48" diameter, 0.465 C.Y./L.F.		100	480	E	65	16.60	25.50	107.10	125
00	60" diameter, 0.727 C.Y./L.F.		90	.533		102	18.45	28	148.45	172
00	72" diameter, 1.05 C.Y./L.F.	A H	80	.600		147	21	31.50	199,50	229
00	84" diameter, 1.43 C.Y./L.F.		75	.640		200	22	34	256	291
00	For bell excavation and concrete, add				2.04		arabia raj			
20	4" bell diameter, 24" shaft, 0.444 C.Y.	B-43	20	2.400	Ec.	+ 45	83	127	255	315
0	6" hell diameter, 30" shaft, 1.57 C.Y.		5.70			159	292	445	896	1,100
0	8' bell diameter, 36" shaft, 3.72 C.Y.	10.	2.40	20		375	695	-1,050	2,120	2,625
10	91 bell diameter, 48" shaft, 4.48 C.Y.		2	24		450	830	1,275	2,555	3,175
10	10' bell diameter, 60" shaft, 5.24 C.Y.		1.70	28.235		530	980	1,500	3,010	3,725
0	12" bell diameter, 72" shaft, 8.74 C.Y.	111	1	48		885	1,650	2,525	5,060	6,300
0	14' bell diameter, 84" shaft, 13.6 C.Y.	-	.70	68.571	*	1,375	2,375	3,625	7,375	9,125
0	Open style, machine crilled, to 50" deep, in wet ground, pulled									
Q.	rasing and pumping, 18" diag per, 0.065 C.Y./L	8-48	160	.350	VLF	9.05	35	17.90	39,30	48.50
0	36" dis no 10.262 C.Y./L.E 49805 efek 0.465 C.Y.	15-45	X	.600 2.514		25.50 45 102	23 12 50.50	66.50	117	935
		16-45	30 25	.92 .600 2.514 2.933 3.520		d5	58.50 58.50 108 129		117 10 377 475	235 460 580
0 0 0	48 day wells 0,465 C.Y.  50 wanters, 0.757 C.Y./L.F.  72" diameter, 1.05 C.Y./L.F.  84" dispeter, 1.43 C.Y./L.F.  For hell of syrvian and or krets, odd	16-49	25	2.514 2.933 3.520		65 102 147	58.50	66.50	377	
0	48 day etc. 0.465 C.Y.  72" diameter, 1.05 C.Y./L.F. 84" director, 1.43 C.Y./L.F. For hell of Avarian and of Arete, odd  79 de Julynstein, 2 sincul, 0.452	8-48	25	2.514 2.933	Eq.	65 102 147	58.50	66.50	377	
0	48 day wells 0,465 C.Y.  50 wanters, 0.757 C.Y./L.F.  72" diameter, 1.05 C.Y./L.F.  84" dispeter, 1.43 C.Y./L.F.  For hell of syrvian and or krets, odd	8-48	25 19,89	2.933 3.520 2.83		147 200	58.X0 108 129 99.80	66.50 122 146	377 475 29 a0	580 300
0	48 day etc. 0.465 C.Y.  72" diameter, 1.05 C.Y./L.F. 84" director, 1.43 C.Y./L.F. For hell of Avarian and of Arete, odd  79 de Julynstein, 2 sincul, 0.452	18-48 18-49	25 19,80 3,70 2,40	2.514 2.933 3.520		65 102 147 200	58.50 108 129	66.50 122 146	377	
0 0	48 duty efek 0,455 C.Y.  or wanter, 0.7 c.Y./L.F.  72" diomete, 1.05 C.Y./L.F.  84" dispeter, 1.43 C.Y./L.F.  For hell or wanten and or crete, odd  Virules/orderete, 2. snoq. 0.449 24.  Desironnellis, 50. snoq. 1.157 C.E.	WE	25 19,80 3,70 2,40	2.514 2.933 3.520 2.83 7.52		65 102 147 200 137 375	58.50 108 129 99.50 99.50	66.50 122 146	377 475 77 400	580 - arch 2,975
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	48 duty efek 0,455 C.Y.  or wanter, 0.7 c.Y./L.F.  72" diomete, 1.05 C.Y./L.F.  84" dispeter, 1.43 C.Y./L.F.  For hell or wanten and or crete, odd  Virules/orderete, 2. snoq. 0.449 24.  Desironnellis, 50. snoq. 1.157 C.E.	WE	25 19,80 3,70 2,40	2.514 2.933 3.520 2.83 7.52		65 102 147 200 137 375	58.50 108 129 99.50 97.5	66.50 122 146 149 1200	377 475 27 - 00 2,400 2,525	2.975 2.975 5,575
0 0 0 0 0 0	48 cury cles Q.455 C.Y.  or wanters, U.757 C.Y./L.F.  84* degreter, 1.43 C.Y./L.F.  For hell or weeting and gracete, add  or see counters, 2 strong, 0.49 etc.  ese counters, 30 strong, 0.49 etc.  91 hell diameter, 48* shoft, 4.48 C.Y.  12' bell diameter, 72* shoft, 8.74 C.Y.  14' bell diameter, 84* shoft, 1.3.6 C.Y.	WE	19,88 19,88 3,74 2,40 3,30	2.514 2.933 3.520 2.81 23.333 20.067		147 200 375 450	108 129 99280 975 1100	66.50 122 146 144 1200 1,100	377 475 22 00 7,400 2,525 2,980	580 - arch 2,975
0 0 0 0 0 0 0	48 covered et al. 485 C.Y.  58 contractes, 0.75 C.Y./L.F.  84° discretes, 1.43 C.Y./L.F.  84° discretes, 1.43 C.Y./L.F.  For hell or execution and of cretes, odd  10 des, ordeness, 20 strong, 0.44 get.  11 des countries, 30 strong, 0.44 get.  12 bell diameter, 48° shoft, 4.48 C.Y.  12 bell diameter, 48° shoft, 8.74 C.Y.  14 bell diameter, 84° shoft, 13.6 C.Y.  Open style, machine drilled, to 50° deep, in soft rocks and	8-49 W	25 19,80 2,40 3,30 1,60	2.914 2.933 3.520 2.81 23.333 20.067 55 88		45 102 147 200 375 450	55 0 108 129 99.50 875 975 120 2,025	66.50 127 146 149 1,200 1,100 1,300 1,300 2,275	377 475 27 - 00 7 400 2,525 7 980 5,185 8,250	2,975 2,975 6,575 10,500
0 0 0 0 0 0 0	48 covered & 0.45 C.Y.  58 contactor, 0.52 C.Y./L.F.  84" discrete; 1.43 C.Y./L.F.  84" discrete; 1.43 C.Y./L.F.  For hell or exprision and contrete, add  of pee, originate, 30 short, 94-year.  91'hell diameter, 48" short, 4.48 C.Y.  12' bell diameter, 48" short, 4.48 C.Y.  14' bell diameter, 84" short, 13.6 C.Y.  Open style, machine drilled, to 50' deep, in soft rocks and medium hard shales, 18" diameter, 0.065 C.Y./L.F.	WE	25 19,80 2,40 3,30 1,60	2.514 2.933 3.520 2.82 23.333 20.007		45 102 147 200 375 450	55 0 108 129 99.50 875 975 120 2,025	66.50 127 146 149 1,200 1,100 1,300 1,300 2,275	377 475 2 400 2,525 7 980 5,185 8,250 146,55	580 240 2,975 3,375 6,575 10,500
0 0 0 0 0 0 0	48 convertee 0,465 C.Y.  50 connecter, 1.05 C.Y./L.F.  84" discrete, 1.43 C.Y./L.F.  84" discrete, 1.43 C.Y./L.F.  For hell of evaping and of crete, odd  of dec./Gorester, 2. singly, 0.45 gar.  51' hell diameter, 48" shoft, 4.48 C.Y.  12' hell diameter, 72" shoft, 8.74 C.Y.  14' bell diameter, 84" shoft, 13.6 C.Y.  Open style, machine drilled, to 50' deep, in soft rocks and medium hard shales, 18" diameter, 0.065 C.Y./L.F.  24" diameter, 0.116 C.Y./L.F.	8-49 W	25 19,80 2,40 3,30 1,60	2.914 2.933 3.520 2.81 23.333 20.067 55 88		65 102 147 200 375 450 885 1,375	58.00 108 129 97.50 47.5 97.5 97.5 2,025 3,225	127 146 149 1,200 1,100 1,100 2,275 3,650	377 475 2 400 2,525 2 980 5,185 8,250 146,55 246,20	580 2975 377 6575 10,500
	48 convertee 0.465 C.Y.  72" diameter, 0.52 C.Y./L.F. 84" diameter, 1.43 C.Y./L.F. 84" diameter, 1.43 C.Y./L.F. For hell of execution and 5° crete, odd  71 des orderes, 2 short, 0.45 2.Y.  9"hell diameter, 48" short, 4.48 C.Y.  12' bell diameter, 72" short, 8.74 C.Y.  14' bell diameter, 84" short, 13.6 C.Y.  Open style, machine drilled, to 50' deep, in soft rocks and medium hard shales, 18" diameter, 0.065 C.Y./L.F.  24" diameter, 0.116 C.Y./L.F.  30" diameter, 0.182 C.Y./L.F.	8-49 W	25 19,88 2,40 3,30 1,60 1 50 30 20	2.514 2.933 3.520 2.82 23.333 20.667 55 88 1.760 2.933 4.400		65 102 147 200 375 450 885 1,375 9,05 16,20 25,50	58.00 108 129 99.80 99.80 97.5 110 2,025 3,225 64.50 108 161	122 146 149 1,100 1,100 2,275 3,650 73 122 183	377 475 2 400 2,505 7 900 5,185 8,250 146,55 246,20 369,50	580 2975 377 6,575 10,500 190 320 480
	48 downsteller 0,465 C.Y.  72" diameter, 0.52 C.Y./L.F. 84" diameter, 1.43 C.Y./L.F. 84" diameter, 1.43 C.Y./L.F. For hell of evenion and 5° crete, odd  41 des downsteller, 2 short, 0.40 get.  91' hell diameter, 48" short, 4.48 C.Y.  12' hell diameter, 72" short, 8.74 C.Y. 14' hell diameter, 34" short, 13.6 C.Y.  Open style, machine drilled, to 50' deep, in soft rocks and medium hard shales, 18" diameter, 0.065 C.Y./L.F. 24" diameter, 0.116 C.Y./L.F. 30" diameter, 0.12 C.Y./L.F. 36" diameter, 0.262 C.Y./L.F.	8-49 W	25 19,80 3,30 3,30 1,60 1 50 30 20 15	2.81 2.933 3.520 2.82 23.333 26.667 55 88 1.760 2.933 4.400 5.867		65 102 147 200 375 450 885 1,375 9,05 16,20 25,50 36,50	58.00 108 129 99.80 97.5 1.10 2.025 8.225 64.50 108 161 215	122 146 144 144 1,100 1,100 1,200 2,275 3,650 73 122 183 243	7400 2,525 2,90 3,85 8,250 146,55 246,20 369,50 494,50	580 2,975 3,775 6,575 10,500 190 320 480 640
	48 convertee 0.465 C.Y.  50 connectes, 1.05 C.Y./L.F.  84" discrete, 1.43 C.Y./L.F.  84" discrete, 1.43 C.Y./L.F.  For hell of execution and 5° crete, odd  51 des objectes, 2 short, 3.75 C.Y.  9" hell diameter, 48" short, 4.48 C.Y.  20 connectes, 34" short, 4.48 C.Y.  112' hell diameter, 72" short, 8.74 C.Y.  14' bell diameter, 84" short, 1.3.6 C.Y.  Open style, machine drilled, to 50' deep, in soft rocks and medium hard shales, 18" diameter, 0.065 C.Y./L.F.  24" diameter, 0.116 C.Y./L.F.  30" diameter, 0.12 C.Y./L.F.  36" diameter, 0.262 C.Y./L.F.  48" diameter, 0.465 C.Y./L.F.	8-49 W	25 19,80 2,40 3,30 1,60 1 50 30 20 15 10	2.514 2.933 3.520 2.61 2.61 2.61 5.62 5.62 8.8 1.760 2.933 4.400 5.867 8.800		885 1,375 450 885 1,375 9,05 16,20 25,50 36,50 65	58.00 108 129 99.20 99.20 97.5 97.5 1.10 2.025 3.225 64.50 108 161 215 325	122 146 149 1,200 1,100 1,100 2,275 3,650 73 122 183 243 365	377 475 2 400 2,505 2,700 5,185 8,250 146,55 246,20 369,50 494,50 755	580 2,975 3,775 6,575 10,500 190 320 480 640 945
	48 convertee 0.465 C.Y.  50 container, 0.52 C.Y./L.F.  84" dispater, 1.43 C.Y./L.F.  84" dispater, 1.43 C.Y./L.F.  For hell of exection and 5° crete, odd  50 des objectes, 2° short, 0.45° 20.  9" hell diameter, 48" short, 4.48 C.Y.  9" hell diameter, 48" short, 1.3.6 C.Y.  12' hell diameter, 27" short, 8.74 C.Y.  14' hell diameter, 84" short, 1.3.6 C.Y.  Open style, machine drilled, to 50' deep, in soft rocks and medium hard shales, 18" diameter, 0.065 C.Y./L.F.  24" diameter, 0.116 C.Y./L.F.  30" diameter, 0.182 C.Y./L.F.  48" diameter, 0.465 C.Y./L.F.  60" diameter, 0.727 C.Y./L.F.	8-49 W	25 19,60 3,30 1,60 1 50 30 20 15 10 7	2.933 3.520 2.83 23.333 20.667 555 88 1.760 2.933 4.400 5.867 8.300 12.571		885 1,375 450 885 1,375 9,05 16,20 25,50 36,50 65	58.00 108 129 99.20 99.20 97.5 1.10 2.025 3.225 64.50 108 161 215 325 460	122 146 149 1,200 1,100 1,100 2,275 3,650 73 122 183 243 365 520	377 475 2 400 2,505 2,700 5,185 8,250 146,55 246,20 369,50 494,50 755 1,082	580 2775 2775 3775 10,500 190 320 480 640 945 1,400
	48 convertee, 0.465 C.Y.  72" diameter, 0.52 C.Y./L.F. 84" diameter, 1.05 C.Y./L.F. 84" diameter, 1.43 C.Y./L.F. For hell of avanian and 5° crete, odd 7 des diameter, 38" short, 4.48 C.Y.  9" hell diameter, 48" short, 4.48 C.Y.  12" hell diameter, 48" short, 1.3.6 C.Y.  14" hell diameter, 84" short, 1.3.6 C.Y.  Open style, machine drilled, to 50" deep, in soft rocks and medium hard shales, 18" diameter, 0.065 C.Y./L.F. 24" diameter, 0.116 C.Y./L.F. 30" diameter, 0.182 C.Y./L.F. 48" diameter, 0.465 C.Y./L.F. 60" diameter, 0.727 C.Y./L.F. 72" diameter, 1.05 C.Y./L.F.	8-49 W	25 19,60 3,30 1,60 1 50 30 20 15 10 7	2.514 2.933 3.520 2.83 23.333 20.667 555 88 1.760 2.933 4.400 5.867 8.300 12.571 14.667	¥ VLE	885 1,375 9,05 16,20 25,50 36,50 65 102 147	50.00 108 129 99.80 97.5 17.5 17.5 2,025 3,225 64.50 108 161 215 325 460 540	122 146 149 1,200 1,100 2,275 3,650 73 122 183 243 365 520 610	377 475 2 400 2,525 7 980 5,185 8,250 146.55 246.20 369.50 494.50 755 1,082 1,297	580 2775 2775 3771 6,575 10,500 190 320 480 640 945 1,400 1,650
	48 convertes 0.465 C.Y.  72" diameter, 0.52 C.Y./L.F. 84" diameter, 1.05 C.Y./L.F. 84" diameter, 1.43 C.Y./L.F. For hell of avacian and of crete, odd  7 de Johnster, 2 Stody, 0.75 21.  10" bell diameter, 48" shoft, 4.48 C.Y.  12" bell diameter, 34" shoft, 13.6 C.Y.  14" bell diameter, 84" shoft, 13.6 C.Y.  Open style, machine drilled, to 50" deep, in soft rocks and medium hard shales, 18" diameter, 0.065 C.Y./L.F. 24" diameter, 0.182 C.Y./L.F. 30" diameter, 0.182 C.Y./L.F. 48" diameter, 0.727 C.Y./L.F. 60" diameter, 1.05 C.Y./L.F. 72" diameter, 1.05 C.Y./L.F. 84" diameter, 1.43 C.Y./L.F.	8-49 W	25 19,60 3,30 1,60 1 50 30 20 15 10 7	2.933 3.520 2.83 23.333 20.667 555 88 1.760 2.933 4.400 5.867 8.300 12.571	¥ VLE	885 1,375 450 885 1,375 9,05 16,20 25,50 36,50 65	58.00 108 129 99.20 99.20 97.5 1.10 2.025 3.225 64.50 108 161 215 325 460	122 146 149 1,200 1,100 1,100 2,275 3,650 73 122 183 243 365 520	377 475 2 400 2,505 2,700 5,185 8,250 146,55 246,20 369,50 494,50 755 1,082	580 2775 2775 3775 10,500 190 320 480 640 945 1,400
	48 covereite 0,465 C.Y.  58 wantere, 0.72 C.Y./L.F. 84" discrete, 1.05 C.Y./L.F. 84" discrete, 1.43 C.Y./L.F. For hell or exertion and coveree, odd  48 pes, ordenete, 32 strong, 0.445 g.Y.  59 hell diameter, 48" shoft, 4.48 C.Y.  12' bell diameter, 72" shoft, 8.74 C.Y. 14' bell diameter, 84" shoft, 13.6 C.Y.  Open style, machine drillad, to 50' deep, in soft rocks and medium hard shales, 18" diameter, 0.065 C.Y./L.F. 24" diameter, 0.116 C.Y./L.F. 30" diameter, 0.262 C.Y./L.F. 48" diameter, 0.262 C.Y./L.F. 48" diameter, 0.727 C.Y./L.F. 72" diameter, 0.727 C.Y./L.F. 72" diameter, 1.05 C.Y./L.F. 84" diameter, 1.143 C.Y./L.F. For bell excovarian and concrete, add	B-49	25 19,80 3,30 2,40 3,30 1,60 1 50 30 20 15 10 7 4 5	2.514 2.933 3.520 2.83 2.067 55 88 1.760 2.933 4.400 5.867 8.800 12.571 14.667 17.600	A Alte	885 1,375 450 25,50 36,50 65 102 147 200	58.00 108 129 97.5 100 2,025 3,225 64.50 108 161 215 325 460 540 645	127 146 149 1,200 1,100 1,100 2,275 3,650 73 122 183 243 365 520 610 730	377 475 2 400 2,525 7,980 5,185 8,250 146,55 246,20 369,50 494,50 7,55 1,082 1,297 1,575	580 2,975 3,000 6,575 10,500 190 320 480 640 945 1,400 1,650 2,025
	48 convertee, 0.45 C.Y.  58 decenter, 1.05 C.Y./L.F.  84" discreter, 1.43 C.Y./L.F.  84" discreter, 1.43 C.Y./L.F.  For hell or exercing and contrete, odd  72" decenterist, 30" short, 4.48 C.Y.  12" bell diameter, 48" short, 4.48 C.Y.  12" bell diameter, 48" short, 4.48 C.Y.  12" bell diameter, 84" short, 13.6 C.Y.  Open style, machine drilled, to 50" deep, in soft rocks and medium hard shales, 18" diameter, 0.065 C.Y./L.F.  24" diameter, 0.116 C.Y./L.F.  30" diameter, 0.182 C.Y./L.F.  36" diameter, 0.262 C.Y./L.F.  48" diameter, 0.72 C.Y./L.F.  60" diameter, 1.05 C.Y./L.F.  84" diameter, 1.05 C.Y./L.F.  84" diameter, 1.13 C.Y./L.F.  For bell excovarian and concrete, add  4" bell diameter, 24" short, 0.444 C.Y.	B-49	25 19,80 3,30 1,60 1 50 30 20 15 10 7 4 5	2.514 2.933 3.520 2.83 2.006/ 55 88 1.760 2.733 4.400 12.571 14.667 17.600 8.073	¥ VLE	885 1,375 450 25,50 3,65 16,20 25,50 36,50 65 102 147 200	58.00 108 129 97.50 100 87.5 97.5 1100 2,025 3,225 64.50 108 161 215 325 460 540 645 296	122 146 149 1,300 1,100 1,100 1,300 2,275 3,650 73 122 183 243 365 520 610 730 235	377 475 2 -00 2,525 2,920 5,185 8,250 146,55 246,20 369,50 494,50 7,55 1,082 1,297 1,575 676	580 2,975 3,755 10,500 190 329 480 640 945 1,400 1,650 2,025
	48 converter, 0.45 C.Y.  58 wantere, 0.45 C.Y.  72" diameter, 1.05 C.Y./L.F.  84" diameter, 1.43 C.Y./L.F.  84" diameter, 1.43 C.Y./L.F.  For hell a wyntim and of creete, old  79 feel, oldreeter, 2 stood, 0.45 gr.  91 hell diameter, 48" shoft, 4.48 C.Y.  12' bell diameter, 48" shoft, 13.6 C.Y.  Open style, machine drilled, to 50' deep, in soft rocks and medium hard shales, 18" diameter, 0.065 C.Y./L.F.  24" diameter, 0.16 C.Y./L.F.  30" diameter, 0.182 C.Y./L.F.  36" diameter, 0.182 C.Y./L.F.  48" diameter, 0.77 C.Y./L.F.  60" diameter, 1.05 C.Y./L.F.  84" diameter, 1.13 C.Y./L.F.  For bell excovarian and concrete, odd  4' hell diameter, 24" shoft, 0.444 C.Y.  6' bell diameter, 23" shoft, 1.57 C.Y.	B-49	25 19,80 3,30 1,60 1 50 30 20 15 10 7 4 5	2.514 2.933 3.520 2.83 2.83 2.83 2.867 5.55 88 1.760 2.933 4.400 7.8800 12.571 14.660 8.073 28.387	↓ VLE Ea.	885 1,375 450 25,50 36,50 65 102 147 200 45 159	58.00 108 129 97.80 87.5 97.5 17.0 2,025 3,225 64.50 108 161 215 340 540 645 296 1,050	122 146 149 1,100 1,100 1,100 2,275 3,650 73 122 183 243 365 520 610 730 335 1,175	377 475 2 400 2,525 2 90 5,185 8,250 146,55 246,20 369,50 494,50 755 1,082 1,297 1,575 676 2,384	580 2,975 3,75 6,575 10,500 190 329 489 640 945 1,450 2,025 875 3,075
	48 convertee, 0.45 C.Y.  50 wantere, 0.52 C.Y.  72" diameter, 1.05 C.Y./L.F.  84" diameter, 1.43 C.Y./L.F.  84" diameter, 1.43 C.Y./L.F.  For hell a wyntim and contrete, add  7 per contrete, 3 strong, 0.44; 21;  6 bell diameter, 48" shoft, 13.6 C.Y.  9" hell diameter, 48" shoft, 13.6 C.Y.  12" bell diameter, 34" shoft, 13.6 C.Y.  Open style, machine drillad, to 50" deep, in soft rocks and medium hard shales, 18" diameter, 0.065 C.Y./L.F.  24" diameter, 0.116 C.Y./L.F.  30" diameter, 0.182 C.Y./L.F.  36" diameter, 0.465 C.Y./L.F.  60" diameter, 0.455 C.Y./L.F.  60" diameter, 1.43 C.Y./L.F.  84" diameter, 1.43 C.Y./L.F.  84" diameter, 1.43 C.Y./L.F.  For hell excovarian and concrete, add  4' bell diameter, 24" shoft, 0.444 C.Y.  6' bell diameter, 30" shoft, 1.57 C.Y.  8' hell diameter, 36" shoft, 3.72 C.Y.	B-49	25 19,80 3,30 1,60 1 50 30 20 15 10 7 6 5 10,90 3,10 1,30	2.514 2.933 3.520 2.83 2.83 2.83 2.83 2.83 2.83 2.83 2.83	↓ VLE Ea.	885 1,375 450 25,50 36,50 65 102 147 200 45 159 375	58.00 108 129 97.80 87.5 97.5 108 109 2,025 3,225 64.50 108 161 215 325 460 540 645 296 1,050 2,475	122 146 149 1,100 1,100 1,100 2,275 3,650 73 122 183 243 365 520 610 730 335 1,175 2,800	377 475 2 400 2,525 7 980 5,185 8,250 146,55 246,20 369,50 494,50 755 1,082 1,297 1,575 676 2,384 5,650	580 2 975 3 720 6,575 10,500 190 320 480 640 945 1,600 1,650 2,025 875 3,075 7,390
	48 converter, 0.45 C.Y.  58 wantere, 0.45 C.Y.  72" diameter, 1.05 C.Y./L.F.  84" diameter, 1.43 C.Y./L.F.  84" diameter, 1.43 C.Y./L.F.  For hell a wyntim and of creete, old  79 feel, oldreeter, 2 stood, 0.45 gr.  91 hell diameter, 48" shoft, 4.48 C.Y.  12' bell diameter, 48" shoft, 13.6 C.Y.  Open style, machine drilled, to 50' deep, in soft rocks and medium hard shales, 18" diameter, 0.065 C.Y./L.F.  24" diameter, 0.16 C.Y./L.F.  30" diameter, 0.182 C.Y./L.F.  36" diameter, 0.182 C.Y./L.F.  48" diameter, 0.77 C.Y./L.F.  60" diameter, 1.05 C.Y./L.F.  84" diameter, 1.13 C.Y./L.F.  For bell excovarian and concrete, odd  4' hell diameter, 24" shoft, 0.444 C.Y.  6' bell diameter, 23" shoft, 1.57 C.Y.	B-49	25 19,80 3,30 2,40 3,30 1,60 1 50 30 20 115 10 7 4 5 5 10,90 3,10 1,30 1,30 1,30	2.514 2.933 3.520 2.83 2.83 2.83 2.867 5.55 88 1.760 2.933 4.400 7.8800 12.571 14.660 8.073 28.387	↓ VL.F. Ea.	885 1,375 450 25,50 36,50 65 102 147 200 45 159	58.00 108 129 97.80 87.5 97.5 17.0 2,025 3,225 64.50 108 161 215 340 540 645 296 1,050	122 146 149 1,100 1,100 1,100 2,275 3,650 73 122 183 243 365 520 610 730 335 1,175	377 475 7 400 2,525 7 980 5,185 8,250 146,55 746,20 969,50 494,50 755 1,082 1,297 1,575 676 2,384 5,650 6,700	580 2,975 3,75 6,575 10,500 190 329 489 640 945 1,450 2,025 875 3,075

# Appendix 5 General Conditions Estimate

# **General Conditions Estimate**

### **General Conditions Estimate**

Item	Unit	Unit Cost	Quantity	Total Cost
General Contractor Personnel (RS I	Means Page 10)			
Admin/Secretary	MTH	\$3,200.00	5	\$2,555.00
Assistant Superintendant	MTH	\$7,600.00		\$98,800.00
Superintendant	MTH	\$8,227.00	13	\$106,951.00
Project Engineer	MTH	\$7,145.00	13	
Project Manager	MTH	\$8,346.00	6.5	\$54,249.00
Senior Project Manager	MTH	\$8,660.00	1.5	
Temporary Facilities (EMJ Corporat	tion)			
Jobsite Office	MTH	\$486.67	15	\$7,300.00
Temporary Toilets	MTH	\$513.33	15	\$7,700.00
Barricades	MTH	\$66.67	15	\$1,000.00
Construction Signs	MTH	\$60.00	15	\$900.00
Dumpsters	MTH	\$133.33	15	\$2,000.00
Temporary Utilities (EMJ Corporation	on)	7. Alexandre		
Temporary Electric	MTH	\$1,000.00	15	\$15,000.00
Temporary Water	MTH	\$46.67	15	\$700.00
Temporary Telephone	MTH	\$646.67	15	\$9,700.00
Cleaning (EMJ Corporation)	35	×		
Misc. Clean-up	MTH	\$233.33	15	\$3,500.00
Site Clean-up	LS	\$2,500.00	1	\$2,500.00
Final Building Clean-up	LS	\$37,000.00	1	\$37,000.00
Miscellaneous (EMJ Corporation)				
Trash Removal	MTH	\$966.67	15	\$14,500.00
Blueprints	LS	\$3,500.00	1	\$3,500.00
Safety (Drug Testing, Equipment, etc.)	LS	\$1,500.00	1	\$1,500.00
Hand Tools	LS	\$6,000.00	1	\$6,000.00
Engineering and Layout	LS	\$2,000.00	1	\$2,000.00
Incidentals	LS	\$4,000.00		\$4,000.00
Insurance	% of Contract	\$16,786,542.00	3%	\$503,596.26
Bonds	% of Contract	\$16,786,542.00	2%	
O&P	% of Contract	\$16,786,542.00	4%	\$671,461.68
Total		0.00		\$1,998,018.78